

IN THE SUPREME COURT OF THE STATE OF NEVADA

Case No. 84345

and

Case No. 84640

Electronically Filed
May 02 2023 04:11 PM
Elizabeth A. Brown
Clerk of Supreme Court

CITY OF LAS VEGAS, a political subdivision of the State of Nevada

Appellant

v.

180 LAND CO, LLC, a Nevada limited-liability company, FORE STARS LTD.,
a Nevada limited liability company,

Respondents

District Court Case No.: A-17-758528-J
Eighth Judicial District Court of Nevada

**CITY OF LAS VEGAS' REPLY APPENDIX
VOLUME 7**

<p>LAS VEGAS CITY ATTORNEY'S OFFICE Bryan K. Scott (#4381) Jeffrey Galliher (#8078) Rebecca Wolfson (#14132) 495 S. Main Street, 6th Floor Las Vegas, NV 89101 Phone: 702.229.6629 Fax: 702.386.1749 bscott@lasvegasnevada.gov jgalliher@lasvegasnevada.gov rwolfson@lasvegasnevada.gov</p>	<p>McDONALD CARANO LLP George F. Ogilvie III (#3552) Amanda C. Yen (#9726) Christopher Molina (#14092) 2300 W. Sahara Ave, Suite 1200 Las Vegas, NV 89102 Phone: 702.873.4100 Fax: 702.873.9966 gogilvie@mcdonaldcarano.com ayen@mcdonaldcarano.com cmolina@mcdonaldcarano.com</p>
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<p>LEONARD LAW, PC Debbie Leonard (#8260) 955 S. Virginia St., Suite #220 Reno, NV 89502 775-964-4656 debbie@leonardlawpc.com</p>	<p>SHUTE, MIHALY & WEINBERGER, LLP Andrew W. Schwartz (CA Bar No. 87699) (Admitted pro hac vice) Lauren M. Tarpey (CA Bar No. 321775) (Admitted pro hac vice) 396 Hayes Street San Francisco, California 94102</p>
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CHRONOLOGICAL INDEX TO CITY'S REPLY APPENDIX

DATE	DOCUMENT	VOLUME	PAGE RANGE
2022-08-10	Plaintiff Landowners' Motion to Determine Take and for Summary Judgment on the Third and Fifth Claims for Relief, Case No. A-18-773268-C	1	REPLY APP 0001 - REPLY APP 0030
2022-08-11	Plaintiff Landowners' Appendix of Exhibits in Support of: Plaintiff Landowners' Motion to Determine Take and for Summary Judgment on the Third and Fifth Claims for Relief, Volume 22, Exhibit 214, Case No. A-18-773268-C	1	REPLY APP 0031 - REPLY APP 0227
2022-08-24	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine Volume 26, Exhibits KKKKK - LLLLL, Case No. A-18-773268-C	2	REPLY APP 0228 - REPLY APP 0364
2022-09-12	Plaintiff Landowners Reply Re: Plaintiff Landowners' Motion to Determine Take and For Summary Judgment on the Third and Fifth Claims for Relief, Case No. A-18-773268-C	2	REPLY APP 0365 - REPLY APP 0395

DATE	DOCUMENT	VOLUME	PAGE RANGE
2022-09-13	Defendant City of Las Vegas' Second Supplemental Appendix of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine Volume 32, Case No. A-18-773268-C	2	REPLY APP 0396 - REPLY APP 0432
2022-11-23	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Countermotion for Summary Judgment on Just Compensation Volume 34, Case No. A-18-773268-C	3	REPLY APP 0433 - REPLY APP 0652
2022-11-23	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Countermotion for Summary Judgment on Just Compensation Volume 35, Case No. A-18-773268-C	4 5	REPLY APP 0653 - REPLY APP 0902 REPLY APP 0903 - REPLY APP 0907
2022-11-23	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Countermotion for Summary Judgment on Just Compensation Volume 36, Case No. A-18-773268-C	5	REPLY APP 0908 - REPLY APP 1096
2022-11-23	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Countermotion for Summary Judgment on Just Compensation Volume 37, Case No. A-18-773268-C	6	REPLY APP 1097 - REPLY APP 1240

DATE	DOCUMENT	VOLUME	PAGE RANGE
2022-11-23	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Countermotion for Summary Judgment on Just Compensation Volume 38, Case No. A-18-773268-C	7	REPLY APP 1241 - REPLY APP 1406
2022-11-23	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Countermotion for Summary Judgment on Just Compensation Volume 39, Case No. A-18-773268-C	7	REPLY APP 1407 - REPLY APP 1476
2023-01-23	Defendant City of Las Vegas' Appendix of Exhibits in Support of Motion to Retax Memorandum of Costs, Volume 1, Exhibits B - C, Case No. A-18-773268-C	8	REPLY APP 1477 - REPLY APP 1667
2022-09-12	Plaintiff Landowners Second Supplement to Appendix of Exhibits in Support of Motion to Determine Take and for Summary Judgment on the Third and Fifth Claims for Relief Volume 24, Excerpt from Exhibit 228, Case No. A-18-773268-C	9	REPLY APP 1668 - REPLY APP 1742

ALPHABETICAL INDEX TO CITY'S REPLY APPENDIX

DATE	DOCUMENT	VOLUME	PAGE RANGE
2023-01-23	Defendant City of Las Vegas' Appendix of Exhibits in Support of Motion to Retax Memorandum of Costs, Volume 1, Exhibits B - C, Case No. A-18-773268-C	8	REPLY APP 1477 - REPLY APP 1667
2022-09-13	Defendant City of Las Vegas' Second Supplemental Appendix of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine Volume 32, Case No. A-18-773268-C	2	REPLY APP 0396 - REPLY APP 0432
2022-08-24	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine Volume 26, Exhibits KKKKK - LLLLL, Case No. A-18-773268-C	2	REPLY APP 0228 - REPLY APP 0364
2022-11-23	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Countermotion for Summary Judgment on Just Compensation Volume 34, Case No. A-18-773268-C	3	REPLY APP 0433 - REPLY APP 0652
2022-11-23	Defendant City of Las Vegas' Supplemental Appendix of Exhibits in Support of City's Countermotion for Summary Judgment on Just Compensation Volume 35, Case No. A-18-773268-C	4 5	REPLY APP 0653 - REPLY APP 0902 REPLY APP 0903 - REPLY APP 0907

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2022-09-12	Plaintiff Landowners Reply Re: Plaintiff Landowners' Motion to Determine Take and For Summary Judgment on the Third and Fifth Claims for Relief, Case No. A-18-773268-C	2	REPLY APP 0365 - REPLY APP 0395

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2022-09-12	Plaintiff Landowners Second Supplement to Appendix of Exhibits in Support of Motion to Determine Take and for Summary Judgment on the Third and Fifth Claims for Relief Volume 24, Excerpt from Exhibit 228, Case No. A-18-773268-C	9	REPLY APP 1668 - REPLY APP 1742
2022-08-11	Plaintiff Landowners' Appendix of Exhibits in Support of: Plaintiff Landowners' Motion to Determine Take and for Summary Judgment on the Third and Fifth Claims for Relief, Volume 22, Exhibit 214, Case No. A-18-773268-C	1	REPLY APP 0031 - REPLY APP 0227
2022-08-10	Plaintiff Landowners' Motion to Determine Take and for Summary Judgment on the Third and Fifth Claims for Relief, Case No. A-18-773268-C	1	REPLY APP 0001 - REPLY APP 0030

DATED this 2nd day of May, 2023.

BY: /s/ Debbie Leonard

<p>LAS VEGAS CITY ATTORNEY'S OFFICE Bryan K. Scott (#4381) Jeffrey Galliher (#8078) Rebecca Wolfson (#14132) 495 S. Main Street, 6th Floor Las Vegas, NV 89101 Phone: 702.229.6629 Fax: 702.386.1749 bscott@lasvegasnevada.gov jgalliher@lasvegasnevada.gov rwolfson@lasvegasnevada.gov</p>	<p>McDONALD CARANO LLP George F. Ogilvie III (#3552) Amanda C. Yen (#9726) Christopher Molina (#14092) 2300 W. Sahara Ave, Suite 1200 Las Vegas, NV 89102 Phone: 702.873.4100 Fax: 702.873.9966 gogilvie@mcdonaldcarano.com ayen@mcdonaldcarano.com cmolina@mcdonaldcarano.com</p>
<p>LEONARD LAW, PC Debbie Leonard (#8260) 955 S. Virginia St., Suite #220 Reno, NV 89502 775-964-4656 debbie@leonardlawpc.com</p>	<p>SHUTE, MIHALY & WEINBERGER, LLP Andrew W. Schwartz (CA Bar No. 87699) (Admitted pro hac vice) Lauren M. Tarpey (CA Bar No. 321775) (Admitted pro hac vice) 396 Hayes Street San Francisco, California 94102</p>

Attorneys for City of Las Vegas

CERTIFICATE OF SERVICE

I HEREBY CERTIFY that I am an employee of Leonard Law, PC, and that on this date a copy of Appendix Volumes 2-9 were electronically filed with the Clerk of the Court for the Nevada Supreme Court by using the Nevada Supreme Court's E-Filing system (E-Flex). Participants in the case who are registered with E-Flex as users will be served by the E-Flex system. All others will be served by U.S. mail.

Kermitt L. Waters
James J. Leavitt
Michael A. Schneider
Autumn L. Waters
Law Offices of Kermitt L. Waters
704 South Ninth Street
Las Vegas, Nevada 89101
Attorneys for Landowners

Elizabeth Ham
EHB Companies
1215 S. Fort Apache Road, Suite 120
Las Vegas, NV 89117
Attorneys for Landowners

Steven M. Silva
Nossaman, LP
895 Pinebrook Road
Reno, NV 89509
Attorneys for Amicus Curiae

Micah S. Echols
Claggett & Sykes Law Firm
4101 Meadows Lane, Suite 100
Las Vegas, Nevada 89107
Attorneys for Landowners

Karl Hall
Jonathan Shipman
City of Reno
1 E. First Street
P. O. Box 1900
Reno, NV 89505
Attorneys for Amicus Curiae

Brandon P. Kemble
Amanda B. Kern
Nicholas G. Vaskov
Henderson City Attorney's Office
P.O. Box 95050, MSC 144
Henderson, NV 89009
Attorneys for Amicus Curiae

Micaela Moore
North Las Vegas City Attorney's Office
2250 Las Vegas Blvd. North, #810
North Las Vegas, NV 89030
Attorneys for Amicus Curiae

Robert D. Sweetin
Davison Van Cleve
300 South 4th Street, Suite 1400
Las Vegas, NV 89101
Attorneys for Amicus Curiae

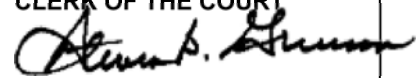
Nancy Porter
Lauren A. Landa
Goicoechea, Di Grazia, Coyle &
Stanton, Ltd.
530 Idaho Street
Elko, NV 89801
Attorneys for Amicus Curiae

Leo Cahoon
501 Mill Street
Ely, NV 89301
Attorneys for Amicus Curiae

Dated: May 2, 2023

/s/ Tricia Trevino

Tricia Trevino



1 **APEN**

2 Bryan K. Scott (NV Bar No. 4381)
3 Philip R. Byrnes (NV Bar No. 166)
4 Rebecca Wolfson (NV Bar No. 14132)
5 LAS VEGAS CITY ATTORNEY'S OFFICE
6 495 South Main Street, 6th Floor
7 Las Vegas, Nevada 89101
8 Telephone: (702) 229-6629
9 Facsimile: (702) 386-1749
10 bscott@lasvegasnevada.gov
11 pbyrnes@lasvegasnevada.gov

12 (Additional Counsel Identified on Signature Page)

13 *Attorneys for Defendant City of Las Vegas*

14 **DISTRICT COURT**

15 **CLARK COUNTY, NEVADA**

16 FORE STARS, LTD, SEVENTY ACRES, LLC, a
17 Nevada limited liability company, DOE
18 INDIVIDUALS I through X, DOE
19 CORPORATIONS I through X, DOE LIMITED
20 LIABILITY COMPANIES I through X,

21 Plaintiffs,

22 CITY OF LAS VEGAS, political subdivision of the
23 State of Nevada, THE EIGHTH JUDICIAL
24 DISTRICT COURT, County of Clark, State of
25 Nevada, DEPARTMENT 24 (the HONORABLE JIM
26 CROCKETT, DISTRICT COURT JUDGE, IN HIS
27 OFFICIAL CAPACITY), ROE government entities I
28 through X, ROE Corporations I through X, ROE
INDIVIDUALS I through X, ROE LIMITED
LIABILITY COMPANIES I through X, ROE quasi-
governmental entities I through X,

Defendants.

Case No. A-18-773268-C
Dept. No. XXIX

**SUPPLEMENTAL APPENDIX OF
EXHIBITS IN SUPPORT OF CITY'S
COUNTERMOTION FOR SUMMARY
JUDGMENT ON JUST COMPENSATION**

VOLUME 38

23 The City of Las Vegas ("City") submits this Supplemental Appendix of Exhibits in support of its
24 Countermotion for Summary Judgment on Just Compensation. This appendix supplements the Appendix
25 of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine filed
26 August 11, 2022 (Volumes 1 through 25); the Supplemental Appendix of Exhibits in Support of City's
27 Renewed Motion for Summary Judgment and Motions in Limine filed August 24, 2022 (Volumes 26
28

through 27); the Second Supplemental Appendix of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine filed September 12, 2022 (Volumes 28 through 32); and the Third Supplemental Appendix of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine filed September 14, 2022 (Volume 33).

Exhibit	Exhibit Description	Vol.	Bates No.
A	City records regarding William Peccole's Petition to Annex 2,246 acres to the City of Las Vegas	1	0001-0011
B	City records regarding the Peccole Land Use Plan and the Z-34-81 rezoning application	1	0012-0030
C	City records regarding the Venetian Foothills Master Plan and the Z-30-86 rezoning application	1	0031-0050
D	Excerpts of the 1985 City of Las Vegas General Plan	1	0051-0061
E	City records regarding Peccole Ranch Master Plan and phase I rezoning application (Z-139-88)	1	0062-0106
F	City records regarding Z-40-89 rezoning application	1	0107-0113
G	Ordinance No. 3472 (establishing the Gaming Enterprise District) and related records	1	0114-0137
H	City records regarding the Amended Peccole Ranch Master Plan and phase II rezoning application (Z-17-90)	1	0138-0194
I	Excerpts of 1992 City of Las Vegas General Plan	2	0195-0248
J	City records related to Badlands Golf Course expansion	2	0249-0254
K	Excerpt of land use case files for GPA-24-98 and GPA-6199	2	0255-0257
L	Ordinance No. 5250 and Excerpts of Las Vegas 2020 Master Plan	2	0258-0273
M	Miscellaneous Southwest Sector Land Use Maps from 2002-2005	2	0274-0277
N	Ordinance No. 5787 and Excerpts of 2005 Land Use Element	2	0278-0291
O	Ordinance No. 6056 and Excerpts of 2009 Land Use & Rural Neighborhoods Preservation Element	2	0292-0301
P	Ordinance No. 6152 and Excerpts of 2012 Land Use & Rural Neighborhoods Preservation Element	2	0302-0317
Q	Ordinance No. 6622 and Excerpts of 2018 Land Use & Rural Neighborhoods Preservation Element	2	0318-0332
R	Ordinance No. 1582	2	0333-0339
S	Ordinance No. 4073 and Excerpt of the 1997 City of Las Vegas Zoning Code	2	0340-0341

Exhibit	Exhibit Description	Vol.	Bates No.
T	Ordinance No. 5353	2	0342-0361
U	Ordinance No. 6135 and Excerpts of City of Las Vegas Unified Development Code adopted March 16, 2011	2	0362-0364
V	Deeds transferring ownership of the Badlands Golf Course	2	0365-0377
W	Third Revised Justification Letter regarding the Major Modification to the 1990 Conceptual Peccole Ranch Master Plan	2	0378-0381
X	Parcel maps recorded by the Developer subdividing the Badlands Golf Course	3	0382-0410
Y	EHB Companies promotional materials	3	0411-0445
Z	General Plan Amendment (GPA-62387), Rezoning (ZON-62392) and Site Development Plan Review (SDR-62393) applications	3	0446-0466
AA	Staff Report regarding 17-Acre Applications	3	0467-0482
BB	Major Modification (MOD-63600), Rezoning (ZON-63601), General Plan Amendment (GPA-63599), and Development Agreement (DIR-63602) applications	3	0483-0582
CC	Letter requesting withdrawal of MOD-63600, GPA-63599, ZON-63601, DIR-63602 applications	4	0583
DD	Transcript of February 15, 2017 City Council meeting	4	0584-0597
EE	Judge Crockett's March 5, 2018 order granting Queensridge homeowners' petition for judicial review, Case No. A-17-752344-J	4	0598-0611
FF	Docket for NSC Case No. 75481	4	0612-0623
GG	Complaint filed by Fore Stars Ltd. and Seventy Acres LLC, Case No. A-18-773268-C	4	0624-0643
HH	General Plan Amendment (GPA-68385), Site Development Plan Review (SDR-68481), Tentative Map (TMP-68482), and Waiver (68480) applications	4	0644-0671
II	June 21, 2017 City Council meeting minutes and transcript excerpt regarding GPA-68385, SDR-68481, TMP-68482, and 68480.	4	0672-0679
JJ	Docket for Case No. A-17-758528-J	4	0680-0768
KK	Judge Williams' Findings of Fact and Conclusions of Law, Case No. A-17-758528-J	5	0769-0793
LL	Development Agreement (DIR-70539) application	5	0794-0879
MM	August 2, 2017 City Council minutes regarding DIR-70539	5	0880-0882

Exhibit	Exhibit Description	Vol.	Bates No.
NN	Judge Sturman's February 15, 2019 minute order granting City's motion to dismiss, Case No. A-18-775804-J	5	0883
OO	Excerpts of August 2, 2017 City Council meeting transcript	5	0884-0932
PP	Final maps for Amended Peccole West and Peccole West Lot 10	5	0933-0941
QQ	Excerpt of the 1983 Edition of the Las Vegas Municipal Code	5	0942-0951
RR	Ordinance No. 2185	5	0952-0956
SS	1990 aerial photograph identifying Phase I and Phase II boundaries, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0957
TT	1996 aerial photograph identifying Phase I and Phase II boundaries, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0958
UU	1998 aerial photograph identifying Phase I and Phase II boundaries, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0959
VV	2015 aerial photograph identifying Phase I and Phase II boundaries, retail development, hotel/casino, and Developer projects, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0960
WW	2015 aerial photograph identifying Phase I and Phase II boundaries, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0961
XX	2019 aerial photograph identifying Phase I and Phase II boundaries, and current assessor parcel numbers for the Badlands property, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0962
YY	2019 aerial photograph identifying Phase I and Phase II boundaries, and areas subject to inverse condemnation litigation, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0963
ZZ	2019 aerial photograph identifying areas subject to proposed development agreement (DIR-70539), produced by the City's Planning & Development	5	0964

Exhibit	Exhibit Description	Vol.	Bates No.
	Department, Office of Geographic Information Systems (GIS)		
AAA	Membership Interest Purchase and Sale Agreement	6	0965-0981
BBB	Transcript of May 16, 2018 City Council meeting	6	0982-0998
CCC	City of Las Vegas' Amicus Curiae Brief, <i>Seventy Acres, LLC v. Binion</i> , Nevada Supreme Court Case No. 75481	6	0999-1009
DDD	Nevada Supreme Court March 5, 2020 Order of Reversal, <i>Seventy Acres, LLC v. Binion</i> , Nevada Supreme Court Case No. 75481	6	1010-1016
EEE	Nevada Supreme Court August 24, 2020 Remittitur, <i>Seventy Acres, LLC v. Binion</i> , Nevada Supreme Court Case No. 75481	6	1017-1018
FFF	March 26, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Entitlements on 17 Acres	6	1019-1020
GGG	September 1, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Final Entitlements for 435-Unit Housing Development Project in Badlands	6	1021-1026
HHH	Complaint Pursuant to 42 U.S.C. § 1983, <i>180 Land Co. LLC et al. v. City of Las Vegas, et al.</i> , 18-cv-00547 (2018)	6	1027-1122
III	9th Circuit Order in <i>180 Land Co. LLC; et al v. City of Las Vegas, et al.</i> , 18-cv-0547 (Oct. 19, 2020)	6	1123-1127
JJJ	Plaintiff Landowners' Second Supplement to Initial Disclosures Pursuant to NRCP 16.1 in 65-Acre case	6	1128-1137
LLL	Bill No. 2019-48: Ordinance No. 6720	7	1138-1142
MMM	Bill No. 2019-51: Ordinance No. 6722	7	1143-1150
NNN	March 26, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Entitlement Requests for 65 Acres	7	1151-1152
OOO	March 26, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Entitlement Requests for 133 Acres	7	1153-1155

Exhibit	Exhibit Description	Vol.	Bates No.
PPP	April 15, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Entitlement Requests for 35 Acres	7	1156-1157
QQQ	Valbridge Property Advisors, Lubawy & Associates Inc., Appraisal Report (Aug. 26, 2015)	7	1158-1247
RRR	Notice of Entry of Order Adopting the Order of the Nevada Supreme Court and Denying Petition for Judicial Review	7	1248-1281
SSS	Letters from City of Las Vegas Approval Letters for 17-Acre Property (Feb. 16, 2017)	8	1282-1287
TTT	Reply Brief of Appellants 180 Land Co. LLC, Fore Stars, LTD., Seventy Acres LLC, and Yohan Lowie in <i>180 Land Co LLC et al v. City of Las Vegas</i> , Court of Appeals for the Ninth Circuit Case No. 19-16114 (June 23, 2020)	8	1288-1294
UUU	Excerpt of Reporter's Transcript of Hearing on City of Las Vegas' Motion to Compel Discovery Responses, Documents and Damages Calculation and Related Documents on Order Shortening Time in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (Nov. 17, 2020)	8	1295-1306
VVV	Plaintiff Landowners' Sixteenth Supplement to Initial Disclosures in <i>180 Land Co., LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (Nov. 10, 2020)	8	1307-1321
WWW	Excerpt of Transcript of Las Vegas City Council Meeting (Aug. 2, 2017)	8	1322-1371
XXX	Notice of Entry of Findings of Facts and Conclusions of Law on Petition for Judicial Review in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (Nov. 26, 2018)	8	1372-1399
YYY	Notice of Entry of Order <i>Nunc Pro Tunc</i> Regarding Findings of Fact and Conclusion of Law Entered November 21, 2019 in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528 (Feb. 6, 2019)	8	1400-1405
ZZZ	City of Las Vegas Agenda Memo – Planning, for City Council Meeting June 21, 2017, Re: GPA-68385, WVR-68480, SDR-68481, and TMP-68482 [PRJ-67184]	8	1406-1432

Exhibit	Exhibit Description	Vol.	Bates No.
AAAA	Excerpts from the Land Use and Rural Neighborhoods Preservation Element of the City's 2020 Master Plan adopted by the City Council of the City on September 2, 2009	8	1433-1439
BBBB	Summons and Complaint for Declaratory Relief and Injunctive Relief, and Verified Claims in Inverse Condemnation in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No.A-18-780184-C	8	1440-1477
CCCC	Notice of Entry of Findings of Fact and Conclusions of Law Granting City of Las Vegas' Motion for Summary Judgment in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No.A-18-780184-C (Dec. 30, 2020)	8	1478-1515
DDDD	Peter Lowenstein Declaration	9	1516-1522
DDDD-1	Exhibit 1 to Peter Lowenstein Declaration: Diagram of Existing Access Points	9	1523-1526
DDDD-2	Exhibit 2 to Peter Lowenstein Declaration: July 5, 2017 Email from Mark Colloton	9	1527-1531
DDDD-3	Exhibit 3 to Peter Lowenstein Declaration: June 28, 2017 Permit application	9	1532-1533
DDDD-4	Exhibit 4 to Peter Lowenstein Declaration: June 29, 2017 Email from Mark Colloton re Rampart and Hualapai	9	1534-1536
DDDD-5	Exhibit 5 to Peter Lowenstein Declaration: August 24, 2017 Letter from City Department of Planning	9	1537
DDDD-6	Exhibit 6 to Peter Lowenstein Declaration: July 26, 2017 Email from Peter Lowenstein re Wall Fence	9	1538
DDDD-7	Exhibit 7 to Peter Lowenstein Declaration: August 10, 2017 Application for Walls, Fences, or Retaining Walls; related materials	9	1539-1546
DDDD-8	Exhibit 8 to Peter Lowenstein Declaration: August 24, 2017 Email from Steve Gebeke	9	1547-1553
DDDD-9	Exhibit 9 to Peter Lowenstein Declaration: Bill No. 2018-24	9	1554-1569
DDDD-10	Exhibit 10 to Peter Lowenstein Declaration: Las Vegas City Council Ordinance No. 6056 and excerpts from Land Use & Rural Neighborhoods Preservation Element	9	1570-1577

Exhibit	Exhibit Description	Vol.	Bates No.
DDDD-11	Exhibit 11 to Peter Lowenstein Declaration: documents submitted to Las Vegas Planning Commission by Jim Jimmerson at February 14, 2017 Planning Commission meeting	9	1578-1587
EEEE	GPA-72220 application form	9	1588-1590
FFFF	Chris Molina Declaration	9	1591-1605
FFFF-1	Fully Executed Copy of Membership Interest Purchase and Sale Agreement for Fore Stars Ltd.	9	1606-1622
FFFF-2	Summary of Communications between Developer and Peccole family regarding acquisition of Badlands Property	9	1623-1629
FFFF-3	Reference map of properties involved in transactions between Developer and Peccole family	9	1630
FFFF-4	Excerpt of appraisal for One Queensridge place dated October 13, 2005	9	1631-1632
FFFF-5	Site Plan Approval for One Queensridge Place (SDR-4206)	9	1633-1636
FFFF-6	Securities Redemption Agreement dated September 14, 2005	9	1637-1654
FFFF-7	Securities Purchase Agreement dated September 14, 2005	9	1655-1692
FFFF-8	Badlands Golf Course Clubhouse Improvement Agreement dated September 6, 2005	9	1693-1730
FFFF-9	Settlement Agreement and Mutual Release dated June 28, 2013	10	1731-1782
FFFF-10	June 12, 2014 emails and Letter of Intent regarding the Badlands Golf Course	10	1783-1786
FFFF-11	July 25, 2014 email and initial draft of Golf Course Purchase Agreement	10	1787-1813
FFFF-12	August 26, 2014 email from Todd Davis and revised purchase agreement	10	1814-1843
FFFF-13	August 27, 2014 email from Billy Bayne regarding purchase agreement	10	1844-1846
FFFF-14	September 15, 2014 email and draft letter to BGC Holdings LLC regarding right of first refusal	10	1847-1848

Exhibit	Exhibit Description	Vol.	Bates No.
FFFF-15	November 3, 2014 email regarding BGC Holdings LLC	10	1849-1851
FFFF-16	November 26, 2014 email and initial draft of stock purchase and sale agreement	10	1852-1870
FFFF-17	December 1, 2015 emails regarding stock purchase agreement	10	1871-1872
FFFF-18	December 1, 2015 email and fully executed signature page for stock purchase agreement	10	1873-1874
FFFF-19	December 23, 2014 emails regarding separation of Fore Stars Ltd. and WRL LLC acquisitions into separate agreements	10	1875-1876
FFFF-20	February 19, 2015 emails regarding notes and clarifications to purchase agreement	10	1877-1879
FFFF-21	February 26, 2015 email regarding revised purchase agreements for Fore Stars Ltd. and WRL LLC	10	1880
FFFF-22	February 27, 2015 emails regarding revised purchase agreements for Fore Stars Ltd. and WRL LLC	10	1881-1882
FFFF-23	Fully executed Membership Interest Purchase Agreement for WRL LLC	10	1883-1890
FFFF-24	June 12, 2015 email regarding clubhouse parcel and recorded parcel map	10	1891-1895
FFFF-25	Quitclaim deed for Clubhouse Parcel from Queensridge Towers LLC to Fore Stars Ltd.	10	1896-1900
FFFF-26	Record of Survey for Hualapai Commons Ltd.	10	1901
FFFF-27	Deed from Hualapai Commons Ltd. to EHC Hualapai LLC	10	1902-1914
FFFF-28	Purchase Agreement between Hualapai Commons Ltd. and EHC Hualapai LLC	10	1915-1931
FFFF-29	City of Las Vegas' First Set of Interrogatories to Plaintiff	10	1932-1945
FFFF-30	Plaintiff 180 Land Company LLC's Responses to City of Las Vegas' First Set of Interrogatories to Plaintiff, 3 rd Supplement	10	1946-1973
FFFF-31	City of Las Vegas' Second Set of Requests for Production of Documents to Plaintiff	11	1974-1981

Exhibit	Exhibit Description	Vol.	Bates No.
FFFF-32	Plaintiff 180 Land Company LLC's Response to Defendant City of Las Vegas' Second Set of Requests for Production of Documents to Plaintiff	11	1982-1989
FFFF-33	September 14, 2020 Letter to Plaintiff regarding Response to Second Set of Requests for Production of Documents	11	1990-1994
FFFF-34	First Supplement to Plaintiff Landowners Response to Defendant City of Las Vegas' Second Set of Requests for Production of Documents to Plaintiff	11	1995-2002
FFFF-35	Motion to Compel Discovery Responses, Documents and Damages Calculation, and Related Documents on Order Shortening Time	11	2003-2032
FFFF-36	Transcript of November 17, 2020 hearing regarding City's Motion to Compel Discovery Responses, Documents and Damages Calculation, and Related Documents on Order Shortening Time	11	2033-2109
FFFF-37	February 24, 2021 Order Granting in Part and denying in part City's Motion to Compel Discovery Responses, Documents and Damages Calculation, and Related Documents on Order Shortening Time	11	2110-2118
FFFF-38	April 1, 2021 Letter to Plaintiff regarding February 24, 2021 Order	11	2119-2120
FFFF-39	April 6, 2021 email from Elizabeth Ghanem Ham regarding letter dated April 1, 2021	11	2121-2123
FFFF-40	Hydrologic Criteria and Drainage Design Manual, Section 200	11	2124-2142
FFFF-41	Hydrologic Criteria and Drainage Design Manual, Standard Form 1	11	2143
FFFF-42	Hydrologic Criteria and Drainage Design Manual, Standard Form 2	11	2144-2148
FFFF-43	Email correspondence regarding minutes of August 13, 2018 meeting with GCW regarding Technical Drainage Study	11	2149-2152
FFFF-44	Excerpts from Peccole Ranch Master Plan Phase II regarding drainage and open space	11	2153-2159
FFFF-45	Aerial photos and demonstrative aids showing Badlands open space and drainage system	11	2160-2163
FFFF-46	August 16, 2016 letter from City Streets & Sanitation Manager regarding Badlands Golf Course Drainage Maintenance	11	2164-2166

Exhibit	Exhibit Description	Vol.	Bates No.
FFFF-47	Excerpt from EHB Companies promotional materials regarding security concerns and drainage culverts	11	2167
GGGG	Landowners' Reply in Support of Countermotion for Judicial Determination of Liability on the Landowners' Inverse Condemnation Claims Etc. in <i>180 Land Co., LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (March 21, 2019)	11	2168-2178
HHHH	June 28, 2016 Letter from Mark Colloton re: Reasons for Access Points Off Hualapai Way and Rampart Blvd.	12	2179-2184
IIII	Transcript of City Council Meeting (May 16, 2018)	12	2185-2260
JJJJ	Excerpt of April 8, 2021 Transcript of Hearing re Plaintiffs' Motion for a New Trial and to Amend (March 11, 2021), Case No. A-18-780184-C	12	2261-2266
KKKK	Affidavit of Donald Richards and accompanying photographs submitted by the Developer on April 15, 2021 in Case No. A-18-780184-C	13	2267-2428
LLLL	Supplemental Declaration of Seth T. Floyd	14	2429-2432
LLLL-1	1981 Peccole Property Land Use Plan	14	2433-
LLLL-2	1985 Las Vegas General Plan	14	2434-2515
LLLL-3	1975 General Plan	14	2516-2611
LLLL-4	Planning Commission meeting records regarding 1985 General Plan	15	2612-2839
LLLL-5	1986 Venetian Foothills Master Plan	15	2840
LLLL-6	1989 Peccole Ranch Master Plan	15	2841
LLLL-7	1990 Master Development Plan Amendment	15	2842
LLLL-8	Citizen's Advisory Committee records regarding 1992 General Plan	15	2843-2860
LLLL-9	1992 Las Vegas General Plan	16-17	2861-3310
LLLL-10	1992 Southwest Sector Map	18	3311
LLLL-11	Ordinance No. 5250 (Adopting 2020 Master Plan)	18	3312-3319

Exhibit	Exhibit Description	Vol.	Bates No.
LLLL-12	Las Vegas 2020 Master Plan	18	3320-3402
LLLL-13	Ordinance No. 5787 (Adopting 2005 Land Use Element)	18	3403-3469
LLLL-14	2005 Land Use Element	18	3470-3527
LLLL-15	Ordinance No. 6056 (Adopting 2009 Land Use and Rural Neighborhoods Preservation Element)	18	3528-3532
LLLL-16	2009 Land Use and Rural Neighborhoods Preservation Element	19	3533-3632
LLLL-17	Ordinance No. 6152 (Adopting revisions to 2009 Land Use and Rural Neighborhoods Preservation Element)	19	3633-3642
LLLL-18	Ordinance No. 6622 (Adopting 2018 Land Use and Rural Neighborhoods Preservation Element)	19	3643-3653
LLLL-19	2018 Land Use & Rural Neighborhoods Preservation Element	19	3654-3753
MMMM	State of Nevada State Board of Equalization Notice of Decision, <i>In the Matter of Fore Star Ltd., et al.</i> (Nov. 30, 2017)	20	3754-3758
NNNN	Clark County Real Property Tax Values	20	3759-3774
OOOO	Clark County Tax Assessor's Property Account Inquiry - Summary Screen	20	3775-3776
PPPP	February 22, 2017 Clark County Assessor Letter to 180 Land Co. LLC, re Assessor's Golf Course Assessment	20	3777
QQQQ	Petitioner's Opening Brief, <i>In the matter of 180 Land Co. LLC</i> (Aug. 29, 2017), State Board of Equalization	20	3778-3815
RRRR	September 21, 2017 Clark County Assessor Stipulation for the State Board of Equalization	20	3816
SSSS	Excerpt of Reporter's Transcript of Hearing in <i>180 Land Co. v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (Feb. 16, 2021)	20	3817-3868
TTTT	June 28, 2016 Letter from Mark Colloton re: Reasons for Access Points Off Hualapai Way and Rampart Blvd.	20	3869-3874

Exhibit	Exhibit Description	Vol.	Bates No.
UUUU	Transcript of City Council Meeting (May 16, 2018)	20	3875-3950
VVVV	Supplemental declaration of Seth Floyd	21	3951-3953
VVVV-1	Southwest Sector Land Use Map (1992)	21	3954
VVVV-2	10/10/1991 Planning Commission Minutes	21	3955-3957
VVVV-3	10/22/1991 Planning Commission Minutes	21	3958-3962
VVVV-4	11/14/1991 Planning Commission Minutes	21	3963-3965
VVVV-5	11/26/1991 Planning Commission Minutes	21	3966-3968
VVVV-6	12/12/1991 Planning Commission Minutes	21	3969-3976
VVVV-7	12/12/1991 Planning Commission Resolution adopting 1992 General Plan	21	3977-3978
VVVV-8	2/5/1992 City Council Meeting Minutes	21	3979
VVVV-9	2/18/1992 Recommending Committee Meeting Minutes	21	3980-4000
VVVV-10	2/19/1992 City Council Meeting Minutes	21	4001-4002
VVVV-11	3/12/1992 Planning Commission Meeting Minutes	21	4003-4004
VVVV-12	3/16/1992 Recommending Committee Meeting Minute	21	4005
VVVV-13	4/1/1992 City Council Meeting Minutes	21	4006-4008
VVVV-14	Ordinance No. 3636 (adopting new general plan)	21	4009-4011

Exhibit	Exhibit Description	Vol.	Bates No.
VVVV-15	2/13/1992 Citizens Advisory Committee Meeting Minutes	21	4012-4015
VVVV-16	3/27/1991 Citizens Advisory Committee Mailout	21	4016-4025
WWWW	Excerpts of NRCP 30(b)(6) Designee of Peccole Nevada Corporation – William Bayne	21	4026-4039
XXXX	Findings of Facts, Conclusions of Law and Order Regarding Motion to Dismiss and Countermotion to Allow More Definite Statement if Necessary and Countermotion to Stay Litigation of Inverse Condemnation Claims Until Resolution of the Petition for Judicial Review and Countermotion for NRCP Rule 56(F) Continuance	21	4040-4051
YYYY	Declaration of Christopher Molina in Support of the City's Countermotion for Summary Judgment and Opposition to Motion to Determine Property Interest	21	4052-4053
ZZZZ	Declaration of Seth Floyd	21	4054-4055
ZZZZ -1	Master planned communities with R-PD zoning	21	4056-4061
ZZZZ -2	General Plan Maps for Master Planned Communities with R-PD zoning	21	4062-4067
AAAAA	Recorder's Amended Transcript of Pending Motions in <i>180 Land Company LLC, et al. vs. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-18-775804 (September 17, 2021)	22	4068-4235
BBBBB	December 23, 2021 letter from Seth Floyd re Entitlements on 17-acre Property; Applications for development of other segments of former Badlands Golf Course	22	4236-4238
CCCCC	July 19, 2022 letter from Seth Floyd re Entitlements on 17-acre portion of Badlands	22	4239-4240
DDDDD	Appraisal of Real Property prepared by The DiFederico Group re the 17-Acre Property	23	4241-4394
EEEEEE	Affidavit of Donald Richards (Ex. 50 to Plaintiff Landowners' Reply in Support of Countermotion for Discovery Pursuant to NRCP 56(d) filed 7/7/2021)	23	4395-4396
FFFFF	Bill No. 2018-5 (Ordinance No. 6617)	23	4397-4405

Exhibit	Exhibit Description	Vol.	Bates No.
GGGGG	Appraisal Consulting Report prepared by Charles E. Jack of Integra Realty Resources	24	4406-4586
HHHHH	Supplemental Declaration Peter Lowenstein	24	4587-4600
HHHHH-1	Email from Steve Swanton re PMP – 58526 and PMP-58527 (Queensridge/Badlands Golf Course)	24	4601-4602
HHHHH-2	June 8, 2015 letter to Angie Scott from Steve Swanton re PMP-59572	24	4603
HHHHH-3	Email from Stephanie Allen to Peter Lowenstein re Development Agreement	24	4604-4605
HHHHH-4	Email from Lucien Paet re New Badlands Parcel Map	24	4606
HHHHH-5	Approved Site Plan for SDR-62393	24	4607
IIIII	Declaration of Kevin McOsker	25	4608-4609
JJJJJ	Videotaped Deposition of Tio Stephan DiFederico, MAI	25	4610-4711
KKKKK	Appellant's Opening Brief filed 11/6/18 in Nevada Supreme Court Case No. 75481	26	4712-4791
LLLLL	Appellant's Amended Reply Brief filed 5/1/19 in Nevada Supreme Court Case No. 75481	26	4792-4829
MMMMM	City of Las Vegas's Motion for Summary Judgment filed 11/9/20 in the 65-Acre Case (No. A-18-780184-C)	26	4830-4862
NNNNN	Plaintiff Landowners' Opposition to the City's Motion for Summary Judgment Etc. filed 11/23/20 in the 65-Acre Case (No. A-18-780184-C)	26	4863-4950
OOOOO	City of Las Vegas' Motion to Remand 133-Acre Applications to the Las Vegas City Council filed 8/9/2021 in the 133-Acre Case (No. A-18-775804-J)	27	4951-4961
PPPPP	Notice of Entry of Findings of Fact, Conclusions of Law Regarding (1) Motion to Remand 133-Acre Applications to Las Vegas City Council and (2) Motion to Dismiss Civil Complaint Improperly Joined with Petition for Judicial Review	27	4962-4973

Exhibit	Exhibit Description	Vol.	Bates No.
QQQQQ	Deposition Transcript of Charles E. Jack, June 16, 2022	28	4974-5168
RRRRR	Deposition Transcript of NRCP 30(b)(6) Designee of Peccole Nevada Corporation – William Bayne	29	5169-5411
SSSSS	Order Granting the City of Las Vegas' Motion to Compel and for an Order to Show Cause in the 35-Acre Case (No. A-17-758528-J)	30	5412-5416
TTTTT	Order Granting the City of Las Vegas' Objection to the Discovery Commissioner's Report and Recommendation in the 35-Acre Case (No. A-17-758528-J)	30	5417-5422
UUUUU	Appraisal of Real Property prepared by The DiFederico Group re the 35-Acre Property	30	5423-5558
VVVVV	Excerpts of Deposition Transcript of Yohan Lowie	31	5559-5566
WWWWW	Declaration of Philip R. Byrnes in Support of City's Reply in Support of City's Renewed Motion for Summary Judgment and City's Motion to Strike Developer's Countermotion for Approval of Entitlements and to End Take	32	5567-5568
WWWWW-1	Agenda Summary Page for Item 28 of the August 3, 2022 Las Vegas City Council meeting	32	5569-5570
WWWWW-2	Settlement Proposal	32	5571-5583
XXXXX	Order Granting Stay	33	5584-5588
YYYYY	Declaration of Oh-Sang Kwon	34	5589-5595
YYYYY-1	Technical Drainage Study for the Seventy 840-050 March 2016	34-35	5596-5982
YYYYY-2	Supplement to Technical Drainage Study for the Seventy 840-050 March 2016	35	5983-6024
YYYYY-3	March 24, 2016 City of Las Vegas Inter-Office Memorandum re Drainage Study for The Seventy	36	6025-6028
YYYYY-4	September 2017 Response to 1st CLV Comments on the Technical Drainage Study for the 435 (Formerly "The Seventy")	36	6029-6193
YYYYY-5	September 14, 2017 - Improvement Plans for the 435	37	6194-6210
YYYYY-6	March 24, 2016 City of Las Vegas Inter-Office Memorandum re Drainage Study for The Seventy	37	6211-6215
YYYYY-7	January 2018 Response to 2nd CLV Comments on the Technical Drainage Study for the 435 (Formerly "The Seventy")	37	6216-6292

Exhibit	Exhibit Description	Vol.	Bates No.
YYYYY-8	January 10, 2018 - Improvement Plans for the 435	37	6293-6309
YYYYY-9	February 1, 2018 City of Las Vegas Inter-Office Memorandum re Drainage Study for the 435 formerly the SEVENTY	37	6310-6314
YYYYY-10	June 2018 Response to 3 rd CLV Comments on the Technical Drainage Study for the 435 (Formerly "The Seventy")	38	6315-6461
YYYYY-11	Improvement Plans for the 435	39	6462-6483
YYYYY-12	July 26, 2018 City of Las Vegas Inter-Office Memorandum re Drainage Study for the 435 formerly the Seventy	39	6484-6489
YYYYY-13	August 13, 2016 GCW Engineers Meeting Minutes	39	6490-6495
YYYYY-14	Email re The 435 TD5 Comments Review Meeting	39	6496-6499
ZZZZZ	Declaration of Michael Cunningham	39	6500
ZZZZZ-1	Administrative Code, 2019 Edition	39	6501-6507

Dated this 23rd day of November, 2022.

McDONALD CARANO LLP

By: /s/ George F. Ogilvie III

George F. Ogilvie III (NV Bar No. 3552)
Christopher Molina (NV Bar No. 14092)
2300 W. Sahara Avenue, Suite 1200
Las Vegas, Nevada 89102

LAS VEGAS CITY ATTORNEY'S OFFICE
Bryan K. Scott (NV Bar No. 4381)
Philip R. Byrnes (NV Bar No. 166)
Rebecca Wolfson (NV Bar No. 14132)
495 South Main Street, 6th Floor
Las Vegas, Nevada 89101

SHUTE, MIHALY & WEINBERGER, LLP
Andrew W. Schwartz (CA Bar No. 87699)
(Admitted *pro hac vice*)
Lauren M. Tarpey (CA Bar No. 321775)
(Admitted *pro hac vice*)
396 Hayes Street
San Francisco, California 94102

Attorneys for City of Las Vegas

1 **CERTIFICATE OF SERVICE**

2 I HEREBY CERTIFY that I am an employee of McDonald Carano LLP, and that on the 23rd
3 day of November, 2022, I caused a true and correct copy of the foregoing **FOURTH SUPPLEMENTAL**
4 **APPENDIX OF EXHIBITS IN SUPPORT OF CITY'S COUNTERMOTION FOR SUMMARY**
5 **JUDGMENT ON JUST COMPENSATION – VOLUME 38** to be electronically served with the
6 Clerk of the Court via the Clark County District Court Electronic Filing Program which will provide
7 copies to all counsel of record registered to receive such electronic notification.

8 /s/ Jelena Jovanovic

9 An employee of McDonald Carano LLP

EXHIBIT “YYYYYY-10”

**RESPONSE TO 3RD CLV COMMENTS
ON THE
TECHNICAL DRAINAGE STUDY FOR THE 435
(FORMERLY "THE SEVENTY")**

840-050

June 2018



Prepared for:

Seventy Acres LLC
9775 West Charleston Boulevard
Las Vegas, Nevada 89117
Phone: (702) 940-6930
Fax: (702) 940-6931

HYDROLOGIC CRITERIA AND DRAINAGE MANUAL
DRAINAGE STUDY INFORMATION FORM

Name of Development: The 435 (formerly known as The Seventy) Date: June 2018

Location of Development: a) Descriptive (Cross Streets) North/South: Hualapai Way

East/West: Rampart Boulevard

b) Section: 32,31 Township: 20S Range: 60E

c) APN : 138-32-301-005

Name of Owner: Seventy Acres LLC

Telephone No.: (702) 940-6930 Fax No.: (702) 940-6931 E-Mail Address: frank@EHBcompanies.com

Address: 9775 W. Charleston Blvd., Las Vegas, Nevada 89117

Contact Person-Name: Steve Jones, P.E. Telephone No.: (702) 804-2000

* E-Mail Address: SJones@gcwengineering.com Fax No.: (702) 804-2299

Firm: GCW, Inc.

Address: 1555 South Rainbow Blvd, Las Vegas, NV 89146

Type of Land Development/Land Disturbance Process:

<input type="checkbox"/>	Rezoning	<input type="checkbox"/>	Subdivision Map	<input type="checkbox"/>	Clearing and Grading Only
<input type="checkbox"/>	Parcel Map	<input type="checkbox"/>	Planned Unit Development	<input checked="" type="checkbox"/>	Other (Please specify below)
<input type="checkbox"/>	Large Parcel Map	<input type="checkbox"/>	Building Permit	<input type="checkbox"/>	Conceptual Drianage, Rough Grade, SD

1. Total Owned Land Area: At Site: +/- 70.52 acres Being Developed/Disturbed: +/- 17.5 acres

2. Is a portion or all of the subject property located in a designated FEMA Flood Hazard Area? ☒ Yes** ☐ No

3. Is the property bordered or crossed by an existing or proposed Clark County Regional Flood

Control District Master Planned Facility? ☒ Yes** ☐ No

4. Proposed type of development (Residential, Commercial, Etc.): Conceptual Drainage, Rough Grade, and Storm Drain Improvements

5. Approximate upstream land area which drains to the subject site: +/- 3.73 sq. mi.

6. Has the site drainage been evaluated in the past? ☒ YES ☐ NO If yes, please identify documentation: Peccole Ranch West Master Study, Queensridge LOMR, Queens Borough Culvert Study

7. If known, please briefly identify the proposed discharge point(s) of runoff from the site: Existing dual (2) - 12'X 12' RCB at northeast corner of site

8. Briefly describe your proposed schedule for the subject project: Phase 1 Infrastructure (This Study), Phase 1 Improvements (Future Study), Phase 2 - Remaining 52.1 acres (Future Studies)



Engineer's Seal

Submit this form as part of the required drainage study to the local entity which has jurisdiction over the subject property. This form may provide sufficient information to serve as the Conceptual Drainage Study.

***New Required Field**

****Review and concurrence of the Clark County Regional Flood Control District is required.**

Revision	Date

Local Entity File No. _____

REFERENCE:

STANDARD FORM 1

**RESPONSE TO 3RD CLV COMMENTS
ON THE
TECHNICAL DRAINAGE STUDY FOR THE 435
(FORMERLY "THE SEVENTY")**

840-050

June 2018

Prepared for:

**Seventy Acres LLC
9775 West Charleston Boulevard
Las Vegas, Nevada 89117
Phone: (702) 940-6930
Fax: (702) 940-6931**

Prepared By:

**GCW, Inc.
1555 S. Rainbow Blvd.
Las Vegas, Nevada 89146
Phone: (702) 804-2000
Fax: (702) 804-2299**

840-050

June 28, 2018

Albert Sung, PE
City of Las Vegas – Department of Public Works
333 N. Rancho Drive – 7th Floor
Las Vegas, NV 89106

**Re: 3rd Response to City of Las Vegas Comments on the
Technical Drainage Study for "The 435" (DS4787C)**

Dear Mr. Sung:

This letter addresses City of Las Vegas (CLV) second review comments dated February 1, 2018 and provides an update on design changes based off of a meeting held on February 21, 2018 between the City of Las Vegas (CLV) and GCW.

Levee

The previous design included an embankment that acted as a levee to direct flow to an open top RCB. The levee and open top RCB are no longer proposed, instead the mainline will be extended further upstream in a similar manner to the first submittal of the project during the interim condition to collect the majority of the flow, with laterals extending from the mainline in key locations to collect the remaining runoff. Note that the size of the proposed RCB for the extension is 10'X10' RCB which differs from the first submittal of the project. The WSPG model has been updated and is included in the appendix. Inlet control calculations for stubs collecting flow in the interim condition and normal depth calculations for all stubs based off of the worst case flow rate have also been included in the appendix.

Hydrology

An interim condition HEC-1 model was prepared to compare with flow rates from the ultimate conditions, MPU, and FEMA flow rates. The interim condition showed a flow rate downstream of the improvements that was higher than the previously modeled ultimate condition flow rate. A separate interim condition WSPG model was prepared to show the higher flow rate meets criteria.

Corrugated Wall Face

Per the aforementioned meeting between CLV and GCW, a corrugated wall face with a 1-inch deep pattern on both sides of the channel along with 3-inches of sacrificial concrete with a tined flow line on the bottom of the channel will be provided at sections to help prevent velocities from exceeding 35 ft/s. A combined Manning's value of 0.023 for mainline 1 and 0.024 for mainline 2 was calculated using a Manning's value of 0.020 for the tined sacrificial concrete bottom and 0.026 for the 1" deep pattern (0.026 Manning's duplicates a D50=1-Inch riprap). The sections with the sacrificial concrete and corrugated wall face include a 30-foot section in the transition before the existing dual 12-foot by 12-foot RCB in the mainline 1 model, a 251-foot section upstream of WSPG station -7825.45 in the mainline 1 model, and a 126-foot section upstream

1555 South Rainbow Boulevard
Las Vegas, Nevada 89146



O 702.804.2000
F 702.804.2299



info@gcwengineering.com
gcwengineering.com

of WSPG station -2775.61 in the mainline 2 model. Note that velocities exceed 35 ft/s by 0.77 ft/s in the 30-foot transition section and by 0.2 ft/s at station 78+25.45 in the mainline 1 model. Since these sections are short and immediately return to below 35 ft/s, 3-inches of sacrificial concrete with corrugated wall facing is provided in the sections, and 35 ft/s is only exceeded by 0.77 ft/s in the worst location the design is considered to be adequate. The mainline 1 and 2 models have been updated and are included in the appendix.

The CLV comment letter has been included in Appendix A for reference. Below are individual responses to each comment included in the review letter.

Comment: "1. An effective HEC-RAS model to determine the existing water surface elevation within the FEMA Special Flood Hazard Area Zone A is required. This model will serve as the base model to develop the duplicate effective model, corrected effective model, pre-project condition model and post-project condition model."

Response: An effective HEC-RAS model has been provided. Figure 9 has been included in the appendix that shows the location of the sections and a summary table of the HEC-RAS model.

Comment: "2. Provide a comparison summary of the HEC-RAS results for the existing, interim, and proposed wash conditions."

Response: The wash is no longer proposed to weir into an open top RCB, therefore interim and proposed condition HEC-RAS models are no longer applicable.

Comment: "3. Extend the HEC-RAS model further upstream to analyze the effects of the sedimentation berms."

Response: The sedimentation berms are no longer proposed with the project.

Comment: "4. Additional HEC-RAS cross sections are required at the weir (upstream and downstream), at the sediment berms, and the turn within the open RCB. Update the model and exhibits accordingly."

Response: The open top RCB and weir are no longer proposed with this project per the upfront discussion.

Comment: "5. For the FEMA flood zone WSE evaluation, the computational flow regime should be "sub-critical flow" not "mix flow" to provide a conservative WSE for floodplain assessment."

Response: The interim and proposed condition HEC-RAS models are no longer applicable. The existing condition HEC-RAS model that is included uses a subcritical flow regime. The HEC-RAS model has been included in the appendix.

Comment: "6. The hydraulic models do not provide a relationship between Mainline 2 and Mainline 1 at the junction structure. The junction structure acts as a major point of confluence and is a critical section of the system. Revise the WSPG and HEC-RAS models to better demonstrate the interaction of the systems (Mainline 1, Mainline 2, and wash) at the junction."

Response: The open top RCB at the wash is no longer proposed. Mainline 2 utilizes the HGL at the junction structure from the Mainline 1 model.

Comment: "7. Based on the results of Comment 6, the computed flow depth at the end of the Mainline 2 system should be used as the initial flow condition at Mainline 1 Station -7536.97 and should be applied as the boundary condition for the HEC-RAS model when conducting the WSE evaluation."

Response: Comment no longer applicable due to design change.

Comment: "8. There is an existing hydraulic jump at the end of the Mainline 1 system per sheet C-6 of the referenced plan for "The Village at Queensridge Culvert". The WSE of 2635.91 should be used as the downstream boundary condition (SO) to incorporate the hydraulic jump impacting the overall storm drain hydraulic performance and avoid any negative impacts to the downstream condition; Or input parameters should be adjusted to reproduce the hydraulic jump as shown on sheet C-6 to evaluate the proposed storm drain system hydraulic performance."

Response: The hydraulic jump seen on sheet C-6 was caused by an embankment located downstream of the outlet. The embankment was removed per the 2nd Update to the Technical Drainage Study for Queens Borough Culvert (DS3674), however the improvement plans were not updated to accurately show the HGL. Refer to the referenced WSPG model and text excerpt from the 2nd update included in the appendix for the starting water surface elevation.

Comment: "9. The Mainline 1 system includes an existing 72-inch (Station -9391.3) with a WSE of 2669.252. Provide a comparison between the current design and the previously approved study/design to assess any negative impacts to the upstream and downstream facilities."

Response: The HGL proposed with this study is 0.48-ft higher during the interim condition and 0.19-ft higher in the ultimate condition compared to the previously approved study which had the HGL at the top of the 72" pipe. This difference is considered insignificant due to the depth of the pipe. An improvement plan sheet showing the culvert HGL has been included in the appendix.

Comment: "10. Include curvature information in the WSPG model for Mainline 2 to estimate super-elevation. Furthermore, with the high flow quantity over 2,000-cfs and a flow velocity of 38.04-fps, which is equal to 22.5-feet of velocity head and super-critical flow condition, roll wave in the straight reach, super-elevation and cross wave along a curve reach and a possible oblique jump should be considered. Ensure the proposed channel cross section provides a stabilized flow condition with sufficient freeboard."

Response: Comment no longer applicable due to design change.

Comment: "11. Provide headwater calculations at the RCB entrance from the open box section."

Response: The open top RCB is no longer proposed. An inlet control calculation has been provided for the entrance of the newly proposed RCB extension.

Comment: "12. Provide updated weir calculations for the revised weir length of the open RCB."

Response: The open top RCB is no longer proposed.

Comment: "13. The future minimum finished floor elevations must be higher than the manholes/road grades of the future road. Revise accordingly."

Response: Plans have been revised so that future minimum finished floor elevations are higher than manholes/road grades of the future road.

Comment: "14. Show 16-foot min. width gates and provide details at maintenance access points from Alta Drive and Rampart Boulevard."

Response: A 16-foot width gate has been provided and details at the maintenance access point from Alta Drive has been provided.

Comment: "15. Verify the existing golf course bridge has adequate capacity and clearance for maintenance vehicles and equipment."

Response: The access road from Rampart Boulevard and utilizing the golf cart bridge near the LVVWD facility is no longer proposed. The access road is now along the top of the RCB with a path down to the 20'X12' RCB opening.

Comment: "16. Show a maintenance access road down to the interim channel area."

Response: Maintenance access roads have been provided to the interim collection areas.

Comment: "17. Revise the post and cable details to reflect a 3-cable fence system."

Response: The post and cable details have been revised to reflect a 3-cable fence system.

Comment: "18. A levee is proposed along the northern side of the interim channel, adjacent to southwestern future development lots. Per Section 303.6.2 of the Manual, since the flood control levee is proposed within a FEMA SFHA and a map revision will be requested based on the levee providing protection against the 100-year flood, FEMA's levee criteria shall be used in order for FEMA to credit the levee. For FEMA to accredit a levee system with 1-percent-annual-chance flood hazard reduction capability on a FIRM, the community/levee owner must submit a package containing the required data and documentation to show that the levee system meets all design and operation requirements of 44 CFR 65.10."

Response: Per the upfront discussion a levee is no longer proposed.

Comment: "19. It is unclear on the profile on Sheet C5.03 where the bottom of the channel is located and how high the HGL is at this section. It appears that the upstream end of the open box is only 2-feet high which means the western wall of the RCB is not fully constructed. Clarify the design of open box section."

Response: Comment no longer applicable due to design change.

Comment: "20. Verify the stationing of SDMH #109 on the profile on Sheet C5.04."

Response: The stationing of SDMH #109 has been corrected.

Comment: "21. Revise the call outs on the lateral profile sheets to call out Construction Note 12 to install temporary plug and cap storm drain line."

Response: The call outs on the lateral profile sheets have been revised to call out construction note 12.

Comment: "22. Revise Sections 5 and 9 on Sheet C8.01 to show the same rip rap specifications for the bottom of the interim channel."

Response: Sections 5 and 9 are no longer proposed per the upfront discussion.

Comment: "23. Revise Sections 3 and 8 on Sheet C8.01 to specify the same scarification extents."

Response: The note has been removed from Section 3 since it is a drainage easement detail based on trench width for the proposed RCB.

Comment: "24. Provide details of the proposed walls at the entrance into the 20' x 12' RCB."

Response: Details for the proposed walls at the entrance into the 20' x 12' RCB have been provided.

The following comments are repeated to reflect routine items previously acknowledged by the Engineer.

Comment: "25. This site development is located within a FEMA SPECIAL FLOOD HAZARD AREA, Zone A. **No permits will be issued until a Conditional Letter of Map Revision (CLOMR/CLOMR-F) is received from FEMA. Permits may be issued upon the receipt of Conditional Letter of Map Revision (CLOMR or CLOMR-F) from FEMA.**"

Response: The requirement for FEMA coordination to receive permits is acknowledged.

Comment: "26. A Letter of Map Revision (LOMR/LOMR-F) must be obtained from FEMA after the completion of any project within a FEMA Special Flood Hazard Area, Flood Zone "A". The bonded improvements shall include a line item of \$50,000.00 for the LOMR. The bonded improvements will not be released until the LOMR/LOMR-F is obtained from FEMA and filed with the City of Las Vegas."

Response: The requirement for an additional bond with regards to LOMR approval is acknowledged.

Comment: "27. The site is located within the Flood Zone A and is adjacent to an existing or proposed *Clark County Regional Flood Control District* (CCRFCD) master planned facility. Therefore, CCRFCD concurrence is required prior to final approval of the drainage study."

Response: The requirement of CCRFCD concurrence prior to final approval is acknowledged.

Comment: "28. Please obtain necessary 404 permits from US Army Corps of Engineers and provide a copy of the permit to City of Las Vegas Flood Control Section prior to issuance of the grading permit. Contact the St. George Field Office of the US Army Corps of Engineers for permit information."

Response: It is acknowledged that necessary 404 permits are required prior to issuance of the grading permit.

Comment: "29. Provide complete *Plans and Project Specifications* for approval by the *City of Las Vegas*. The Structural Plans and Details shall be a part of the Civil Improvement Plan set. This project is considered as a *Capital Improvement Project* (CIP) with developer funding."

Response: Complete Plans and Project Specifications will be provided to the City of Las Vegas for approval after the approval of the technical drainage study. It is acknowledged that the structural plans and details will be part of the Civil Improvement Plan set and that the project is considered a CIP project.

Comment: "30. Structural plans for the proposed storm drain improvements and pertinent flood control facilities must be submitted for review. Provide a soils report, structural calculations and specifications, two wet stamped structural sets, and a grading plan to the *Building Department* for processing. The engineer must provide a copy of *Building Department* approval of the structures to Regional Flood prior to their concurrence and to *Flood Control* prior to final acceptance of the drainage study."

Response: Structural plans for the proposed storm drain improvements and pertinent flood control facilities will be submitted for review after the approval of the technical drainage study. A soils report, structural calculations and specifications, two wet stamped structural sets, and a grading plan will be provided to the *Building Department* for processing. It is acknowledged that Building Department approval must be provided to Regional Flood for concurrence and to Flood Control prior to final acceptance.

Comment: "31. All proposed improvements associated with the Storm Drain facilities shall be bonded and inspected. This project shall require Special Inspection. Coordinate the requirements of and the Agreements needed for Special Inspection with the Building Department."

Response: It is acknowledged that the storm drain facilities must be bonded and inspected and that the project will require special inspection. The requirements and agreements needed for special inspection will be coordinated with the building department.

Comment: "32. The proposed improvements show drainage facilities of a size that must be reviewed for access and maintenance concerns. The engineer must submit an extra set of improvement plans to the *City Streets & Sanitation Department* for their review and comments. *Streets & Sanitation Department's* approval must be secured prior to the conditional drainage study approval."

Response: Updated plans will continue to be submitted to the City Street and Sanitation Department for their review and comments.

Comment: "33. Provide new public drainage easements for the area of the site impacted by the proposed MPU facility improvements. The easement shall note that the public drainage improvements (MPU facilities) are publicly maintained and all onsite storm drain and surface improvements are privately maintained and the easement must be dedicated and recorded by separate document prior to the final acceptance of the improvement plans. Provide legal description and an exhibit of the drainage easement to Flood Control and *Rae Heller* (702-229-2139) of *City of Las Vegas Right of Way Section* for the recordation process after the subject drainage study is conceptually approved. The existing drainage easements shall be vacated by separate action and the recording of the new easements shall be done consecutively."

Response: New public drainage easements with the note that the MPU facilities are publically maintained and onsite storm drain and surface improvements are privately maintained have been provided. It is acknowledged that the easement must be dedicated and recorded prior to final acceptance of the improvement plans. A legal description and exhibit will be provided to Flood Control and Mary Wulff for the recordation process after conceptual approval. It is acknowledged that the existing drainage easements shall be vacated by separate action and the recording of new easement will be done consecutively.

Comment: "34. Technical drainage studies are required for each of the future development super pads. The technical drainage studies for the developments may not be submitted until the conditional approval of this pertinent infrastructure drainage study is obtained. Final approval for the infrastructure study must be obtained prior to conditional approval of the impacted development super pad drainage studies."

Response: It is acknowledged that technical drainage studies are needed for future development of the super pads. It is also noted that conditional approval of this study is required before the submittal of the technical drainage studies for the future developments and that final approval of this study is required prior to conditional approval of the future development studies.

Comment: "35. This project currently has no Proposed Buildings or Structures. Should the project propose changes to this design assumption, then the Engineer is to update the drainage study detailing the flood zone impacts and provide addresses for each building in a FEMA Flood Hazard Zone prior to obtaining a grading permit. This information is necessary to insure that the elevation certificates are provided for each address prior to completion of construction. This information is required until such time as a LOMR is approved that removes the development from the SFHA."

Response: Comment acknowledged.

Comment: "36. Proposed storm drain laterals have been identified to collect flows from Peccole West Lot 9 and Queensridge Fairway Homes. Extend the storm drain system to collect the 100-year flows from these adjacent subdivisions."

Response: Comment will be addressed in future study.

Comment: "37. Continue to coordinate the MPU facility changes that are proposed with this development."

Response: MPU facility changes will continue to be coordinated.

Comment: "38. Storm drain facilities are located on cut/fill slopes. Revise the slopes and/or the storm drain alignment to maintain 12-foot access roads. Provide a cross section detail of the maintenance access."

Response: 12-foot access roads on top of storm drain to every manhole and inlet opening is maintained. Maintenance access details are included in the improvement plans.

Comment: "39. Provide a concrete pad and maintenance access to the inlet structures for the local storm drains. Show the needed drainage easements for these facilities."

Response: Maintenance access and drainage easements have been provided. Concrete pads have been provided at the inlet locations for the trunk RCBs for public maintenance. All other storm drains are to be privately maintained and do not require concrete pads.


Comment: "40. The existing and proposed utility crossings of the storm drain must be shown on the storm drain plan and profiles sheets and on the lateral profiles. Indicate the type of pipe material for water and sewer lines. Review separation requirements between utilities and show all of the utility crossings of the storm drains."

Response: Existing utilities that intersect the alignment of the proposed storm drain are shown in the storm drain profiles. Note the existing sewer at approximate Station 66+40 has adequate clearance.

If you have any questions or require additional information, please do not hesitate to contact me at 804-2130.

Respectfully,

GCW, INC.



Nelson Baggs, E.I.
Flood Control Division

Enclosures

c: Gia Nguyen, GCW
Steve Jones, GCW
Scott Plummer, GCW

**THE 435 – 3rd CLV Response to Comments
APPENDIX LAYOUT**

Appendix A. City of Las Vegas Comments

1. February 1, 2018 CLV Comments

Appendix B. Hydrologic Calculations

1. Interim HEC-1 Model

Appendix C. Hydraulic Calculations

1. Ultimate Condition Main 1 WSPG Model
2. Interim Condition Main 1 WSPG Model
3. Mainline 1 Inlet Control Calculation
4. Transition Length Calculation
5. Ultimate Condition Main 2 WSPG Model
6. Stub Inlet Control Calculations
7. Pipe Normal Depth Calculations
8. Lateral Loss Calculations
9. Existing Conditions HEC-RAS Model
10. Interim Ditch Normal Depth Calculation

Appendix D. Drainage Exhibits

1. Figure 7R – Storm Drain Facility Summary
2. Figure 8R – WSPG Exhibit
3. Figure 9 - Effective HEC-RAS Cross Section Map
4. Figure 15 – Interim Condition Drainage Map


Appendix E. Reference Material

1. 2nd Update to the Technical Drainage Study for Queens Borough Culvert
 - a. CLV Approval Letter
 - b. Text Excerpt: Embankment Removal
 - c. WSPG Model
2. 72-Inch at (2) 12'X12' RCB Storm Drain Profile

Appendix F. Improvement Plans (Folded Separately)

APPENDIX A

City of Las Vegas Comments

CITY OF LAS VEGAS		DATE:
INTER-OFFICE MEMORANDUM		February 1, 2018
TO: Land Development Services Department of Building & Safety		FROM: Jennifer Shinn  Flood Control Engr. Associate Department of Public Works
SUBJECT: Drainage Study for: The 435 formerly The SEVENTY		COPIES TO: GCW Engineers
Cross Streets:	SWC of Rampart & Alta	Seventy Acres LLC
File Number:	F:\Depot\DSMemos\DS4787C.ZNA.doc	Bart Anderson, P.E., DevCo
Parcel Number:	138-32-301-005, 006, 210-008	CCRFCD
Zoning Action:	SDR-62393; GPA-62387; ZON-62392	
FEMA Flood Zone	YES <input checked="" type="checkbox"/> NO	
Proposed Storm Drain	YES <input checked="" type="checkbox"/> NO	

HISTORY	DATE RECEIVED	DATE REVIEWED	COMMENTS	REVIEW FEES	FEES PAID Payment Trn #
1 st Submittal	3/3/2016 & 3/9/2016	3/23/2016	See Comments Below	\$400.00	425231: \$400
2 nd Submittal	9/18/17	11/9/2017	See Comments Below	\$400.00	490193: \$400
3 rd Submittal	1/11/18	2/1/2018	See Comments Below	\$400.00	492825: \$400
TOTAL FEES (LDDRS):				\$1200.00	----

REMARKS: This site development is within a FEMA SPECIAL FLOOD HAZARD AREA, Zone A. No permits of any kind will be issued for this project until a Conditional Letter of Map Revision (CLOMR/CLOMR-F) is received from FEMA.

The Drainage Study for the subject project has been reviewed and:

	is approved subject to conformance to all City standards and the following conditions:
X	must be resubmitted or supplemented including the following:
	is conditionally approved subject to Clark County Regional Flood Control District concurrence.
	is conditionally approved subject to NDOT concurrence.

1. An effective HEC-RAS model to determine the existing water surface elevation within the FEMA Special Flood Hazard Area Zone A is required. This model will serve as the base model to develop the duplicate effective model, corrected effective model, pre-project condition model and post-project condition model.
2. Provide a comparison summary of the HEC-RAS results for the existing, interim, and proposed wash conditions.
3. Extend the HEC-RAS model further upstream to analyze the effects of the sedimentation berms.
4. Additional HEC-RAS cross sections are required at the weir (upstream and downstream), at the sediment berms, and the turn within the open RCB. Update the model and exhibits accordingly.

5. For the FEMA flood zone WSE evaluation, the computational flow regime should be "sub-critical flow" not "mix flow" to provide a conservative WSE for floodplain assessment.
6. The hydraulic models do not provide a relationship between Mainline 2 and Mainline 1 at the junction structure. The junction structure acts as a major point of confluence and is a critical section of the system. Revise the WSPG and HEC-RAS models to better demonstrate the interaction of the systems (Mainline 1, Mainline 2, and wash) at the junction.
7. Based on the results of Comment 6, the computed flow depth at the end of the Mainline 2 system should be used as the initial flow condition at Mainline 1 Station -7536.97 and should be applied as the boundary condition for the HEC-RAS model when conducting the WSE evaluation.
8. There is an existing hydraulic jump at the end of the Mainline 1 system per sheet C-6 of the referenced plan for "The Village at Queensridge Culvert". The WSE of 2635.91 should be used as the downstream boundary condition (SO) to incorporate the hydraulic jump impacting the overall storm drain hydraulic performance and avoid any negative impacts to the downstream condition; Or input parameters should be adjusted to reproduce the hydraulic jump as shown on sheet C-6 to evaluate the proposed storm drain system hydraulic performance.
9. The Mainline 1 system includes an existing 72-inch (Station -9391.3) with a WSE of 2669.252. Provide a comparison between the current design and the previously approved study/design to assess any negative impacts to the upstream and downstream facilities.
10. Include curvature information in the WSPG model for Mainline 2 to estimate super-elevation. Furthermore, with the high flow quantity over 2,000-cfs and a flow velocity of 38.04-fps, which is equal to 22.5-feet of velocity head and super-critical flow condition, roll wave in the straight reach, super-elevation and cross wave along a curve reach and a possible oblique jump should be considered. Ensure the proposed channel cross section provides a stabilized flow condition with sufficient freeboard.
11. Provide headwater calculations at the RCB entrance from the open box section.
12. Provide updated weir calculations for the revised weir length of the open RCB.
13. The future minimum finished floor elevations must be higher than the manholes/road grades of the future road. Revise accordingly.
14. Show 16-foot min. width gates and provide details at maintenance access points from Alta Drive and Rampart Boulevard.
15. Verify the existing golf course bridge has adequate capacity and clearance for maintenance vehicles and equipment.
16. Show a maintenance access road down to the interim channel area.
17. Revise the post and cable details to reflect a 3-cable fence system.
18. A levee is proposed along the northern side of the interim channel, adjacent to southwestern future development lots. Per Section 303.6.2 of the Manual, since the flood control levee is proposed within a FEMA SFHA and a map revision will be requested based on the levee providing protection against the 100-year flood, FEMA's levee criteria shall be used in order for FEMA to credit the levee. For FEMA to accredit a levee system with 1-percent-annual-chance flood hazard reduction capability on a FIRM, the community/levee owner must submit a package containing the required data and documentation to show that the levee system meets all design and operation requirements of 44 CFR 65.10.

19. It is unclear on the profile on Sheet C5.03 where the bottom of the channel is located and how high the HGL is at this section. It appears that the upstream end of the open box is only 2-feet high which means the western wall of the RCB is not fully constructed. Clarify the design of open box section.
20. Verify the stationing of SDMH #109 on the profile on Sheet C5.04.
21. Revise the call outs on the lateral profile sheets to call out Construction Note 12 to install temporary plug and cap storm drain line.
22. Revise Sections 5 and 9 on Sheet C8.01 to show the same rip rap specifications for the bottom of the interim channel.
23. Revise Sections 3 and 8 on Sheet C8.01 to specify the same scarification extents.
24. Provide details of the proposed walls at the entrance into the 20' x 12' RCB.

The following comments are repeated to reflect routine items previously acknowledged by the Engineer.

25. This site development is located within a FEMA SPECIAL FLOOD HAZARD AREA, Zone A. **No permits will be issued until a Conditional Letter of Map Revision (CLOMR/CLOMR-F) is received from FEMA. Permits may be issued upon the receipt of Conditional Letter of Map Revision (CLOMR or CLOMR-F) from FEMA.**
26. A Letter of Map Revision (LOMR/LOMR-F) must be obtained from FEMA after the completion of any project within a FEMA Special Flood Hazard Area, Flood Zone "A". The bonded improvements shall include a line item of **\$50,000.00** for the LOMR. The bonded improvements will not be released until the LOMR/LOMR-F is obtained from FEMA and filed with the City of Las Vegas.
27. The site is located within the Flood Zone A and is adjacent to an existing or proposed *Clark County Regional Flood Control District (CCRCD)* master planned facility. Therefore, CCRCD concurrence is required prior to final approval of the drainage study.
28. Please obtain necessary 404 permits from US Army Corps of Engineers and provide a copy of the permit to City of Las Vegas Flood Control Section prior to issuance of the grading permit. Contact the St. George Field Office of the US Army Corps of Engineers for permit information.
29. Provide complete *Plans and Project Specifications* for approval by the *City of Las Vegas*. The Structural Plans and Details shall be a part of the Civil Improvement Plan set. This project is considered as a *Capital Improvement Project (CIP)* with developer funding.
30. Structural plans for the proposed storm drain improvements and pertinent flood control facilities must be submitted for review. Provide a soils report, structural calculations and specifications, two wet stamped structural sets, and a grading plan to the *Building Department* for processing. The engineer must provide a copy of *Building Department* approval of the structures to Regional Flood prior to their concurrence and to *Flood Control* prior to final acceptance of the drainage study.
31. All proposed improvements associated with the Storm Drain facilities shall be bonded and inspected. This project shall require Special Inspection. Coordinate the requirements of and the Agreements needed for Special Inspection with the Building Department.
32. The proposed improvements show drainage facilities of a size that must be reviewed for access and maintenance concerns. The engineer must submit an extra set of improvement plans to the *City Streets & Sanitation Department* for their review and comments. *Streets & Sanitation Department's* approval must be secured prior to the conditional drainage study approval.
33. Provide new public drainage easements for the area of the site impacted by the proposed MPU facility improvements. The easement shall note that the public drainage improvements (MPU

facilities) are publicly maintained and all onsite storm drain and surface improvements are privately maintained and the easement must be dedicated and recorded by separate document prior to the final acceptance of the improvement plans. Provide legal description and an exhibit of the drainage easement to Flood Control and *Rae Heller* (702-229-2139) of *City of Las Vegas Right of Way Section* for the recordation process after the subject drainage study is conceptually approved. The existing drainage easements shall be vacated by separate action and the recording of the new easements shall be done consecutively.

34. Technical drainage studies are required for each of the future development super pads. The technical drainage studies for the developments may not be submitted until the conditional approval of this pertinent infrastructure drainage study is obtained. Final approval for the infrastructure study must be obtained prior to conditional approval of the impacted development super pad drainage studies.
35. This project currently has no Proposed Buildings or Structures. Should the project propose changes to this design assumption, then the Engineer is to update the drainage study detailing the flood zone impacts and provide addresses for each building in a FEMA Flood Hazard Zone prior to obtaining a grading permit. This information is necessary to insure that the elevation certificates are provided for each address prior to completion of construction. This information is required until such time as a LOMR is approved that removes the development from the SFHA.

Flood Control understands that this overall project will be developed in Phases. The following comments are repeated to reflect items that shall be addressed in future study updates as the Phases develop.

36. Proposed storm drain laterals have been identified to collect flows from Peccole West Lot 9 and Queensridge Fairway Homes. Extend the storm drain system to collect the 100-year flows from these adjacent subdivisions.
37. Continue to coordinate the MPU facility changes that are proposed with this development.
38. Storm drain facilities are located on cut/fill slopes. Revise the slopes and/or the storm drain alignment to maintain 12-foot access roads. Provide a cross section detail of the maintenance access.
39. Provide a concrete pad and maintenance access to the inlet structures for the local storm drains. Show the needed drainage easements for these facilities.
40. The existing and proposed utility crossings of the storm drain must be shown on the storm drain plan and profiles sheets and on the lateral profiles. Indicate the type of pipe material for water and sewer lines. Review separation requirements between utilities and show all of the utility crossings of the storm drains.

NOTE: Please be advised that all land surface area disturbances over 1 acre or any area adjacent to a water way must submit to the *Nevada Division of Environmental Protection* a "Notice of Intent" to discharge that certifies a stormwater pollution prevention plan has been developed and is maintained on site; for inclusion in the Stormwater General Permit No. NVR100000. A phased construction unit in a contiguous subdivision is considered under construction until all stripped or disturbed surface areas have been covered by paving, building construction or planting. For more information, including forms and applications see <http://ndep.nv.gov/bwpc/storm01.htm> or call (775) 687-9429.

NOTE: The engineer must submit the drainage study to FEMA for a Conditional Letter of Map Revision (CLOMR). A favorable CLOMR must be obtained prior to the issuance of any permits. This site is located in a **FEMA Zone A**. *Clark County Regional Flood Control District* (CCRFCD) review and approval is required prior to recordation of final map or issuance of building/grading permits. The Engineer must send a copy of the report to the CCRFCD for review. **The developer/engineer must also obtain a Letter of Map Revision (LOMR) using the approved drainage study as technical support to inform FEMA of the modifications within the flood zone. The approved LOMR must be submitted to the City of Las Vegas prior to the release of the bond.** FEMA Elevation Certificates, showing as-built finish floor elevations, must be completed for each building in the FEMA A Zone. The certificate must be submitted to the *City of Las Vegas Flood Control Section* prior to scheduling a framing inspection.

END OF REMARKS
JKS/PBJ

T/R/S: T20S/R60E/12
AREA L-32

APPENDIX B

Hydrologic Calculations

```
1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*      JUN 1998
*      VERSION 4.1
*
* RUN DATE 21JUN18 TIME 08:10:45
*
*****

INT.OUT

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
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X   X XXXXXX XXXX      X
X   X X      X   X     XX
X   X X      X       X
XXXXXX XXXX  X   XXXXX X
X   X X      X       X
X   X X      X   X     X
X   X XXXXXX XXXXX    XXX
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

*DIAGRAM
1 ID *****
2 ID * .....: *
3 ID * : .....: *
4 ID * : THE 435 : *
5 ID * : .....: *
6 ID * : INTERIM CONDITIONS : *
7 ID * : .....: *
8 ID * : RETURN PERIOD _ _ _ 100 & 10 -YEAR : *
9 ID * : DISTRIBUTION _ _ _ 6-HOUR SDN3 : *
10 ID * : PROJECT NO _ _ _ 840.050 : *
11 ID * : FILENAME _ _ _ INT.H1 : *
12 ID * : DATE MODELED _ _ _ 6/08/18 : *
13 ID * : MODELED BY _ _ _ NB : *
14 ID * : .....: *
15 ID * : .....: *
16 ID * : .....: *
17 ID *****
18 ID
19 ID REFERENCED HYDROLOGIC MODELS:
20 ID 2013 LAS VEGAS VALLEY FLOOD CONTROL MASTER PLAN UPDATE
21 ID CITY OF LAS VEGAS CITY WIDE HYDROLOGY ANALYSIS (PBS&J 1997)
22 ID CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2008 MASTER PLAN UPDATE
23 ID GOWAN WATERSHED (ALL)
24 ID RECOMMENDED DRAINAGE SYSTEM WITH ULTIMATE DEVELOPMENT
25 ID INPUT FILE = ALLGOW3.DAT
26 ID INPUT FILE DATE = MAY 5, 2008
27 ID DESIGN STORM = 100-YEAR 6-HR STORM
28 ID STORM DISTRIBUTION = SDN #3
29 ID MODELED BY PBS&J (MICHELE L. D'ALESSANDRO, E.I., CFM)
30 ID CHECKED BY PBS&J (HARSHAL B. DESAI, P.E., CFM)
31 ID STORM CENTERING = FULL WATERSHED
32 ID JR CARDS CONTAIN DARFS BASED ON THE FOLLOWING VALUES:
33 ID
34 ID AREA DARF
35 ID SQ. MI.
36 ID 0-0.5 0.99
37 ID 0.5-1 0.975
38 ID 1-2 0.95
39 ID 2-3 0.925
40 ID 3-4 0.915
41 ID 4-5 0.908
42 ID 5-6 0.903
43 ID 6-7 0.895
44 ID 10yr 0.570
45 ID
46 ID JR CARD RATIOS REPRESENT DEPTH-AREA REDUCTION FACTORS (DARF'S)
47 ID
48 ID 100-YEAR, 6-HOUR STORM, SDN3
49 ID
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Page 1

INT.OUT

50	IT	5	0	0	650						
51	IO	5	0	0							
52	IN	5	0	0							
53	JR	PREC	0.99	0.975	0.95	0.925	0.915	0.908	0.903	0.895	0.570

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

54	KK	ON5									
55	KM	OFFSITE BASIN ON5									
56	PB	3.05									
57	BA	0.0147									
58	PC	0	0.02	0.057	0.07	0.087	0.108	0.124	0.13	0.13	0.13
59	PC	0.13	0.13	0.13	0.133	0.14	0.142	0.148	0.158	0.172	0.181
60	PC	0.19	0.197	0.199	0.2	0.201	0.204	0.214	0.229	0.241	0.249
61	PC	0.251	0.256	0.27	0.278	0.281	0.283	0.295	0.322	0.352	0.409
62	PC	0.499	0.59	0.71	0.744	0.781	0.812	0.819	0.835	0.851	0.856
63	PC	0.86	0.868	0.876	0.888	0.91	0.926	0.937	0.95	0.97	0.976
64	PC	0.982	0.985	0.987	0.989	0.99	0.993	0.993	0.994	0.995	0.998
65	PC	0.998	0.999	1							
66	LS	0	82								
67	UD	.105									

68	KK	57B-3C									
69	KM	OFFSITE BASIN 57B-3C									
70	PB	3.05									
71	BA	0.0069									
72	LS	0	87								
73	UD	.118									

74	KK	ON6									
75	KM	OFFSITE BASIN ON6									
76	PB	3.04									
77	BA	0.0035									
78	LS	0	93								
79	UD	.057									

80	KK	CON6									
81	KM	COMBINE 57B-3C AND ON6									
82	HC	2									

83	KK	CCON6									
84	KM	COMBINE ON5 AND CON6									
85	HC	2									

86	KK	RCCON6									
87	KM	ROUTE CCON6 TO CON8									
88	KM	LENGTH SLOPE n-VALUE				SHAPE	WIDTH	S-SLOPE			
89	RD	2015 .037 .040	0	TRAP	20	2					

90	KK	ON8									
91	KM	ONSITE BASIN ON8									
92	PB	2.99									
93	BA	0.0190									
94	LS	0	82								
95	UD	.073									

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

96	KK	CON8									
97	KM	COMBINE CCON6 AND ON8									
98	HC	2									

99	KK	SW11									
100	BA	0.589									
101	PB	3.34									
102	LS	0	87.8								
103	UD	0.311									

104	KK	RSW11									
105	KM	ROUTE SW11 TO CSW17									
106	KM	FACILITY = ANGEL PARK - CHARLESTON BOULEVARD									
107	KM	FACILITY # = APCB 0064, 0080									
108	KM	LINING = RCB									
109	RD	2338 0.0167 0.015	0	TRAP	7	0					

Page 2

INT.OUT

110 KK SW17
111 BA 0.356
112 PB 3.30
113 LS 0 87.8
114 UD 0.271
*

115 KK CSW17
116 KM COMBINE RSW11 AND SW17
117 HC 2
*

118 KK RCSW17
119 KM ROUTE CSW17 TO CSW18
120 KM FACILITY = ANGEL PARK - CHARLESTON BOULEVARD
121 KM FACILITY # = APCB 0000,0001,0019,0050
122 KM LINING = RCB
123 RD 3600 0.014 0.015 0 TRAP 11 0
*

124 KK SW18
125 BA 0.405
126 PB 3.27
127 LS 0 86.8
128 UD 0.271
*

129 KK CSW18
130 KM COMBINE RCSW17 AND SW18
131 HC 2
*

1

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

132 KK RCSW18
133 KM ROUTE CSW18 TO C12A
134 KM FACILITY = ANGEL PARK SOUTH
135 KM FACILITY # = APSO 0254,0255,0258,0345,0346; APCB 0000
136 KM NATURAL WASH
137 KM LENGTH = 5,200
138 KM SLOPE = 1.4%
139 KM N = 0.040
140 KM HYDRAULIC RADIUS = 1.5
141 KM VELOCITY = 9.2
142 RM 2 0.157 0.15
*

143 KK 12A
144 BA 0.392
145 PB 3.20
146 LS 0 91.2
147 UD 0.264
*

148 KK C12A
149 KM COMBINE 12A AND RCSW18
150 HC 2
*

151 KK RC12A
152 KM ROUTE THRU 12B
153 KM FACILITY = ANGEL PARK SOUTH
154 KM FACILITY # = APSO 0204, 0205
155 KM NATURAL WASH
156 KM LENGTH = 2,600
157 KM SLOPE = 3.5%
158 KM N = 0.040
159 KM HYDRAULIC RADIUS = 1.5
160 KM VELOCITY = 14.5
161 RM 1 0.05 0.15
*

162 KK 12B
163 BA 0.260
164 PB 3.13
165 LS 0 91.0
166 UD 0.233
*

167 KK C12B
168 KM COMBINE 12B AND RC12A
169 HC 2
*

1

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

Page 3

```

170      KK  57B-2A
171      KM  OFFSITE BASIN 57B-2A
172      PB   3.05
173      BA  0.0098
174      LS    0      87
175      UD   .159
      *

176      KK  57B-3F
177      KM  OFFSITE BASIN 57B-3F
178      PB   3.05
179      BA  0.0116
180      LS    0      87
181      UD   .142
      *

182      KK  57B-3E
183      KM  OFFSITE BASIN 57B-3E
184      PB   3.06
185      BA  0.0251
186      LS    0      87
187      UD   .214
      *

188      KK   ON9
189      KM  ONSITE BASIN ON9
190      PB   3.06
191      BA  0.0399
192      LS    0      82
193      UD   .232
      *

194      KK   CON9
195      KM  COMBINE C12B, 57B-2A, 57B-3F, 57B-3E AND ON9
196      HC    5
      *

197      KK   RCON9
198      KM  ROUTE CON9 TO CON10
199      KM  LENGTH SLOPE n-VALUE SHAPE WIDTH S-SLOPE
200      RD  1540 .030 .040 0 TRAP 50 2
      *

201      KK  57B-3G
202      KM  OFFSITE BASIN 57B-3G
203      PB   2.99
204      BA  0.0023
205      LS    0      87
206      UD   .072
      *

```

1

HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

207      KK  57B-2B
208      KM  OFFSITE BASIN 57B-2B
209      PB   2.99
210      BA  0.0047
211      LS    0      87
212      UD   .089
      *

213      KK  57B-2C
214      KM  OFFSITE BASIN 57B-2C
215      PB   2.96
216      BA  0.0027
217      LS    0      87
218      UD   .069
      *

219      KK   ON10
220      KM  ONSITE BASIN ON10
221      PB   2.98
222      BA  0.0177
223      LS    0      82
224      UD   .079
      *

225      KK   CON10
226      KM  COMBINE C57B-2A, 57B-3G, 57B-2B, 57B-2C AND ON10
227      HC    5
      *

228      KK  CCON10
229      KM  COMBINE CON8 AND CON10
230      HC    2

```

INT.OUT

*

231 KK RCON10
232 KM ROUTE CCON10 TO CON11
233 KM LENGTH SLOPE n-VALUE SHAPE WIDTH S-SLOPE
234 RD 510 .014 .040 0 TRAP 20 2
*

235 KK ON11
236 KM ONSITE BASIN ON11
237 PB 2.95
238 BA 0.0089
239 LS 0 82
240 UD .082
*

241 KK CON11
242 KM COMBINE CCON10 AND ON11
243 HC 2
*

1

HEC-1 INPUT

PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

244 KK 57B-2D
245 KM OFFSITE BASIN 57B-2D
246 PB 3.09
247 BA 0.0088
248 LS 0 91
249 UD .130
*

250 KK 57B-2E
251 KM OFFSITE BASIN 57B-2E
252 PB 3.08
253 BA 0.0227
254 LS 0 91
255 UD .102
*

256 KK C57B-2E
257 KM COMBINE 57B-2D AND 57B-2E
258 HC 2
*

259 KK 57B-2G1
260 KM OFFSITE BASIN 57B-2G1
261 PB 3.08
262 BA 0.0026
263 LS 0 87
264 UD .052
*

265 KK ON12
266 KM ONSITE BASIN ON12
267 PB 3.08
268 BA 0.0182
269 LS 0 82
270 UD .121
*

271 KK CON12
272 KM COMBINE C57B-2E, 57B-2G1 AND ON12
273 HC 3
*

274 KK 57B-2G2
275 KM OFFSITE BASIN 57B-2G2
276 PB 3.03
277 BA 0.0073
278 LS 0 87
279 UD .094
*

1

HEC-1 INPUT

PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

280 KK ON13
281 KM ONSITE BASIN ON13
282 PB 3.04
283 BA 0.0187
284 LS 0 82
285 UD .107
*

286 KK CON13
287 KM COMBINE CON12, 57B-2G2 AND ON13

Page 5

288 HC 3
*

289 KK 57B-2F
290 KM OFFSITE BASIN 57B-2F
291 PB 3.03
292 BA 0.0902
293 LS 0 91
294 UD .167
*

295 KK 57B-2H2
296 KM OFFSITE BASIN 57B-2H2
297 PB 3.04
298 BA 0.0156
299 LS 0 87
300 UD .182
*

301 KK ON14
302 KM ONSITE BASIN ON14
303 PB 3.00
304 BA 0.0054
305 LS 0 82
306 UD .193
*

307 KK CON14
308 KM COMBINE C57B-2F, 57B-2H2 AND ON14
309 HC 3
*

310 KK RCON14
311 KM ROUTE CON14 TO CON15
312 KM LENGTH SLOPE n-VALUE SHAPE WIDTH S-SLOPE
313 RD 2160 .032 .040 0 TRAP 20 2
*

314 KK 57B-2I
315 KM OFFSITE BASIN 57B-2I
316 PB 2.99
317 BA 0.0072
318 LS 0 87
319 UD .090
*

1

HEC-1 INPUT

PAGE 9

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

320 KK 57B-2H1
321 KM OFFSITE BASIN 57B-2H1
322 PB 3.01
323 BA 0.0291
324 LS 0 87
325 UD .296
*

326 KK ON15
327 KM ONSITE BASIN ON15
328 PB 2.98
329 BA 0.0351
330 LS 0 82
331 UD .114
*

332 KK CON15
333 KM COMBINE CON13, CON14, 57B-21, 57B-2H1 AND ON15
334 HC 5
*

335 KK ON16
336 KM ONSITE BASIN ON16
337 PB 2.97
338 BA 0.0180
339 LS 0 82
340 UD .088
*

341 KK CON16
342 KM COMBINE CON15 AND ON16
343 HC 2
*

344 KK RCON16
345 KM ROUTE CON16 TO CON17
346 KM LENGTH SLOPE n-VALUE SHAPE WIDTH S-SLOPE
347 RD 705 .036 .040 0 TRAP 20 2
*

INT.OUT

348 KK ON17
349 KM ONSITE BASIN ON17
350 PB 2.93
351 BA 0.0069
352 LS 0 82
353 UD .079
*

354 KK CON17
355 KM COMBINE CON16 CON11 AND ON17
356 HC 3
*

1

HEC-1 INPUT

PAGE 10

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

357 KK 13B-1
358 BA 0.249
359 PB 3.19
360 LS 0 91.6
361 UD 0.284
*

362 KK RC13B-1
363 KM ROUTE 13B-1 TO C13B-2
364 KM GRIFFITH PARK DRIVE AND HUALAPAI WAY
365 RD 3000 0.018 0.016 0 TRAP 0 50
*

366 KK 13B-2
367 BA 0.216
368 PB 3.14
369 LS 0 89.7
370 UD 0.231
*

371 KK C13B-2
372 KM COMBINE 13B-2 AND RC13B-1
373 KM HUALAPAI WAY AND LOCAL FACILITY
374 HC 2
*

375 KK RC13B-2
376 KM ROUTE C13B-2 TO CCPIC-A
377 KM LINING = GRASS
378 RD 4900 0.021 0.03 0 TRAP 40 6
*

379 KK 19A
380 BA 0.253
381 PB 3.25
382 LS 0 89.9
383 UD 0.351
*

384 KK R19A
385 KM ROUTE 19A TO C13A-1
386 KM UNNAMED ROAD
387 RD 4300 0.021 0.016 0 TRAP 0 50
*

388 KK 13A-1
389 BA 0.224
390 PB 3.19
391 LS 0 91.4
392 UD 0.302
*

1

HEC-1 INPUT

PAGE 11

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

393 KK C13A-1
394 KM COMBINE 13A-1 AND R19A
395 KM TOWN CENTER DRIVE AND SWALE
396 HC 2
*

397 KK RC13A-1
398 KM ROUTE C13A-1 TO C13A-2
399 KM NATURAL WASH
400 KM TRAVEL LENGTH = 2,800
401 KM SLOPE = 2.1%
402 KM N = 0.040
403 KM HYDRAULIC RADIUS = 1.5
404 KM VELOCITY = 11.4
405 RM 1 0.068 0.15

Page 7

*
 406 KK 13A-2
 407 BA 0.188
 408 PB 3.15
 409 LS 0 90.0
 410 UD 0.236
 *
 411 KK C13A-2
 412 KM COMBINE 13A-2 AND RC13A-1
 413 HC 2
 *
 414 KK RC13A-2
 415 KM ROUTE C13A-2 TO CPIC-C
 416 KM LINING = GRASS
 417 RD 5200 0.015 0.03 0 TRAP 40 4
 *
 418 KK PIC-C
 419 BA 0.243
 420 PB 3.08
 421 LS 0 90.4
 422 UD 0.373
 *
 423 KK CPIC-C
 424 KM COMBINE PIC-C AND RC13A-2
 425 HC 2
 *
 426 KK RCPIC-C
 427 KM ROUTE CPIC-C TO CPIC-A
 428 KM LINING = GRASS
 429 RD 2200 0.025 0.03 0 TRAP 40 4
 *

1

HEC-1 INPUT

PAGE 12

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

430 KK PIC-A
 431 BA 0.359
 432 PB 3.03
 433 LS 0 91.1
 434 UD 0.499
 *
 435 KK CPIC-A
 436 KM COMBINE RCPIC-C AND PIC-A
 437 HC 2
 *
 438 KK CCPIC-A
 439 KM COMBINE CPIC-A AND RC13B-2
 440 HC 2
 *
 441 KK ON18
 442 KM ONSITE BASIN ON18
 443 PB 2.95
 444 BA 0.0317
 445 LS 0 82
 446 UD .224
 *
 447 KK CON18
 448 KM COMBINE CCPIC-A AND ON18
 449 HC 2
 *
 450 KK 57B-1A
 451 KM OFFSITE BASIN 57B-1A
 452 PB 2.96
 453 BA 0.0443
 454 LS 0 85
 455 UD .179
 *
 456 KK 57B-1B
 457 KM OFFSITE BASIN 57B-1B
 458 PB 2.91
 459 BA 0.0301
 460 LS 0 93
 461 UD .150
 *
 462 KK ON19

INT.OUT

463 KM ONSITE BASIN ON19
464 PB 2.92
465 BA 0.0116
466 LS 0 82
467 UD .090
*

1

HEC-1 INPUT

PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

468 KK CON19
469 KM COMBINE CON18, 57B-1A, 57B-1B AND ON19
470 HC 4
*

471 KK CON20
472 KM COMBINE CON17 AND CON19
473 HC 2
*

474 KK ON1
475 KM OFFSITE BASIN ON1
476 PB 3.08
477 BA 0.0397
478 LS 0 82
479 UD .131
*

480 KK 57B-3A
481 KM ONSITE BASIN 57B-3A
482 PB 3.07
483 BA 0.0259
484 LS 0 85
485 UD .149
*

486 KK CON1
487 KM COMBINE 57B-3A AND ON1
488 HC 2
*

489 KK RCON1
490 KM ROUTE CON1 TO CON2
491 KM LENGTH SLOPE n-VALUE SHAPE WIDTH S-SLOPE
492 RD 3020 .027 .040 0 TRAP 50 3
*

493 KK 57B-3B
494 KM OFFSITE BASIN 57B-3B
495 PB 3.00
496 BA 0.0513
497 LS 0 85
498 UD .166
*

499 KK ON2
500 KM OFFSITE BASIN ON2
501 PB 3.00
502 BA 0.0273
503 LS 0 82
504 UD .159
*

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HEC-1 INPUT

PAGE 14

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

505 KK CON2
506 KM COMBINE CON1, 57B-3B AND ON2
507 HC 3
*

508 KK 57B-3D
509 KM OFFSITE BASIN 57B-3D
510 PB 2.99
511 BA 0.0184
512 LS 0 87
513 UD .160
*

514 KK ON3
515 KM ONSITE BASIN ON3
516 PB 2.96
517 BA 0.0040
518 LS 0 82
519 UD .056
*

520 KK CON3
 521 KM COMBINE CON2, 57B-3D AND ON3
 522 HC 3
 *

523 KK ON4
 524 KM OFFSITE BASIN ON4
 525 PB 2.94
 526 BA 0.0073
 527 LS 0 82
 528 UD .086
 *

529 KK CON4
 530 KM COMBINE CON3 AND ON4
 531 HC 2
 *

532 KK 57B-4A
 533 KM OFFSITE BASIN 57B-4A
 534 PB 2.93
 535 BA 0.0070
 536 LS 0 82
 537 UD .102
 *

538 KK CON21
 539 KM COMBINE 57B-4A AND CON4
 540 HC 2
 *

1

HEC-1 INPUT

PAGE 15

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

541 KK ON11A
 542 KM ONSITE BASIN ON11A
 543 PB 2.95
 544 BA 0.0141
 545 LS 0 82
 546 UD .084
 *

547 KK CON21
 548 KM COMBINE CON21 AND ON11A
 549 HC 2
 *

550 KK ON21
 551 KM ONSITE BASIN ON21
 552 PB 2.91
 553 BA 0.0259
 554 LS 0 82
 555 UD .146
 *

556 KK CON22
 557 KM COMBINE CON21 AND ON21
 558 HC 2
 *

559 KK 57B-1C
 560 KM OFFSITE BASIN 57B-1C
 561 PB 2.89
 562 BA 0.0009
 563 LS 0 96
 564 UD .065
 *

565 KK ON20
 566 KM ONSITE BASIN ON20
 567 PB 2.89
 568 BA 0.0038
 569 LS 0 82
 570 UD .054
 *

571 KK CON23
 572 KM COMBINE CON20, CON22, 57B-1C AND ON20
 573 HC 4
 *

574 KK 57B-4B
 575 KM OFFSITE BASIN 57B-4B
 576 PB 2.91
 577 BA 0.0110
 578 LS 0 96
 579 UD .071
 *

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
580	KK 57B-4C
581	KM OFFSITE BASIN 57B-4C
582	PB 2.90
583	BA 0.0122
584	LS 0 96
585	UD .118
	*
586	KK C57B-4C
587	KM COMBINE 57B-4B AND 57B-4C
588	HC 2
	*
589	KK DON4
590	KM ONSITE BASIN DON4
591	PB 2.88
592	BA 0.0272
593	LS 0 95
594	UD .198
	*
595	KK CON24
596	KM COMBINE CON23, C57B-4C AND DON4
597	HC 3
	*
598	KK 57B-1
599	KM OFFSITE BASIN 57B-1
600	BA 0.0485
601	PB 2.89
602	LS 0 93.7
603	UD 0.173
	*
604	KK 57B-3
605	KM OFFSITE BASIN 57B-3
606	BA 0.0481
607	PB 3.06
608	LS 0 89.3
609	UD 0.256
	*
610	KK 57B-4
611	KM OFFSITE BASIN 57B-4
612	BA 0.1293
613	PB 2.91
614	LS 0 93.8
615	UD 0.202
	*

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
616	KK C57B-4
617	KM COMBINE 57B-3 AND 57B-4
618	HC 2
	*
619	KK PIC-B
620	BA 0.441
621	PB 2.98
622	LS 0 91.1
623	UD 0.471
	*
624	KK RPIC-B
625	KM ROUTE PIC-B TO CC57B-4
626	KM FACILITY = ANGEL PARK - PECCOLE 1
627	KM FACILITY # = APP1 0000
628	KM LINING = RCP
629	RD 2982 0.024 0.013 0 CIRC 6
	*
630	KK CC57B-4
631	KM COMBINE CON24, C57B-1, C57B-4, PIC-B
632	HC 4
	*
633	ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT

LINE

(V) ROUTING

(--->) DIVERSION OR PUMP FLOW

NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW	INT.OUT
54	ON5		
	.		
	.		
68	57B-3C		
	.		
	.		
74		ON6	
	.		
	.		
80	CON6.....		
	.		
	.		
83	CCON6.....		
	V		
	V		
86	RCCON6		
	.		
	.		
90	ON8		
	.		
	.		
96	CON8.....		
	.		
	.		
99	SW11		
	V		
	V		
104	RSW11		
	.		
	.		
110		SW17	
	.		
	.		
115	CSW17.....		
	V		
	V		
118	RCSW17		
	.		
	.		
124		SW18	
	.		
	.		
129	CSW18.....		
	V		
	V		
132	RCSW18		
	.		
	.		
143		12A	
	.		
	.		
148	C12A.....		
	V		
	V		
151	RC12A		
	.		
	.		
162		12B	
	.		
	.		
167	C12B.....		
	.		
	.		
170		57B-2A	
	.		
	.		
176		57B-3F	
	.		
	.		
182		57B-3E	
	.		
	.		
188			ON9
	.		
	.		
194	CON9.....		
	V		
	V		
197	RCON9		
	.		
	.		
201	57B-3G		
	.		
	.		
207		57B-2B	
	.		
	.		

213	57B-2C	INT.OUT
	
219	ON10

225	.	CON10			
	.	.				
228	CCON10				
	V					
	V					
231	RCCON10					
	.					
235	.	ON11				
	.	.				
241	CON11				
	.					
244	.	57B-2D				
	.	.				
250	.	.	57B-2E			
	.	.	.			
256	.	C57B-2E			
	.	.				
259	.	.	57B-2G1			
	.	.	.			
265	.	.	.	ON12		
		
271	.	CON12			
	.	.				
274	.	.	57B-2G2			
	.	.	.			
280	.	.	.	ON13		
		
286	.	CON13			
	.	.				
289	.	.	57B-2F			
	.	.	.			
295	.	.	.	57B-2H2		
		
301	ON14	
	
307	.	.	CON14		
	.	.	V			
	.	.	V			
310	.	.	RCON14			
	.	.	.			
314	.	.	.	57B-2I		
		
320	57B-2H1	
	
326	ON15

332	.	CON15			
	.	.				
335	.	.	ON16			
	.	.	.			
341	.	CON16			
	.	V				
	.	V				
344	.	RCON16				
	.	.				
348	.	.	ON17			
	.	.	.			
354	CON17				
	.					

```

357 .      13B-1
    .      V
    .      V
362 .      RC13B-1
    .      .
    .      .
366 .      .      13B-2
    .      .
    .      .
371 .      C13B-2.....
    .      V
    .      V
375 .      RC13B-2
    .      .
    .      .
379 .      .      19A
    .      .      V
    .      .      V
384 .      .      R19A
    .      .
    .      .
388 .      .      .      13A-1
    .      .
    .      .
393 .      .      C13A-1.....
    .      .      V
    .      .      V
397 .      .      RC13A-1
    .      .
    .      .
406 .      .      .      13A-2
    .      .
    .      .
411 .      .      C13A-2.....
    .      .      V
    .      .      V
414 .      .      RC13A-2
    .      .
    .      .
418 .      .      .      PIC-C
    .      .
    .      .
423 .      .      CPIC-C.....
    .      .      V
    .      .      V
426 .      .      RCPIC-C
    .      .
    .      .
430 .      .      .      PIC-A
    .      .
    .      .
435 .      .      CPIC-A.....
    .      .
    .      .
438 .      CCPIC-A.....
    .      .
    .      .
441 .      .      ON18
    .      .
    .      .
447 .      CON18.....
    .      .
    .      .
450 .      .      57B-1A
    .      .
    .      .
456 .      .      .      57B-1B
    .      .
    .      .
462 .      .      .      .      ON19
    .      .      .
    .      .
468 .      CON19.....
    .      .
    .      .
471 .      CON20.....
    .      .
    .      .
474 .      .      ON1
    .      .
    .      .
480 .      .      .      57B-3A
    .      .
    .      .
486 .      .      CON1.....
    .      .      V
    .      .      V
489 .      .      RCON1

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.      .
493    .      .      57B-3B
.      .      .
499    .      .      .      ON2
.      .      .
505    .      CON2.....
.      .
508    .      .      57B-3D
.      .      .
514    .      .      .      ON3
.      .      .
520    .      CON3.....
.      .
523    .      .      ON4
.      .
529    .      CON4.....
.      .
532    .      .      57B-4A
.      .      .
538    .      CON21.....
.      .
541    .      .      ON11A
.      .
547    .      CON21.....
.      .
550    .      .      ON21
.      .
556    .      CON22.....
.      .
559    .      .      57B-1C
.      .      .
565    .      .      .      ON20
.      .      .
571    CON23.....
.      .
574    .      57B-4B
.      .
580    .      .      57B-4C
.      .
586    .      C57B-4C.....
.      .
589    .      .      DON4
.      .
595    CON24.....
.      .
598    .      57B-1
.      .
604    .      .      57B-3
.      .      .
610    .      .      .      57B-4
.      .      .
616    .      .      C57B-4.....
.      .
619    .      .      .      PIC-B
.      .      .      V
624    .      .      .      RPIC-B
.      .      .
630    CC57B-4.....

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION


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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 21JUN18 TIME 08:10:45
*
*****

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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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* .....:
* :
* : THE 435 :
* :
* : INTERIM CONDITIONS :
* : .....:
* : RETURN PERIOD _ _ _ 100 & 10 -YEAR :
* : DISTRIBUTION _ _ _ 6-HOUR SDN3 :
* : PROJECT NO _ _ _ 840.050 :
* : FILENAME _ _ _ INT.H1 :
* : DATE MODELED _ _ _ 6/08/18 :
* : MODELED BY _ _ _ NB :
* : .....:
* :
* : .....:
* : .....:
*****

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REFERENCED HYDROLOGIC MODELS:
 2013 LAS VEGAS VALLEY FLOOD CONTROL MASTER PLAN UPDATE
 CITY OF LAS VEGAS CITY WIDE HYDROLOGY ANALYSIS (PBS&J 1997)
 CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2008 MASTER PLAN UPDATE
 GOWAN WATERSHED (ALL)
 RECOMMENDED DRAINAGE SYSTEM WITH ULTIMATE DEVELOPMENT
 INPUT FILE = ALLGOW3.DAT
 INPUT FILE DATE = MAY 5, 2008
 DESIGN STORM = 100-YEAR 6-HR STORM
 STORM DISTRIBUTION = SDN #3
 MODELED BY PBS&J (MICHELE L. D'ALESSANDRO, E.I., CFM)
 CHECKED BY PBS&J (HARSHAL B. DESAI, P.E., CFM)
 STORM CENTERING = FULL WATERSHED
 JR CARDS CONTAIN DARFS BASED ON THE FOLLOWING VALUES:

AREA	DARF
SQ. MI.	
0-0.5	0.99
0.5-1	0.975
1-2	0.95
2-3	0.925
3-4	0.915
4-5	0.908
5-6	0.903
6-7	0.895
10yr	0.570

JR CARD RATIOS REPRESENT DEPTH-AREA REDUCTION FACTORS (DARF'S)

100-YEAR, 6-HOUR STORM, SDN3

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51 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

IT         HYDROGRAPH TIME DATA
          NMIN      5  MINUTES IN COMPUTATION INTERVAL
          IDATE      1  0  STARTING DATE
          ITIME      0000 STARTING TIME
          NQ        650 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE     3  0  ENDING DATE
          NDTIME     0605 ENDING TIME
          ICENT      19  CENTURY MARK

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE 54.08 HOURS

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

INT.OUT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.99 .98 .95 .93 .92 .91 .90 .89 .57

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN		RATIOS APPLIED TO PRECIPITATION								
					RATIO 1 .99	RATIO 2 .98	RATIO 3 .95	RATIO 4 .93	RATIO 5 .92	RATIO 6 .91	RATIO 7 .90	RATIO 8 .89	RATIO 9 .57
HYDROGRAPH AT +	ON5	.01	1	FLOW TIME	18. 3.50	18. 3.58	17. 3.58	16. 3.58	16. 3.58	16. 3.58	16. 3.58	16. 3.58	7. 3.58
HYDROGRAPH AT +	57B-3C	.01	1	FLOW TIME	11. 3.58	10. 3.58	10. 3.58	10. 3.58	9. 3.58	9. 3.58	9. 3.58	9. 3.58	4. 3.58
HYDROGRAPH AT +	ON6	.00	1	FLOW TIME	8. 3.50	8. 3.50	8. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	4. 3.50
2 COMBINED AT +	CON6	.01	1	FLOW TIME	18. 3.50	18. 3.50	17. 3.50	16. 3.50	16. 3.50	16. 3.50	16. 3.50	16. 3.50	8. 3.50
2 COMBINED AT +	CCON6	.03	1	FLOW TIME	36. 3.50	36. 3.50	34. 3.50	33. 3.50	32. 3.50	32. 3.50	32. 3.50	31. 3.50	14. 3.50
ROUTED TO +	RCCON6	.03	1	FLOW TIME	34. 3.67	33. 3.67	32. 3.67	31. 3.67	30. 3.67	30. 3.67	30. 3.67	29. 3.67	14. 3.67
HYDROGRAPH AT +	ON8	.02	1	FLOW TIME	27. 3.50	26. 3.50	25. 3.50	24. 3.50	23. 3.50	23. 3.50	23. 3.50	22. 3.50	9. 3.50
2 COMBINED AT +	CON8	.04	1	FLOW TIME	54. 3.58	53. 3.58	50. 3.58	48. 3.58	47. 3.58	47. 3.58	46. 3.58	46. 3.58	19. 3.67
HYDROGRAPH AT +	SW11	.59	1	FLOW TIME	759. 3.75	743. 3.75	717. 3.75	691. 3.75	680. 3.75	673. 3.75	668. 3.75	660. 3.75	330. 3.75
ROUTED TO +	RSW11	.59	1	FLOW TIME	754. 3.75	738. 3.75	712. 3.75	686. 3.75	676. 3.75	668. 3.75	663. 3.75	655. 3.75	325. 3.75
HYDROGRAPH AT +	SW17	.36	1	FLOW TIME	479. 3.67	469. 3.67	452. 3.67	436. 3.67	429. 3.67	424. 3.67	421. 3.67	416. 3.67	205. 3.67
2 COMBINED AT +	CSW17	.94	1	FLOW TIME	1221. 3.75	1196. 3.75	1153. 3.75	1111. 3.75	1095. 3.75	1083. 3.75	1075. 3.75	1061. 3.75	530. 3.75
ROUTED TO +	RCSW17	.94	1	FLOW TIME	1211. 3.75	1186. 3.75	1143. 3.75	1101. 3.75	1083. 3.75	1073. 3.75	1063. 3.75	1051. 3.75	521. 3.75
HYDROGRAPH AT +	SW18	.41	1	FLOW TIME	519. 3.67	507. 3.67	489. 3.67	470. 3.67	463. 3.67	457. 3.67	454. 3.67	448. 3.67	215. 3.75
2 COMBINED AT +	CSW18	1.35	1	FLOW TIME	1718. 3.75	1682. 3.75	1622. 3.75	1562. 3.75	1537. 3.75	1521. 3.75	1508. 3.75	1490. 3.75	736. 3.75
ROUTED TO +	RCSW18	1.35	1	FLOW TIME	1610. 3.92	1576. 3.92	1520. 3.92	1464. 3.92	1441. 3.92	1426. 3.92	1414. 3.92	1397. 3.92	690. 3.92
HYDROGRAPH AT +	12A	.39	1	FLOW TIME	576. 3.67	565. 3.67	547. 3.67	529. 3.67	521. 3.67	516. 3.67	513. 3.67	507. 3.67	272. 3.67
2 COMBINED AT +	C12A	1.74	1	FLOW TIME	2046. 3.83	2003. 3.83	1932. 3.83	1861. 3.83	1832. 3.83	1813. 3.83	1798. 3.83	1776. 3.83	881. 3.83

Page 17

INT.OUT													
ROUTED TO													
+	RC12A	1.74	1	FLOW TIME	2025. 3.92	1983. 3.92	1913. 3.92	1843. 3.92	1815. 3.92	1796. 3.92	1782. 3.92	1760. 3.92	880. 3.92
HYDROGRAPH AT													
+	12B	.26	1	FLOW TIME	387. 3.67	380. 3.67	367. 3.67	355. 3.67	350. 3.67	347. 3.67	344. 3.67	340. 3.67	182. 3.67
2 COMBINED AT													
+	C12B	2.00	1	FLOW TIME	2259. 3.83	2212. 3.83	2134. 3.83	2056. 3.83	2024. 3.83	2002. 3.83	1987. 3.83	1962. 3.83	990. 3.92
HYDROGRAPH AT													
+	57B-2A	.01	1	FLOW TIME	14. 3.58	14. 3.58	13. 3.58	13. 3.58	13. 3.58	13. 3.58	12. 3.58	12. 3.58	6. 3.58
HYDROGRAPH AT													
+	57B-3F	.01	1	FLOW TIME	17. 3.58	17. 3.58	16. 3.58	16. 3.58	15. 3.58	15. 3.58	15. 3.58	15. 3.58	7. 3.58
HYDROGRAPH AT													
+	57B-3E	.03	1	FLOW TIME	32. 3.67	31. 3.67	30. 3.67	29. 3.67	29. 3.67	28. 3.67	28. 3.67	28. 3.67	13. 3.67
HYDROGRAPH AT													
+	ON9	.04	1	FLOW TIME	41. 3.67	40. 3.67	38. 3.67	36. 3.67	36. 3.67	35. 3.67	35. 3.67	34. 3.67	14. 3.67
5 COMBINED AT													
+	CON9	2.09	1	FLOW TIME	2330. 3.83	2281. 3.83	2200. 3.83	2120. 3.83	2087. 3.83	2064. 3.83	2048. 3.83	2023. 3.83	1012. 3.92
ROUTED TO													
+	RCON9	2.09	1	FLOW TIME	2307. 3.92	2259. 3.92	2181. 3.92	2103. 3.92	2071. 3.92	2048. 3.92	2032. 3.92	2007. 3.92	1012. 3.92
HYDROGRAPH AT													
+	57B-3G	.00	1	FLOW TIME	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	3. 3.50	3. 3.50	2. 3.50
HYDROGRAPH AT													
+	57B-2B	.00	1	FLOW TIME	8. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	3. 3.50
HYDROGRAPH AT													
+	57B-2C	.00	1	FLOW TIME	5. 3.50	5. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	2. 3.50
HYDROGRAPH AT													
+	ON10	.02	1	FLOW TIME	24. 3.50	23. 3.50	22. 3.50	21. 3.50	21. 3.50	21. 3.50	21. 3.50	20. 3.50	8. 3.50
5 COMBINED AT													
+	CON10	2.12	1	FLOW TIME	2314. 3.92	2266. 3.92	2188. 3.92	2110. 3.92	2077. 3.92	2055. 3.92	2039. 3.92	2014. 3.92	1015. 3.92
2 COMBINED AT													
+	CCON10	2.16	1	FLOW TIME	2335. 3.92	2286. 3.92	2208. 3.92	2128. 3.92	2096. 3.92	2073. 3.92	2057. 3.92	2032. 3.92	1025. 3.92
ROUTED TO													
+	RCCON10	2.16	1	FLOW TIME	2333. 3.92	2285. 3.92	2205. 3.92	2126. 3.92	2094. 3.92	2070. 3.92	2055. 3.92	2030. 3.92	1020. 3.92
HYDROGRAPH AT													
+	ON11	.01	1	FLOW TIME	12. 3.50	11. 3.50	11. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	4. 3.50
2 COMBINED AT													
+	CON11	2.17	1	FLOW TIME	2335. 3.92	2287. 3.92	2208. 3.92	2128. 3.92	2096. 3.92	2072. 3.92	2057. 3.92	2032. 3.92	1021. 3.92
HYDROGRAPH AT													
+	57B-2D	.01	1	FLOW TIME	16. 3.58	15. 3.58	15. 3.58	14. 3.58	14. 3.58	14. 3.58	14. 3.58	14. 3.58	7. 3.58
HYDROGRAPH AT													
+	57B-2E	.02	1	FLOW TIME	42. 3.50	41. 3.50	40. 3.50	38. 3.50	38. 3.50	37. 3.50	37. 3.50	37. 3.50	19. 3.50
2 COMBINED AT													
+	C57B-2E	.03	1	FLOW TIME	56. 3.50	55. 3.50	53. 3.50	52. 3.50	51. 3.50	50. 3.50	50. 3.50	49. 3.50	26. 3.50
HYDROGRAPH AT													
+	57B-2G1	.00	1	FLOW TIME	5. 3.50	5. 3.50	5. 3.50	5. 3.50	5. 3.50	4. 3.50	4. 3.50	4. 3.50	2. 3.50

INT.OUT												
HYDROGRAPH AT												
+	ON12	.02	1	FLOW TIME	23. 3.58	23. 3.58	22. 3.58	21. 3.58	20. 3.58	20. 3.58	20. 3.58	8. 3.58
3 COMBINED AT												
+	CON12	.05	1	FLOW TIME	83. 3.50	81. 3.50	78. 3.50	75. 3.50	74. 3.50	73. 3.50	73. 3.50	36. 3.58
HYDROGRAPH AT												
+	57B-2G2	.01	1	FLOW TIME	12. 3.50	11. 3.50	11. 3.50	11. 3.50	10. 3.50	10. 3.50	10. 3.50	5. 3.50
HYDROGRAPH AT												
+	ON13	.02	1	FLOW TIME	23. 3.58	23. 3.58	22. 3.58	21. 3.58	21. 3.58	20. 3.58	20. 3.58	8. 3.58
3 COMBINED AT												
+	CON13	.08	1	FLOW TIME	118. 3.50	115. 3.50	111. 3.50	107. 3.50	105. 3.50	104. 3.50	103. 3.50	49. 3.58
HYDROGRAPH AT												
+	57B-2F	.09	1	FLOW TIME	147. 3.58	145. 3.58	140. 3.58	135. 3.58	133. 3.58	132. 3.58	131. 3.58	69. 3.58
HYDROGRAPH AT												
+	57B-2H2	.02	1	FLOW TIME	21. 3.58	21. 3.58	20. 3.58	19. 3.58	19. 3.58	19. 3.58	19. 3.58	9. 3.58
HYDROGRAPH AT												
+	ON14	.01	1	FLOW TIME	6. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	2. 3.67
3 COMBINED AT												
+	CON14	.11	1	FLOW TIME	174. 3.58	171. 3.58	165. 3.58	159. 3.58	157. 3.58	155. 3.58	154. 3.58	79. 3.58
ROUTED TO												
+	RCON14	.11	1	FLOW TIME	166. 3.67	163. 3.67	158. 3.67	156. 3.67	153. 3.67	152. 3.67	151. 3.67	79. 3.67
HYDROGRAPH AT												
+	57B-2I	.01	1	FLOW TIME	12. 3.50	11. 3.50	11. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	5. 3.50
HYDROGRAPH AT												
+	57B-2H1	.03	1	FLOW TIME	32. 3.75	31. 3.75	30. 3.75	29. 3.75	29. 3.75	28. 3.75	28. 3.75	13. 3.75
HYDROGRAPH AT												
+	ON15	.04	1	FLOW TIME	42. 3.58	41. 3.58	40. 3.58	38. 3.58	37. 3.58	37. 3.58	36. 3.58	15. 3.58
5 COMBINED AT												
+	CON15	.26	1	FLOW TIME	346. 3.58	338. 3.58	326. 3.58	314. 3.58	309. 3.58	306. 3.58	303. 3.58	142. 3.58
HYDROGRAPH AT												
+	ON16	.02	1	FLOW TIME	23. 3.50	23. 3.50	22. 3.50	21. 3.50	20. 3.50	20. 3.50	20. 3.50	8. 3.50
2 COMBINED AT												
+	CON16	.28	1	FLOW TIME	367. 3.58	359. 3.58	345. 3.58	333. 3.58	327. 3.58	324. 3.58	321. 3.58	150. 3.58
ROUTED TO												
+	RCON16	.28	1	FLOW TIME	359. 3.58	351. 3.58	338. 3.58	326. 3.58	320. 3.58	316. 3.58	313. 3.58	147. 3.67
HYDROGRAPH AT												
+	ON17	.01	1	FLOW TIME	9. 3.50	9. 3.50	8. 3.50	8. 3.50	8. 3.50	8. 3.50	8. 3.50	3. 3.50
3 COMBINED AT												
+	CON17	2.45	1	FLOW TIME	2550. 3.83	2496. 3.83	2408. 3.83	2319. 3.83	2284. 3.83	2258. 3.83	2240. 3.83	1108. 3.92
HYDROGRAPH AT												
+	13B-1	.25	1	FLOW TIME	354. 3.67	347. 3.67	336. 3.67	325. 3.67	321. 3.67	318. 3.67	315. 3.67	169. 3.75
ROUTED TO												
+	RC13B-1	.25	1	FLOW TIME	354. 3.75	347. 3.75	336. 3.75	324. 3.75	320. 3.75	317. 3.75	314. 3.83	171. 3.83
HYDROGRAPH AT												
+	13B-2	.22	1	FLOW TIME	310. 3.67	304. 3.67	294. 3.67	283. 3.67	279. 3.67	277. 3.67	274. 3.67	140. 3.67
2 COMBINED AT												

+	C13B-2	.47	1	FLOW TIME	634.3.75	622.3.75	INT.OUT 602.3.75	581.3.75	573.3.75	567.3.75	563.3.75	557.3.75	294.3.75
ROUTED TO													
+	RC13B-2	.47	1	FLOW TIME	641.3.83	628.3.83	607.3.83	586.3.83	578.3.83	572.3.83	568.3.83	561.3.83	295.3.92
HYDROGRAPH AT													
+	19A	.25	1	FLOW TIME	318.3.75	312.3.75	301.3.75	291.3.75	287.3.75	284.3.75	282.3.75	278.3.75	144.3.75
ROUTED TO													
+	R19A	.25	1	FLOW TIME	319.3.92	313.3.92	302.3.92	292.3.92	288.3.92	285.3.92	283.3.92	280.3.92	146.3.92
HYDROGRAPH AT													
+	13A-1	.22	1	FLOW TIME	308.3.75	303.3.75	293.3.75	283.3.75	279.3.75	277.3.75	275.3.75	272.3.75	147.3.75
2 COMBINED AT													
+	C13A-1	.48	1	FLOW TIME	595.3.83	583.3.83	564.3.83	545.3.83	537.3.83	532.3.83	528.3.83	522.3.83	273.3.83
ROUTED TO													
+	RC13A-1	.48	1	FLOW TIME	581.3.92	569.3.92	551.3.92	532.3.92	524.3.92	519.3.92	515.3.92	509.3.92	268.3.92
HYDROGRAPH AT													
+	13A-2	.19	1	FLOW TIME	272.3.67	267.3.67	258.3.67	249.3.67	246.3.67	243.3.67	241.3.67	238.3.67	124.3.67
2 COMBINED AT													
+	C13A-2	.66	1	FLOW TIME	782.3.83	766.3.83	740.3.83	715.3.83	704.3.83	697.3.83	692.3.83	684.3.83	354.3.83
ROUTED TO													
+	RC13A-2	.66	1	FLOW TIME	781.3.92	765.3.92	738.3.92	712.3.92	702.3.92	694.3.92	689.3.92	681.3.92	354.4.00
HYDROGRAPH AT													
+	PIC-C	.24	1	FLOW TIME	280.3.83	274.3.83	265.3.83	256.3.83	252.3.83	250.3.83	248.3.83	245.3.83	129.3.83
2 COMBINED AT													
+	CPIC-C	.91	1	FLOW TIME	1041.3.92	1020.3.92	985.3.92	951.3.92	937.3.92	927.3.92	920.3.92	909.3.92	462.3.92
ROUTED TO													
+	RCPIC-C	.91	1	FLOW TIME	1030.3.92	1009.3.92	975.3.92	940.3.92	922.3.92	915.3.92	908.3.92	896.3.92	461.4.00
HYDROGRAPH AT													
+	PIC-A	.36	1	FLOW TIME	356.3.92	349.3.92	338.3.92	326.3.92	322.3.92	318.3.92	316.3.92	312.3.92	165.3.92
2 COMBINED AT													
+	CPIC-A	1.27	1	FLOW TIME	1386.3.92	1359.3.92	1313.3.92	1266.3.92	1243.3.92	1233.3.92	1224.3.92	1208.3.92	625.4.00
2 COMBINED AT													
+	CCPIC-A	1.73	1	FLOW TIME	1997.3.92	1959.3.92	1895.3.92	1830.3.92	1800.3.92	1785.3.92	1772.3.92	1750.3.92	900.4.00
HYDROGRAPH AT													
+	ON18	.03	1	FLOW TIME	31.3.67	30.3.67	29.3.67	27.3.67	27.3.67	26.3.67	26.3.67	26.3.67	10.3.67
2 COMBINED AT													
+	CON18	1.76	1	FLOW TIME	2015.3.92	1977.3.92	1912.3.92	1846.3.92	1816.3.92	1801.3.92	1788.3.92	1765.3.92	906.4.00
HYDROGRAPH AT													
+	57B-1A	.04	1	FLOW TIME	54.3.58	53.3.58	51.3.58	48.3.58	48.3.58	47.3.58	47.3.58	46.3.58	20.3.58
HYDROGRAPH AT													
+	57B-1B	.03	1	FLOW TIME	51.3.58	50.3.58	49.3.58	47.3.58	47.3.58	46.3.58	46.3.58	45.3.58	25.3.58
HYDROGRAPH AT													
+	ON19	.01	1	FLOW TIME	14.3.50	14.3.50	13.3.50	13.3.50	13.3.50	12.3.50	12.3.50	12.3.50	5.3.50
4 COMBINED AT													
+	CON19	1.85	1	FLOW TIME	2060.3.92	2020.3.92	1954.3.92	1887.3.92	1856.3.92	1840.3.92	1827.3.92	1804.3.92	923.3.92
2 COMBINED AT													
+	CON20	4.30	1	FLOW	4576.	4485.	4334.	4182.	4116.	4076.	4045.	3995.	2032.

				INT.OUT									
TIME				3.92	3.92	3.92	3.92	3.92	3.92	3.92	3.92	3.92	3.92
HYDROGRAPH AT													
+	ON1	.04	1	FLOW	50.	49.	47.	45.	44.	43.	43.	42.	18.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
HYDROGRAPH AT													
+	57B-3A	.03	1	FLOW	36.	35.	34.	32.	32.	31.	31.	31.	14.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
2 COMBINED AT													
+	CON1	.07	1	FLOW	86.	84.	80.	77.	76.	75.	74.	73.	32.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
ROUTED TO													
+	RCON1	.07	1	FLOW	86.	84.	80.	77.	76.	75.	74.	73.	30.
				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.83
HYDROGRAPH AT													
+	57B-3B	.05	1	FLOW	66.	65.	62.	59.	58.	58.	57.	56.	25.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
HYDROGRAPH AT													
+	ON2	.03	1	FLOW	31.	30.	29.	28.	27.	27.	27.	26.	11.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
3 COMBINED AT													
+	CON2	.14	1	FLOW	164.	160.	153.	145.	143.	141.	139.	137.	55.
				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75
HYDROGRAPH AT													
+	57B-3D	.02	1	FLOW	26.	25.	24.	23.	23.	23.	23.	22.	11.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
HYDROGRAPH AT													
+	ON3	.00	1	FLOW	6.	6.	6.	5.	5.	5.	5.	5.	2.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
3 COMBINED AT													
+	CON3	.17	1	FLOW	189.	185.	177.	169.	165.	163.	161.	159.	64.
				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75
HYDROGRAPH AT													
+	ON4	.01	1	FLOW	9.	9.	9.	8.	8.	8.	8.	8.	3.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
2 COMBINED AT													
+	CON4	.17	1	FLOW	195.	190.	182.	173.	170.	168.	166.	164.	66.
				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75
HYDROGRAPH AT													
+	57B-4A	.01	1	FLOW	8.	8.	8.	7.	7.	7.	7.	7.	3.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.58
2 COMBINED AT													
+	CON21	.18	1	FLOW	201.	196.	187.	179.	175.	173.	171.	168.	67.
				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75
HYDROGRAPH AT													
+	ON11A	.01	1	FLOW	18.	18.	17.	16.	16.	16.	16.	15.	6.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
2 COMBINED AT													
+	CON21	.20	1	FLOW	211.	206.	197.	188.	185.	182.	180.	178.	71.
				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75
HYDROGRAPH AT													
+	ON21	.03	1	FLOW	29.	28.	27.	26.	25.	25.	25.	24.	10.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
2 COMBINED AT													
+	CON22	.22	1	FLOW	236.	230.	220.	210.	206.	204.	202.	199.	78.
				TIME	3.58	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75
HYDROGRAPH AT													
+	57B-1C	.00	1	FLOW	2.	2.	2.	2.	2.	2.	2.	2.	1.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
HYDROGRAPH AT													
+	ON20	.00	1	FLOW	6.	5.	5.	5.	5.	5.	5.	5.	2.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
4 COMBINED AT													
+	CON23	4.53	1	FLOW	4745.	4650.	4486.	4321.	4252.	4203.	4171.	4121.	2087.
				TIME	3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.92
HYDROGRAPH AT													
+	57B-4B	.01	1	FLOW	24.	24.	23.	22.	22.	22.	22.	22.	13.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50

INT.OUT

HYDROGRAPH AT													
+	57B-4C	.01	1	FLOW	23.	22.	22.	21.	21.	21.	21.	20.	12.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.58
2 COMBINED AT													
+	C57B-4C	.02	1	FLOW	47.	46.	45.	43.	43.	43.	42.	42.	25.
				TIME	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.50
HYDROGRAPH AT													
+	DON4	.03	1	FLOW	44.	43.	42.	41.	40.	40.	40.	39.	23.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
3 COMBINED AT													
+	CON24	4.58	1	FLOW	4787.	4690.	4525.	4359.	4290.	4241.	4208.	4158.	2103.
				TIME	3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.92
HYDROGRAPH AT													
+	57B-1	.05	1	FLOW	80.	79.	76.	74.	73.	72.	72.	71.	40.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
HYDROGRAPH AT													
+	57B-3	.05	1	FLOW	63.	62.	60.	58.	57.	56.	56.	55.	28.
				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67
HYDROGRAPH AT													
+	57B-4	.13	1	FLOW	202.	198.	192.	186.	184.	182.	181.	179.	101.
				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
2 COMBINED AT													
+	C57B-4	.18	1	FLOW	259.	254.	246.	238.	235.	233.	232.	229.	127.
				TIME	3.58	3.58	3.67	3.67	3.67	3.67	3.67	3.67	3.67
HYDROGRAPH AT													
+	PIC-B	.44	1	FLOW	442.	433.	419.	405.	399.	395.	392.	388.	205.
				TIME	3.92	3.92	3.92	3.92	3.92	3.92	3.92	3.92	3.92
ROUTED TO													
+	RPIC-B	.44	1	FLOW	439.	431.	416.	402.	396.	392.	390.	385.	202.
				TIME	3.92	3.92	3.92	3.92	3.92	3.92	3.92	3.92	3.92
4 COMBINED AT													
+	CC57B-4	5.25	1	FLOW	5433.	5325.	5139.	4953.	4875.	4820.	4784.	4727.	2392.
				TIME	3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.92

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL			VOLUME
							PEAK	TIME TO PEAK		
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)		(IN)
FOR PLAN = 1	RATIO=	.00								
RCCON6	MANE	4.25	34.85	216.75	1.61	5.00	33.88	220.00		1.61

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2157E+01 EXCESS= .0000E+00 OUTFLOW= .2162E+01 BASIN STORAGE= .2734E-02 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00								
RCCON6	MANE	4.25	34.03	216.75	1.58	5.00	33.16	220.00		1.57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2106E+01 EXCESS= .0000E+00 OUTFLOW= .2111E+01 BASIN STORAGE= .2708E-02 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00								
RCCON6	MANE	4.25	32.67	216.75	1.51	5.00	31.96	220.00		1.51

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2022E+01 EXCESS= .0000E+00 OUTFLOW= .2026E+01 BASIN STORAGE= .2664E-02 PERCENT ERROR= -.3

FOR PLAN = 1	RATIO=	.00								
RCCON6	MANE	4.25	31.31	216.75	1.45	5.00	30.75	220.00		1.45

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1938E+01 EXCESS= .0000E+00 OUTFLOW= .1942E+01 BASIN STORAGE= .2619E-02 PERCENT ERROR= -.4

FOR PLAN = 1	RATIO=	.00								
RCCON6	MANE	4.25	30.77	216.75	1.43	5.00	30.27	220.00		1.42

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1905E+01 EXCESS= .0000E+00 OUTFLOW= .1909E+01 BASIN STORAGE= .2601E-02 PERCENT ERROR= -.4

		INT.OUT							
FOR PLAN = 1	RATIO=	.00							
RCCON6	MANE	4.25	30.39	216.75	1.41	5.00	29.93	220.00	1.41
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1881E+01 EXCESS= .0000E+00 OUTFLOW= .1886E+01 BASIN STORAGE= .2588E-02 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO=	.00							
RCCON6	MANE	4.25	30.11	216.75	1.40	5.00	29.69	220.00	1.39
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1865E+01 EXCESS= .0000E+00 OUTFLOW= .1869E+01 BASIN STORAGE= .2579E-02 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO=	.00							
RCCON6	MANE	4.25	29.68	216.75	1.38	5.00	29.30	220.00	1.37
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1838E+01 EXCESS= .0000E+00 OUTFLOW= .1842E+01 BASIN STORAGE= .2564E-02 PERCENT ERROR= -.4									
FOR PLAN = 1	RATIO=	.00							
RCCON6	MANE	3.75	14.36	221.25	.63	5.00	14.02	220.00	.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8405E+00 EXCESS= .0000E+00 OUTFLOW= .8424E+00 BASIN STORAGE= .2039E-02 PERCENT ERROR= -.5									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.02	755.16	226.24	2.08	5.00	753.82	225.00	2.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6522E+02 EXCESS= .0000E+00 OUTFLOW= .6522E+02 BASIN STORAGE= .1654E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.03	740.95	226.07	2.03	5.00	738.42	225.00	2.03
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6380E+02 EXCESS= .0000E+00 OUTFLOW= .6381E+02 BASIN STORAGE= .1696E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.05	714.15	226.19	1.96	5.00	712.14	225.00	1.96
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6145E+02 EXCESS= .0000E+00 OUTFLOW= .6145E+02 BASIN STORAGE= .1622E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.06	686.99	226.38	1.88	5.00	685.95	225.00	1.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5911E+02 EXCESS= .0000E+00 OUTFLOW= .5911E+02 BASIN STORAGE= .1763E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.07	677.33	225.62	1.85	5.00	675.73	225.00	1.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5818E+02 EXCESS= .0000E+00 OUTFLOW= .5818E+02 BASIN STORAGE= .1832E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.07	669.72	225.52	1.83	5.00	668.38	225.00	1.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5752E+02 EXCESS= .0000E+00 OUTFLOW= .5752E+02 BASIN STORAGE= .1613E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.08	665.29	226.22	1.82	5.00	663.31	225.00	1.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5706E+02 EXCESS= .0000E+00 OUTFLOW= .5706E+02 BASIN STORAGE= .1791E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.08	656.69	226.27	1.79	5.00	654.91	225.00	1.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5631E+02 EXCESS= .0000E+00 OUTFLOW= .5632E+02 BASIN STORAGE= .1761E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO=	.00							
RSW11	MANE	1.43	328.10	225.73	.88	5.00	324.89	225.00	.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2754E+02 EXCESS= .0000E+00 OUTFLOW= .2754E+02 BASIN STORAGE= .1787E-02 PERCENT ERROR= .0									

INT.OUT

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 1.65 1211.98 225.57 2.06 5.00 1210.68 225.00 2.06

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1040E+03 EXCESS= .0000E+00 OUTFLOW= .1040E+03 BASIN STORAGE= .3928E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 1.66 1187.90 225.78 2.02 5.00 1185.71 225.00 2.02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1018E+03 EXCESS= .0000E+00 OUTFLOW= .1018E+03 BASIN STORAGE= .3507E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 1.68 1144.91 225.68 1.94 5.00 1143.40 225.00 1.94

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9799E+02 EXCESS= .0000E+00 OUTFLOW= .9800E+02 BASIN STORAGE= .3522E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 1.71 1102.37 225.64 1.87 5.00 1101.22 225.00 1.87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9424E+02 EXCESS= .0000E+00 OUTFLOW= .9424E+02 BASIN STORAGE= .3477E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 1.72 1087.77 227.00 1.84 5.00 1083.30 225.00 1.84

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9278E+02 EXCESS= .0000E+00 OUTFLOW= .9279E+02 BASIN STORAGE= .3927E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 1.73 1077.08 226.26 1.82 5.00 1072.79 225.00 1.82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9172E+02 EXCESS= .0000E+00 OUTFLOW= .9173E+02 BASIN STORAGE= .3817E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 1.73 1069.06 226.95 1.81 5.00 1062.80 225.00 1.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9100E+02 EXCESS= .0000E+00 OUTFLOW= .9101E+02 BASIN STORAGE= .3937E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 1.74 1055.75 226.36 1.78 5.00 1050.97 225.00 1.78

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8979E+02 EXCESS= .0000E+00 OUTFLOW= .8980E+02 BASIN STORAGE= .3511E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCSW17 MANE 2.30 524.06 227.64 .87 5.00 520.91 225.00 .87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4386E+02 EXCESS= .0000E+00 OUTFLOW= .4387E+02 BASIN STORAGE= .3897E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 1.67 2325.51 231.44 2.07 5.00 2306.80 235.00 2.07

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2301E+03 EXCESS= .0000E+00 OUTFLOW= .2301E+03 BASIN STORAGE= .3123E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 1.68 2279.65 231.56 2.02 5.00 2258.94 235.00 2.02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2252E+03 EXCESS= .0000E+00 OUTFLOW= .2252E+03 BASIN STORAGE= .2858E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 1.70 2197.90 232.94 1.95 5.00 2181.01 235.00 1.95

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2170E+03 EXCESS= .0000E+00 OUTFLOW= .2170E+03 BASIN STORAGE= .2984E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 1.72 2118.94 232.70 1.87 5.00 2102.63 235.00 1.88

INT.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2088E+03 EXCESS= .0000E+00 OUTFLOW= .2088E+03 BASIN STORAGE= .3195E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 1.73 2088.03 232.28 1.85 5.00 2070.54 235.00 1.85

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2056E+03 EXCESS= .0000E+00 OUTFLOW= .2056E+03 BASIN STORAGE= .2784E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 1.74 2062.77 233.22 1.83 5.00 2047.86 235.00 1.83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2033E+03 EXCESS= .0000E+00 OUTFLOW= .2033E+03 BASIN STORAGE= .2736E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 1.75 2050.03 232.14 1.81 5.00 2032.41 235.00 1.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2017E+03 EXCESS= .0000E+00 OUTFLOW= .2017E+03 BASIN STORAGE= .2832E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 1.75 2021.32 233.22 1.79 5.00 2006.95 235.00 1.79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1991E+03 EXCESS= .0000E+00 OUTFLOW= .1991E+03 BASIN STORAGE= .2680E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON9 MANE 2.26 1012.15 235.03 .89 5.00 1012.06 235.00 .89

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9869E+02 EXCESS= .0000E+00 OUTFLOW= .9869E+02 BASIN STORAGE= .3005E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON10 MANE .60 2333.28 234.63 2.05 5.00 2332.79 235.00 2.05

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2358E+03 EXCESS= .0000E+00 OUTFLOW= .2358E+03 BASIN STORAGE= .6461E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON10 MANE .61 2285.03 235.07 2.00 5.00 2284.96 235.00 2.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2307E+03 EXCESS= .0000E+00 OUTFLOW= .2307E+03 BASIN STORAGE= .6535E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON10 MANE .62 2205.87 234.78 1.93 5.00 2205.32 235.00 1.93

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2223E+03 EXCESS= .0000E+00 OUTFLOW= .2223E+03 BASIN STORAGE= .6329E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON10 MANE .62 2126.09 235.18 1.86 5.00 2125.98 235.00 1.86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2139E+03 EXCESS= .0000E+00 OUTFLOW= .2139E+03 BASIN STORAGE= .6895E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON10 MANE .63 2093.78 235.14 1.83 5.00 2093.60 235.00 1.83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2106E+03 EXCESS= .0000E+00 OUTFLOW= .2106E+03 BASIN STORAGE= .6335E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON10 MANE .63 2070.79 234.75 1.81 5.00 2070.42 235.00 1.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2082E+03 EXCESS= .0000E+00 OUTFLOW= .2082E+03 BASIN STORAGE= .6563E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON10 MANE .63 2054.84 234.72 1.79 5.00 2054.60 235.00 1.79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2065E+03 EXCESS= .0000E+00 OUTFLOW= .2065E+03 BASIN STORAGE= .6369E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00

						INT. OUT			
RCON10	MANE	.63	2029.69	235.08	1.77	5.00	2029.52	235.00	1.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2039E+03 EXCESS= .0000E+00 OUTFLOW= .2039E+03 BASIN STORAGE= .6497E-03 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= .00									
RCON10	MANE	.80	1022.36	235.96	.87	5.00	1020.18	235.00	.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1008E+03 EXCESS= .0000E+00 OUTFLOW= .1008E+03 BASIN STORAGE= .6474E-03 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	4.25	167.38	221.00	1.99	5.00	166.33	220.00	1.99
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1179E+02 EXCESS= .0000E+00 OUTFLOW= .1181E+02 BASIN STORAGE= .2635E-02 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	4.25	164.16	221.00	1.95	5.00	163.07	220.00	1.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1155E+02 EXCESS= .0000E+00 OUTFLOW= .1156E+02 BASIN STORAGE= .2609E-02 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	4.25	158.77	221.00	1.88	5.00	157.63	220.00	1.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1114E+02 EXCESS= .0000E+00 OUTFLOW= .1115E+02 BASIN STORAGE= .2565E-02 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	4.00	155.50	220.00	1.81	5.00	155.50	220.00	1.81
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1074E+02 EXCESS= .0000E+00 OUTFLOW= .1075E+02 BASIN STORAGE= .2457E-02 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	4.00	153.27	220.00	1.78	5.00	153.27	220.00	1.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1057E+02 EXCESS= .0000E+00 OUTFLOW= .1059E+02 BASIN STORAGE= .2440E-02 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	4.00	151.72	220.00	1.77	5.00	151.72	220.00	1.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1046E+02 EXCESS= .0000E+00 OUTFLOW= .1047E+02 BASIN STORAGE= .2427E-02 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	4.00	150.60	220.00	1.75	5.00	150.60	220.00	1.75
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1038E+02 EXCESS= .0000E+00 OUTFLOW= .1039E+02 BASIN STORAGE= .2418E-02 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	4.25	146.92	221.00	1.73	5.00	145.67	220.00	1.73
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1024E+02 EXCESS= .0000E+00 OUTFLOW= .1025E+02 BASIN STORAGE= .2466E-02 PERCENT ERROR= -.1									
FOR PLAN = 1 RATIO= .00									
RCON14	MANE	5.00	78.65	220.00	.88	5.00	78.65	220.00	.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5186E+01 EXCESS= .0000E+00 OUTFLOW= .5194E+01 BASIN STORAGE= .2404E-02 PERCENT ERROR= -.2									
FOR PLAN = 1 RATIO= .00									
RCON16	MANE	1.14	364.28	215.97	1.76	5.00	359.39	215.00	1.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2616E+02 EXCESS= .0000E+00 OUTFLOW= .2616E+02 BASIN STORAGE= .6526E-03 PERCENT ERROR= .0									
FOR PLAN = 1 RATIO= .00									
RCON16	MANE	1.15	355.90	216.44	1.72	5.00	350.77	215.00	1.72
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2557E+02 EXCESS= .0000E+00 OUTFLOW= .2557E+02 BASIN STORAGE= .6583E-03 PERCENT ERROR= .0									

INT.OUT

FOR PLAN = 1 RATIO= .00
RCON16 MANE 1.16 341.56 215.75 1.65 5.00 337.55 215.00 1.66

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2460E+02 EXCESS= .0000E+00 OUTFLOW= .2460E+02 BASIN STORAGE= .6620E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON16 MANE 1.17 331.02 216.11 1.59 5.00 325.60 215.00 1.59

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2366E+02 EXCESS= .0000E+00 OUTFLOW= .2366E+02 BASIN STORAGE= .6418E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON16 MANE 1.18 325.64 216.11 1.56 5.00 320.26 215.00 1.57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2327E+02 EXCESS= .0000E+00 OUTFLOW= .2328E+02 BASIN STORAGE= .6381E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON16 MANE 1.19 320.08 215.76 1.55 5.00 315.72 215.00 1.55

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2300E+02 EXCESS= .0000E+00 OUTFLOW= .2300E+02 BASIN STORAGE= .6932E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON16 MANE 1.19 319.08 216.37 1.53 5.00 313.36 215.00 1.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2281E+02 EXCESS= .0000E+00 OUTFLOW= .2281E+02 BASIN STORAGE= .6902E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON16 MANE 1.20 314.09 216.32 1.51 5.00 308.69 215.00 1.51

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2248E+02 EXCESS= .0000E+00 OUTFLOW= .2248E+02 BASIN STORAGE= .6429E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RCON16 MANE 1.53 149.77 217.94 .72 5.00 147.02 220.00 .72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1076E+02 EXCESS= .0000E+00 OUTFLOW= .1076E+02 BASIN STORAGE= .6687E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
RC13B-1 MANE 5.00 353.60 225.00 2.27 5.00 353.60 225.00 2.27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3020E+02 EXCESS= .0000E+00 OUTFLOW= .3021E+02 BASIN STORAGE= .1566E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13B-1 MANE 5.00 346.83 225.00 2.23 5.00 346.83 225.00 2.23

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2960E+02 EXCESS= .0000E+00 OUTFLOW= .2961E+02 BASIN STORAGE= .1548E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13B-1 MANE 5.00 335.54 225.00 2.15 5.00 335.54 225.00 2.15

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2860E+02 EXCESS= .0000E+00 OUTFLOW= .2861E+02 BASIN STORAGE= .1518E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13B-1 MANE 5.00 324.25 225.00 2.08 5.00 324.25 225.00 2.08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2760E+02 EXCESS= .0000E+00 OUTFLOW= .2762E+02 BASIN STORAGE= .1489E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13B-1 MANE 5.00 319.73 225.00 2.05 5.00 319.73 225.00 2.05

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2721E+02 EXCESS= .0000E+00 OUTFLOW= .2722E+02 BASIN STORAGE= .1476E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13B-1 MANE 5.00 316.57 225.00 2.03 5.00 316.57 225.00 2.03

										INT.OUT
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2693E+02 EXCESS= .0000E+00 OUTFLOW= .2694E+02 BASIN STORAGE= .1468E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-1	MANE	5.00	314.32	230.00	2.01	5.00	314.32	230.00	2.01	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2673E+02 EXCESS= .0000E+00 OUTFLOW= .2675E+02 BASIN STORAGE= .1462E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-1	MANE	5.00	310.89	230.00	1.99	5.00	310.89	230.00	1.99	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2641E+02 EXCESS= .0000E+00 OUTFLOW= .2643E+02 BASIN STORAGE= .1452E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-1	MANE	5.00	171.06	230.00	1.05	5.00	171.06	230.00	1.05	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1391E+02 EXCESS= .0000E+00 OUTFLOW= .1392E+02 BASIN STORAGE= .1716E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	640.80	230.00	2.18	5.00	640.80	230.00	2.18	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5392E+02 EXCESS= .0000E+00 OUTFLOW= .5398E+02 BASIN STORAGE= .5817E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	628.20	230.00	2.13	5.00	628.20	230.00	2.13	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5282E+02 EXCESS= .0000E+00 OUTFLOW= .5288E+02 BASIN STORAGE= .5767E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	607.17	230.00	2.06	5.00	607.17	230.00	2.06	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5100E+02 EXCESS= .0000E+00 OUTFLOW= .5105E+02 BASIN STORAGE= .5683E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	586.10	230.00	1.99	5.00	586.10	230.00	1.99	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4918E+02 EXCESS= .0000E+00 OUTFLOW= .4923E+02 BASIN STORAGE= .5597E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	578.31	230.00	1.96	5.00	578.31	230.00	1.96	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4845E+02 EXCESS= .0000E+00 OUTFLOW= .4850E+02 BASIN STORAGE= .7165E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	572.39	230.00	1.94	5.00	572.39	230.00	1.94	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4794E+02 EXCESS= .0000E+00 OUTFLOW= .4799E+02 BASIN STORAGE= .7136E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	568.15	230.00	1.92	5.00	568.15	230.00	1.92	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4758E+02 EXCESS= .0000E+00 OUTFLOW= .4763E+02 BASIN STORAGE= .7115E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	561.38	230.00	1.90	5.00	561.38	230.00	1.90	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4700E+02 EXCESS= .0000E+00 OUTFLOW= .4705E+02 BASIN STORAGE= .6748E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
RC13B-2	MANE	5.00	295.27	235.00	.98	5.00	295.27	235.00	.98	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2427E+02 EXCESS= .0000E+00 OUTFLOW= .2430E+02 BASIN STORAGE= .7210E-02 PERCENT ERROR= -.1										
FOR PLAN = 1 RATIO= .00										
R19A	MANE	5.00	318.89	235.00	2.18	5.00	318.89	235.00	2.18	

INT.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2936E+02 EXCESS= .0000E+00 OUTFLOW= .2938E+02 BASIN STORAGE= .2006E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
R19A MANE 5.00 312.72 235.00 2.13 5.00 312.72 235.00 2.13

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2875E+02 EXCESS= .0000E+00 OUTFLOW= .2877E+02 BASIN STORAGE= .1983E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
R19A MANE 5.00 302.45 235.00 2.06 5.00 302.45 235.00 2.06

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2774E+02 EXCESS= .0000E+00 OUTFLOW= .2776E+02 BASIN STORAGE= .1945E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
R19A MANE 5.00 292.17 235.00 1.98 5.00 292.17 235.00 1.98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2673E+02 EXCESS= .0000E+00 OUTFLOW= .2675E+02 BASIN STORAGE= .1906E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
R19A MANE 5.00 288.05 235.00 1.95 5.00 288.05 235.00 1.95

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2633E+02 EXCESS= .0000E+00 OUTFLOW= .2635E+02 BASIN STORAGE= .1891E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
R19A MANE 5.00 285.17 235.00 1.93 5.00 285.17 235.00 1.93

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2605E+02 EXCESS= .0000E+00 OUTFLOW= .2606E+02 BASIN STORAGE= .1880E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
R19A MANE 5.00 283.11 235.00 1.92 5.00 283.11 235.00 1.92

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2585E+02 EXCESS= .0000E+00 OUTFLOW= .2586E+02 BASIN STORAGE= .1872E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
R19A MANE 5.00 279.82 235.00 1.89 5.00 279.82 235.00 1.89

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2553E+02 EXCESS= .0000E+00 OUTFLOW= .2554E+02 BASIN STORAGE= .1860E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
R19A MANE 5.00 146.43 235.00 .96 5.00 146.43 235.00 .96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1300E+02 EXCESS= .0000E+00 OUTFLOW= .1300E+02 BASIN STORAGE= .2023E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13A-2 MANE 5.00 780.51 235.00 2.18 5.00 780.51 235.00 2.18

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7731E+02 EXCESS= .0000E+00 OUTFLOW= .7736E+02 BASIN STORAGE= .8795E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13A-2 MANE 5.00 764.75 235.00 2.14 5.00 764.75 235.00 2.14

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7572E+02 EXCESS= .0000E+00 OUTFLOW= .7577E+02 BASIN STORAGE= .8721E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13A-2 MANE 5.00 738.48 235.00 2.06 5.00 738.48 235.00 2.06

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7309E+02 EXCESS= .0000E+00 OUTFLOW= .7314E+02 BASIN STORAGE= .8303E-02 PERCENT ERROR= -.1

FOR PLAN = 1 RATIO= .00
RC13A-2 MANE 5.00 712.20 235.00 1.99 5.00 712.20 235.00 1.99

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7047E+02 EXCESS= .0000E+00 OUTFLOW= .7051E+02 BASIN STORAGE= .8180E-02 PERCENT ERROR= -.1

		INT.OUT							
FOR PLAN = 1	RATIO= .00								
RC13A-2	MANE	5.00	701.68	235.00	1.96	5.00	701.68	235.00	1.96
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6942E+02 EXCESS= .0000E+00 OUTFLOW= .6947E+02 BASIN STORAGE= .8130E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RC13A-2	MANE	5.00	694.32	235.00	1.94	5.00	694.32	235.00	1.94
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6869E+02 EXCESS= .0000E+00 OUTFLOW= .6873E+02 BASIN STORAGE= .8095E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RC13A-2	MANE	5.00	689.06	235.00	1.92	5.00	689.06	235.00	1.92
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6817E+02 EXCESS= .0000E+00 OUTFLOW= .6821E+02 BASIN STORAGE= .7878E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RC13A-2	MANE	5.00	680.64	235.00	1.90	5.00	680.64	235.00	1.90
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6733E+02 EXCESS= .0000E+00 OUTFLOW= .6738E+02 BASIN STORAGE= .7838E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RC13A-2	MANE	5.00	353.55	240.00	.98	5.00	353.55	240.00	.98
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3459E+02 EXCESS= .0000E+00 OUTFLOW= .3462E+02 BASIN STORAGE= .6811E-02 PERCENT ERROR= -.1									
FOR PLAN = 1	RATIO= .00								
RCPIC-C	MANE	2.90	1036.21	237.50	2.15	5.00	1029.58	235.00	2.15
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1041E+03 EXCESS= .0000E+00 OUTFLOW= .1041E+03 BASIN STORAGE= .2599E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .00								
RCPIC-C	MANE	2.92	1018.48	236.21	2.11	5.00	1009.34	235.00	2.11
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1020E+03 EXCESS= .0000E+00 OUTFLOW= .1020E+03 BASIN STORAGE= .2441E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .00								
RCPIC-C	MANE	2.95	983.10	236.05	2.03	5.00	975.10	235.00	2.03
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9842E+02 EXCESS= .0000E+00 OUTFLOW= .9843E+02 BASIN STORAGE= .3029E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .00								
RCPIC-C	MANE	2.99	947.55	235.94	1.96	5.00	940.20	235.00	1.96
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9487E+02 EXCESS= .0000E+00 OUTFLOW= .9488E+02 BASIN STORAGE= .2774E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .00								
RCPIC-C	MANE	3.00	935.30	237.12	1.93	5.00	921.65	235.00	1.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9346E+02 EXCESS= .0000E+00 OUTFLOW= .9347E+02 BASIN STORAGE= .2840E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .00								
RCPIC-C	MANE	3.01	923.69	237.96	1.91	5.00	914.93	235.00	1.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9247E+02 EXCESS= .0000E+00 OUTFLOW= .9248E+02 BASIN STORAGE= .2450E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .00								
RCPIC-C	MANE	3.02	912.75	235.55	1.90	5.00	907.94	235.00	1.89
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9176E+02 EXCESS= .0000E+00 OUTFLOW= .9177E+02 BASIN STORAGE= .2737E-02 PERCENT ERROR= .0									
FOR PLAN = 1	RATIO= .00								
RCPIC-C	MANE	3.03	906.65	236.52	1.87	5.00	895.54	235.00	1.87
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9064E+02 EXCESS= .0000E+00 OUTFLOW= .9064E+02 BASIN STORAGE= .3045E-02 PERCENT ERROR= .0									

INT.OUT

FOR PLAN = 1 RATIO= .00
 RCPIC-C MANE 3.82 462.80 240.43 .96 5.00 461.30 240.00 .96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4647E+02 EXCESS= .0000E+00 OUTFLOW= .4648E+02 BASIN STORAGE= .2735E-02 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 5.00 85.62 225.00 1.50 5.00 85.62 225.00 1.50

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5242E+01 EXCESS= .0000E+00 OUTFLOW= .5262E+01 BASIN STORAGE= .6505E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 5.00 83.65 225.00 1.47 5.00 83.65 225.00 1.47

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5111E+01 EXCESS= .0000E+00 OUTFLOW= .5131E+01 BASIN STORAGE= .6457E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 5.00 80.35 225.00 1.40 5.00 80.35 225.00 1.40

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4894E+01 EXCESS= .0000E+00 OUTFLOW= .4914E+01 BASIN STORAGE= .6374E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 5.00 77.02 225.00 1.34 5.00 77.02 225.00 1.34

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4680E+01 EXCESS= .0000E+00 OUTFLOW= .4699E+01 BASIN STORAGE= .6290E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 5.00 75.69 225.00 1.32 5.00 75.69 225.00 1.32

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4594E+01 EXCESS= .0000E+00 OUTFLOW= .4613E+01 BASIN STORAGE= .6256E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 5.00 74.75 225.00 1.30 5.00 74.75 225.00 1.30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4535E+01 EXCESS= .0000E+00 OUTFLOW= .4553E+01 BASIN STORAGE= .6232E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 5.00 74.08 225.00 1.29 5.00 74.08 225.00 1.29

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4492E+01 EXCESS= .0000E+00 OUTFLOW= .4511E+01 BASIN STORAGE= .6038E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 5.00 73.00 225.00 1.27 5.00 73.00 225.00 1.27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4425E+01 EXCESS= .0000E+00 OUTFLOW= .4442E+01 BASIN STORAGE= .6011E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
 RCON1 MANE 4.00 31.17 228.00 .55 5.00 30.06 230.00 .54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1896E+01 EXCESS= .0000E+00 OUTFLOW= .1909E+01 BASIN STORAGE= .5556E-02 PERCENT ERROR= -1.0

FOR PLAN = 1 RATIO= .00
 RPIC-B MANE 1.74 439.87 237.27 2.03 5.00 439.01 235.00 2.03

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4783E+02 EXCESS= .0000E+00 OUTFLOW= .4783E+02 BASIN STORAGE= .2578E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
 RPIC-B MANE 1.75 432.13 236.45 1.99 5.00 430.53 235.00 1.99

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4685E+02 EXCESS= .0000E+00 OUTFLOW= .4685E+02 BASIN STORAGE= .2499E-03 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00
 RPIC-B MANE 1.76 417.58 236.27 1.92 5.00 416.38 235.00 1.92

INT.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4522E+02 EXCESS= .0000E+00 OUTFLOW= .4522E+02 BASIN STORAGE= .2493E-03 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RPIC-B	MANE	1.78	403.10	236.14	1.85	5.00	402.16	235.00	1.85

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4360E+02 EXCESS= .0000E+00 OUTFLOW= .4360E+02 BASIN STORAGE= .2464E-03 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RPIC-B	MANE	1.78	398.34	236.81	1.83	5.00	396.16	235.00	1.83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4296E+02 EXCESS= .0000E+00 OUTFLOW= .4296E+02 BASIN STORAGE= .2533E-03 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RPIC-B	MANE	1.78	393.51	237.29	1.81	5.00	392.22	235.00	1.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4251E+02 EXCESS= .0000E+00 OUTFLOW= .4250E+02 BASIN STORAGE= .2248E-03 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RPIC-B	MANE	1.79	390.10	235.85	1.79	5.00	389.58	235.00	1.79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4218E+02 EXCESS= .0000E+00 OUTFLOW= .4218E+02 BASIN STORAGE= .2523E-03 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RPIC-B	MANE	1.79	386.39	236.40	1.77	5.00	385.05	235.00	1.77

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4167E+02 EXCESS= .0000E+00 OUTFLOW= .4167E+02 BASIN STORAGE= .2662E-03 PERCENT ERROR= .0

FOR PLAN = 1	RATIO=	.00							
RPIC-B	MANE	2.03	203.87	238.08	.91	5.00	202.47	235.00	.91

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2143E+02 EXCESS= .0000E+00 OUTFLOW= .2143E+02 BASIN STORAGE= .2507E-03 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

APPENDIX C

Hydraulic Calculations

[TITLE]
GCW #840.050A (The 435 - CCRFCD STORM DRAIN)
MAIN1 TRUNK
3rd RTC to TDS

0

[REPORT]
COMPOSITE_ONLY

[NETWORK]
**TYPE NAME
**-----
Outlet "No 1"
Transition "No 2"
Transition "No 3"
Reach "No 4"
Reach "No 5"
Reach "No 6"
Reach "No 7"
Reach "No 8"
Reach "No 9"
Reach "No 10"
Reach "No 11"
Reach "No 12"
Reach "No 13"
Reach "No 14"
Reach "No 15"
Reach "No 16"
Junction "No 17"
Reach "No 18"
Transition "No 19"
Reach "No 20"
Reach "No 21"
Reach "No 22"
Reach "No 23"
Reach "No 24"
Reach "No 25"
Reach "No 26"
Reach "No 27"
Junction "No 28"
Reach "No 29"
Reach "No 30"
Junction "No 31"
Reach "No 32"
Reach "No 33"
Junction "No 34"
Reach "No 35"
Reach "No 36"
Headwork "No 37"

**BRANCH DEFINITIONS

[OUTLET]
**NAME STATION INVERT GROUND CHANNEL WATER SURFACE
** ELEV ELEV ID ELEV (opt.)
**-----
"No 1" 0 2621.3 0 "channel14" 0

[HEADWORK]
**NAME INVERT GROUND CHANNEL FLOW WATER SURFACE
** ELEV ELEV ID ELEV (opt.)
**-----
"No 37" 2739.62 0 "channel 4" 2450 0

[WALLENTANCE]
**NAME INVERT GROUND CHANNEL LOSS
** ELEV ELEV ID COEFFICIENT(opt.)
**-----

[WALLEXIT]
**NAME INVERT GROUND CHANNEL LOSS
** ELEV ELEV ID COEFFICIENT(opt.)
**-----

[BRIDGEENTRANCE]
**NAME INVERT GROUND CHANNEL REDUCTION
** ELEV ELEV ID FACTOR(opt.)
**-----

[BRIDGEEXIT]
**NAME INVERT GROUND CHANNEL REDUCTION
** ELEV ELEV ID FACTOR(opt.)
**-----

[JOIN]
**NAME INVERT GROUND CHANNEL LENGTH MANNINGS n NUMBER OF CONFLUENCE
** ELEV ELEV ID BRANCHES ANGLE
**-----

[JUNCTION]

main0626.wsx								
**Name	INVERT ELEV	GROUND ELEV	CHANNEL ID	LENGTH	MANNINGS n	NUMBER OF LATERALS	CONFLUENCE ANGLE	FLOW
**-----								
"No 17"	2663.13	0	"channel10"	10	0.015	1		
"No 17_Lateral1"	2663.42		"channel6"				-60	188
"No 28"	2701.73	0	"channel 4"	36.66	0.015	1		
"No 28_Lateral1"	2701.73		"channel3"				-15	2008
"No 31"	2721.11	0	"channel 4"	26.53	0.015	2		
"No 31_Lateral1"	2721.13		"channel5"				-30	9
"No 31_Lateral2"	2721.13		"channel11"				58	17
"No 34"	2734.24	0	"channel 4"	8	0.015	2		
"No 34_Lateral1"	2734.52		"72 pipe"				30	8
"No 34_Lateral2"	2734.52		"72 pipe"				30	5

[TRANSITION]

**NAME	INVERT ELEV	GROUND ELEV	CHANNEL ID	LENGTH	MANNINGS n
**-----					
"No 2"	2621.65	0	"channel15"	24.86	0.015
"No 3"	2621.81	0	"channel10"	10	0.015
"No 19"	2668.54	0	"channel12"	30	0.023

[REACH]

**NAME	INVERT ELEV	GROUND ELEV	CHANNEL ID	LENGTH	MANNINGS n	CURVE (opt)	ANGLE POINT(opt)	NUMBER MANHOLES(opt)
**-----								
"No 4"	2623.18	0	"channel10"	90.31	0.015	0	0	0
"No 5"	2623	0	"Channel10"	2.32	0.015	0	0	0
"No 6"	2625	0	"Channel10"	70.62	0.015	-40.46	0	0
"No 7"	2625.48	0	"Channel10"	17.41	0.015	0	0	0
"No 8"	2627.86	0	"Channel10"	85.3	0.015	48.87	0	0
"No 9"	2631.86	0	"Channel10"	143.47	0.015	0	0	0
"No 10"	2645.03	0	"Channel10"	472.89	0.015	13.91	0	0
"No 11"	2648.24	0	"Channel10"	115.41	0.015	-66.13	0	0
"No 12"	2651.53	0	"Channel10"	118.22	0.015	0	0	0
"No 13"	2655.26	0	"Channel10"	466.14	0.015	0	0	0
"No 14"	2656.61	0	"Channel10"	168.86	0.015	90	0	0
"No 15"	2659.44	0	"Channel10"	565	0.015	0	0	0
"No 16"	2662.94	0	"channel10"	145.16	0.015	0	0	0
"No 18"	2666.75	0	"channel10"	194.84	0.015	0	0	0
"No 20"	2670.81	0	"channel12"	38.03	0.015	0	0	0
"No 21"	2671.71	0	"channel12"	90.08	0.015	34.41	0	0
"No 22"	2675.47	0	"channel12"	375.81	0.015	0	0	0
"No 23"	2676.57	0	"channel12"	109.42	0.015	12.54	0	0
"No 24"	2677.16	0	"channel12"	59.62	0.015	0	0	0
"No 25"	2677.68	0	"channel12"	52.03	0.015	-19.87	0	0
"No 26"	2686	0	"channel12"	616.02	0.015	0	0	0
"No 27"	2700.81	0	"channel12"	251.82	0.023	-20.04	0	0
"No 29"	2710.25	0	"channel 4"	338.86	0.015	-26.97	0	0
"No 30"	2720.45	0	"channel 4"	407.05	0.015	0	0	0
"No 32"	2732.17	0	"channel 4"	613.91	0.015	0	0	0
"No 33"	2734.1	0	"channel 4"	107.29	0.015	40.982	0	0
"No 35"	2738.05	0	"channel 4"	219.12	0.015	0	0	0
"No 36"	2739.62	0	"channel 4"	87.41	0.015	33.388	0	0

[CHANNEL]

**REGULAR TYPES 1-4								
**ID	TYPE	HEIGHT	WIDTH	LEFT SLOPE	RIGHT SLOPE	NUMBER PIERS	AVG PIER WIDTH	INVERT CROSS FALL
**-----								
"channel 4"	3	10	10	0	0	0	0	0
"channel10"	3	12	25	0	0	1	1	0
"channel16"	4	6	6					
"channel13"	3	8	10	0	0	0	0	0
"channel15"	4	4	4					
"channel111"	3	6	6	0	0	0	0	0
"72 pipe"	4	6	6					
"channel12"	3	12	14	0	0	0	0	0

**IRREGULAR TYPES 5-6

**ID	TYPE	NUMBER PIERS	AVG PIER WIDTH	PIER1 ELEV	PIER2 ELEV	PIER3 ELEV	PIER4 ELEV	PIER5 ELEV	PIER6 ELEV	PIER7 ELEV	PIER8 ELEV	PIER9 ELEV	PIER10 ELEV
**-----													
"channel14"5		0	0										
"channel15"5		0	0										

[POINT]

**ID	XCOORD	YCOORD
**-----		
"channel14"	0	2648
"channel14"	19.09	2648
"channel14"	50.85	2645
"channel14"	111.11	2621

"channel14"	159.24	2621
"channel14"	186.97	2635.98
"channel14"	248.78	2640

"channel15"	0	2648
"channel15"	11.03	2648
"channel15"	54.93	2638
"channel15"	84.46	2622
"channel15"	136.39	2622
"channel15"	173.21	2640

 Water Surface Profile Gradient (WSPG)
 XP WSPG
 Engine Version 1.3 06/09/2010
 XP Software www.xpsoftware.com

INPUT FILE

 C:\Program Files (x86)\CIVILD\main0626.wsx
 Computed 06/28/18 08:35:43

TITLE INFORMATION

 GCW #840.050A (The 435 - CCRFCD STORM DRAIN)
 MAIN1 TRUNK
 3rd RTC to TDS

0

WARNING SUMMARY

 WARNING 47: Junction No 28 has a different channel than its direct downstream element.
 WARNING 15: Invert elevation of element No 5 is not larger than invert elevation of the direct downstream element.
 WARNING 25: Link type element No 16 has different invert elevation than its upstream node.
 WARNING 25: Link type element No 27 has different invert elevation than its upstream node.
 WARNING 25: Link type element No 30 has different invert elevation than its upstream node.
 WARNING 25: Link type element No 33 has different invert elevation than its upstream node.
 WARNING 36: D/S processing stopped in junction No 34 because critical momentum is greater than maximum momentum.
 WARNING 36: D/S processing stopped in junction No 31 because critical momentum is greater than maximum momentum.
 WARNING 36: D/S processing stopped in junction No 28 because critical momentum is greater than maximum momentum.

RESULTS

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Main Line

=====

Composite Profile:

ELEMENT	TYPE	STATION	INVERT	GROUND	W.S.	DEPTH	Q	VELOC.	VELOC.	ENERGY	SUPER
CRITICAL	FROUDE	SLOPE	NORMAL	CROSS							
NAME			ELEV	ELEV	ELEV				HEAD	GRADE IN	ELEV
DEPTH	NUMBER	DEPTH	SECTION								
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
###											
"No 1"	Outlet	0.00	2621.30	0.00	*2623.864	2.564	4685.00	34.01	17.96	2641.83	0.000
6.041	0.000	0.00000	0.000	Irreg.open							
"No 2"	Transition	24.86	2621.65	0.00	*2624.014	2.364	4685.00	35.06	19.09	2643.10	0.000
5.855	6.025	0.01408	0.000	Irreg.open							
"No 3"	Transition	34.86	2621.81	0.00	*2627.920	6.110	4685.00	31.95	15.85	2643.77	0.000
10.580	2.278	0.01600	0.000	Tr./Rect.closed							
"No 4"	Reach	125.17	2623.18	0.00	*2629.094	5.914	4685.00	33.01	16.92	2646.01	0.000
10.580	2.392	0.01517	7.244	Tr./Rect.closed							
"No 5"	Reach	127.49	2623.00	0.00	*2628.864	5.864	4685.00	33.29	17.21	2646.07	0.000
10.580	2.423	-0.07759	12.000	Tr./Rect.closed							
"No 6"	Reach	198.11	2625.00	0.00	*2630.893	5.893	4685.00	33.13	17.04	2647.93	0.000
10.580	2.405	0.02832	5.720	Tr./Rect.closed							
"No 7"	Reach	215.52	2625.48	0.00	*2631.378	5.898	4685.00	33.10	17.01	2648.39	0.000
10.580	2.402	0.02757	5.778	Tr./Rect.closed							
"No 8"	Reach	300.82	2627.86	0.00	*2633.794	5.934	4685.00	32.89	16.80	2650.60	0.000
10.580	2.380	0.02790	5.752	Tr./Rect.closed							
"No 9"	Reach	444.29	2631.86	0.00	*2637.879	6.019	4685.00	32.43	16.33	2654.21	0.000
10.580	2.329	0.02788	5.754	Tr./Rect.closed							
	"i.p."	649.70	2637.58	0.00	*2643.808	6.227	4685.00	31.35	15.26	2659.07	0.000
10.580	2.214	0.02785	5.756	Tr./Rect.closed							
	"i.p."	813.77	2642.15	0.00	*2648.681	6.531	4685.00	29.89	13.87	2662.55	0.000
10.580	2.061	0.02785	5.756	Tr./Rect.closed							
"No 10"	Reach	917.18	2645.03	0.00	*2651.879	6.849	4685.00	28.50	12.61	2664.49	0.000
10.580	1.919	0.02785	5.756	Tr./Rect.closed							
	"i.p."	977.00	2646.69	0.00	*2653.811	7.117	4685.00	27.43	11.68	2665.49	0.000
10.580	1.812	0.02781	5.759	Tr./Rect.closed							
"No 11"	Reach	1032.59	2648.24	0.00	*2655.705	7.465	4685.00	26.15	10.62	2666.32	0.000
10.580	1.687	0.02781	5.759	Tr./Rect.closed							
	"i.p."	1059.03	2648.98	0.00	*2656.660	7.684	4685.00	25.40	10.02	2666.68	0.000
10.580	1.615	0.02783	5.758	Tr./Rect.closed							
	"i.p."	1093.48	2649.93	0.00	*2657.993	8.059	4685.00	24.22	9.11	2667.10	0.000
10.580	1.504	0.02783	5.758	Tr./Rect.closed							
	"i.p."	1119.09	2650.65	0.00	*2659.100	8.452	4685.00	23.09	8.28	2667.38	0.000
10.580	1.400	0.02783	5.758	Tr./Rect.closed							
	"i.p."	1137.77	2651.17	0.00	*2660.032	8.865	4685.00	22.02	7.53	2667.56	0.000
10.580	1.303	0.02783	5.758	Tr./Rect.closed							

"No 12"	Reach	1150.81	2651.53	0.00	*2660.828	9.298	4685.00	21.00	6.84	2667.67	0.000
10.580	1.213	0.02783	5.758	Tr./Rect.closed							
	"i.p."	1160.50	2651.61	0.00	*2660.905	9.298	4685.00	21.00	6.84	2667.75	0.000
10.580	1.213	0.00800	9.298	Tr./Rect.closed							
"No 13"	Reach	1616.95	2655.26	0.00	*2664.396	9.136	4685.00	21.37	7.09	2671.49	0.000
10.580	1.246	0.00800	9.298	Tr./Rect.closed							
"No 14"	Reach	1785.81	2656.61	0.00	*2665.586	8.976	4685.00	21.75	7.34	2672.93	0.000
10.580	1.279	0.00799	9.301	Tr./Rect.closed							
	"i.p."	1852.89	2656.95	0.00	*2665.540	8.594	4685.00	22.71	8.01	2673.55	0.000
10.580	1.365	0.00501	11.219	Tr./Rect.closed							
	"i.p."	1927.28	2657.32	0.00	*2665.513	8.194	4685.00	23.82	8.81	2674.33	0.000
10.580	1.467	0.00501	11.219	Tr./Rect.closed							
	"i.p."	2001.41	2657.69	0.00	*2665.503	7.813	4685.00	24.98	9.69	2675.20	0.000
10.580	1.575	0.00501	11.219	Tr./Rect.closed							
	"i.p."	2074.55	2658.06	0.00	*2665.506	7.449	4685.00	26.20	10.66	2676.17	0.000
10.580	1.692	0.00501	11.219	Tr./Rect.closed							
	"i.p."	2146.29	2658.42	0.00	*2665.518	7.103	4685.00	27.48	11.73	2677.25	0.000
10.580	1.817	0.00501	11.219	Tr./Rect.closed							
	"i.p."	2216.35	2658.77	0.00	*2665.539	6.772	4685.00	28.82	12.90	2678.44	0.000
10.580	1.952	0.00501	11.219	Tr./Rect.closed							
	"i.p."	2284.56	2659.11	0.00	*2665.565	6.457	4685.00	30.23	14.19	2679.76	0.000
10.580	2.097	0.00501	11.219	Tr./Rect.closed							
"No 15"	Reach	2350.81	2659.44	0.00	*2665.597	6.157	4685.00	31.71	15.61	2681.21	0.000
10.580	2.252	0.00501	11.219	Tr./Rect.closed							
"No 16"	Reach	2495.97	2662.94	0.00	*2669.133	6.193	4685.00	31.52	15.43	2684.56	0.000
10.580	2.232	0.02411	6.075	Tr./Rect.closed							
"No 17"	Junction	2505.97	2663.13	0.00	*2668.751	5.621	4497.00	33.33	17.25	2686.00	0.000
10.295	0.000	0.01900	0.000	Tr./Rect.closed							
	"i.p."	2576.90	2664.45	0.00	*2669.941	5.493	4497.00	34.11	18.07	2688.01	0.000
10.295	2.565	0.01858	6.499	Tr./Rect.closed							
"No 18"	Reach	2700.81	2666.75	0.00	*2671.988	5.238	4497.00	35.77	19.87	2691.86	0.000
10.295	2.755	0.01858	6.499	Tr./Rect.closed							
"No 19"	Transition	2730.81	2668.54	0.00	*2678.801	10.261	4497.00	31.31	15.22	2694.02	0.000
12.000	1.722	0.05967	0.000	Tr./Rect.closed							
	"i.p."	2735.77	2668.84	0.00	*2679.213	10.377	4497.00	30.95	14.88	2694.09	0.000
12.000	1.693	0.05969	6.053	Tr./Rect.closed							
	"i.p."	2754.16	2669.93	0.00	*2680.817	10.883	4497.00	29.51	13.53	2694.34	0.000
12.000	1.577	0.05969	6.053	Tr./Rect.closed							
"No 20"	Reach	2768.84	2670.81	0.00	*2682.225	11.415	4497.00	28.14	12.30	2694.52	0.000
12.000	1.468	0.05969	6.053	Tr./Rect.closed							
"No 21"	Reach	2858.92	2671.71	0.00	*2683.006	11.296	4497.00	28.44	12.56	2695.56	0.000
12.000	1.491	0.00999	12.000	Tr./Rect.closed							
	"i.p."	2968.92	2672.81	0.00	*2683.941	11.131	4497.00	28.86	12.93	2696.87	0.000
12.000	1.524	0.01001	12.000	Tr./Rect.closed							
"No 22"	Reach	3234.73	2675.47	0.00	*2686.083	10.613	4497.00	30.27	14.23	2700.31	0.000
12.000	1.637	0.01001	12.000	Tr./Rect.closed							
"No 23"	Reach	3344.15	2676.57	0.00	*2686.932	10.362	4497.00	31.00	14.92	2701.85	0.000
12.000	1.697	0.01005	12.000	Tr./Rect.closed							
"No 24"	Reach	3403.77	2677.16	0.00	*2687.371	10.211	4497.00	31.46	15.37	2702.74	0.000
12.000	1.735	0.00990	12.000	Tr./Rect.closed							
"No 25"	Reach	3455.80	2677.68	0.00	*2687.756	10.076	4497.00	31.88	15.78	2703.54	0.000
12.000	1.770	0.00999	12.000	Tr./Rect.closed							
	"i.p."	3492.25	2678.17	0.00	*2688.211	10.039	4497.00	32.00	15.90	2704.11	0.000
12.000	1.780	0.01351	10.672	Tr./Rect.closed							
	"i.p."	3833.60	2682.78	0.00	*2692.354	9.572	4497.00	33.56	17.49	2709.84	0.000
12.000	1.912	0.01351	10.672	Tr./Rect.closed							
"No 26"	Reach	4071.82	2686.00	0.00	*2695.126	9.126	4497.00	35.20	19.24	2714.36	0.000
12.000	2.053	0.01351	10.672	Tr./Rect.closed							
	"i.p."	4144.73	2690.29	0.00	*2699.743	9.455	4497.00	33.97	17.92	2717.66	0.000
12.000	1.947	0.05881	8.394	Tr./Rect.closed							
	"i.p."	4209.35	2694.09	0.00	*2704.005	9.917	4497.00	32.39	16.29	2720.30	0.000
12.000	1.813	0.05881	8.394	Tr./Rect.closed							
	"i.p."	4253.21	2696.67	0.00	*2707.069	10.401	4497.00	30.88	14.81	2721.88	0.000
12.000	1.688	0.05881	8.394	Tr./Rect.closed							
	"i.p."	4284.46	2698.51	0.00	*2709.414	10.908	4497.00	29.45	13.46	2722.88	0.000
12.000	1.571	0.05881	8.394	Tr./Rect.closed							
	"i.p."	4307.17	2699.84	0.00	*2711.282	11.441	4497.00	28.08	12.24	2723.52	0.000
12.000	1.463	0.05881	8.394	Tr./Rect.closed							
"No 27"	Reach	4323.64	2700.81	0.00	*2712.809	11.999	4497.00	26.77	11.13	2723.94	0.000
12.000	1.362	0.05881	8.394	Tr./Rect.closed							
"No 28"	Junction	4360.30	2701.73	0.00	*2715.667	13.937	2489.00	24.95	9.67	2725.34	0.000
10.000	0.000	0.02510	0.000	Tr./Rect.closed							
"No 29"	Reach	4699.16	2710.25	0.00	*2723.083	12.833	2489.00	24.95	9.67	2732.75	0.000
10.000	1.392	0.02514	7.593	Tr./Rect.closed							
"No 30"	Reach	5106.21	2720.45	0.00	*2730.719	10.269	2489.00	24.95	9.67	2740.39	0.000
10.000	1.392	0.02506	7.603	Tr./Rect.closed							
"No 31"	Junction	5132.74	2721.11	0.00	*2731.610	10.500	2463.00	24.69	9.47	2741.08	0.000
10.000	0.000	0.02488	0.000	Tr./Rect.closed							
"No 32"	Reach	5746.65	2732.17	0.00	*2742.888	10.718	2463.00	24.69	9.47	2752.35	0.000
10.000	1.378	0.01802	8.599	Tr./Rect.closed							
"No 33"	Reach	5853.94	2734.10	0.00	*2746.137	12.037	2463.00	24.69	9.47	2755.60	0.000
10.000	1.378	0.01799	8.604	Tr./Rect.closed							
"No 34"	Junction	5861.94	2734.24	0.00	*2746.481	12.241	2450.00	24.56	9.37	2755.85	0.000
10.000	0.000	0.01750	0.000	Tr./Rect.closed							
"No 35"	Reach	6081.06	2738.05	0.00	*2750.464	12.414	2450.00	24.56	9.37	2759.83	0.000
10.000	1.370	0.01739	8.685	Tr./Rect.closed							
"No 36"	Reach	6168.47	2739.62	0.00	*2753.194	13.574	2450.00	24.56	9.37	2762.56	0.000

10.000	1.370	0.01796	8.573	Tr./Rect.closed								
"No 37"	Headwrk	6168.47	2739.62	0.00	*2753.194	13.574	2450.00	24.56	9.37	2762.56	0.000	
10.000	0.000	0.00000	0.000	Tr./Rect.closed								

*) in the W.S.ELEV column indicates flooding, it is set whenever W.S.ELEV > GROUND ELEV
i.p. = intermediate point processing results for reaches

[TITLE]
 GCW #840.050A (The 435 - CCRFCD STORM DRAIN)
 MAIN1 TRUNK INTERIM CONDITION
 3rd RTC to TDS

0

[REPORT]
 COMPOSITE_ONLY

[NETWORK]
 **TYPE NAME
 **-----
 Outlet "No 1"
 Transition "No 2"
 Transition "No 3"
 Reach "No 4"
 Reach "No 5"
 Reach "No 6"
 Reach "No 7"
 Reach "No 8"
 Reach "No 9"
 Reach "No 10"
 Reach "No 11"
 Reach "No 12"
 Reach "No 13"
 Reach "No 14"
 Reach "No 15"
 Reach "No 16"
 Junction "No 17"
 Reach "No 18"
 Transition "No 19"
 Reach "No 20"
 Reach "No 21"
 Reach "No 22"
 Reach "No 23"
 Reach "No 24"
 Reach "No 25"
 Reach "No 26"
 Reach "No 27"
 Junction "No 28"
 Reach "No 29"
 Reach "No 30"
 Junction "No 31"
 Reach "No 32"
 Reach "No 33"
 Junction "No 34"
 Reach "No 35"
 Reach "No 36"
 Headwork "No 37"

**BRANCH DEFINITIONS

[OUTLET]
 **NAME STATION INVERT GROUND CHANNEL WATER SURFACE
 ** ELEV ELEV ID ELEV (opt.)
 **-----
 "No 1" 0 2621.3 0 "channel14" 0

[HEADWORK]
 **NAME INVERT GROUND CHANNEL FLOW WATER SURFACE
 ** ELEV ELEV ID ID ELEV (opt.)
 **-----
 "No 37" 2739.62 0 "channel 4" 2450 0

[WALLENTANCE]
 **NAME INVERT GROUND CHANNEL LOSS
 ** ELEV ELEV ID COEFFICIENT(opt.)
 **-----

[WALLEXIT]
 **NAME INVERT GROUND CHANNEL LOSS
 ** ELEV ELEV ID COEFFICIENT(opt.)
 **-----

[BRIDGEENTRANCE]
 **NAME INVERT GROUND CHANNEL REDUCTION
 ** ELEV ELEV ID FACTOR(opt.)
 **-----

[BRIDGEEXIT]
 **NAME INVERT GROUND CHANNEL REDUCTION
 ** ELEV ELEV ID FACTOR(opt.)
 **-----

[JOIN]
 **NAME INVERT GROUND CHANNEL LENGTH MANNINGS n NUMBER OF CONFLUENCE
 ** ELEV ELEV ID BRANCHES ANGLE
 **-----

[JUNCTION]

main0626int.wsx								
**Name	INVERT	GROUND	CHANNEL	LENGTH	MANNINGS n	NUMBER OF	CONFLUENCE	FLOW
**-----	ELEV	ELEV	ID			LATERALS	ANGLE	
"No 17"	2663.13	0	"channel10"	10	0.015	1		
"No 17_Lateral1"	2663.42		"channel6"				-60	287
"No 28"	2701.73	0	"channel 4"	36.66	0.015	1		
"No 28_Lateral1"	2701.73		"channel3"				-15	2008
"No 31"	2721.11	0	"channel 4"	26.53	0.015	2		
"No 31_Lateral1"	2721.13		"channel5"				-30	9
"No 31_Lateral2"	2721.13		"channel11"				58	17
"No 34"	2734.24	0	"channel 4"	8	0.015	2		
"No 34_Lateral1"	2734.52		"72 pipe"				30	8
"No 34_Lateral2"	2734.52		"72 pipe"				30	5

[TRANSITION]

**NAME	INVERT	GROUND	CHANNEL	LENGTH	MANNINGS n
**-----	ELEV	ELEV	ID		
"No 2"	2621.65	0	"channel15"	24.86	0.015
"No 3"	2621.81	0	"channel10"	10	0.015
"No 19"	2668.54	0	"channel12"	30	0.023

[REACH]

**NAME	INVERT	GROUND	CHANNEL	LENGTH	MANNINGS n	CURVE	ANGLE	NUMBER
**-----	ELEV	ELEV	ID			(opt)	POINT(opt)	MANHOLES(opt)
"No 4"	2623.18	0	"channel10"	90.31	0.015	0	0	0
"No 5"	2623	0	"Channel10"	2.32	0.015	0	0	0
"No 6"	2625	0	"Channel10"	70.62	0.015	-40.46	0	0
"No 7"	2625.48	0	"Channel10"	17.41	0.015	0	0	0
"No 8"	2627.86	0	"Channel10"	85.3	0.015	48.87	0	0
"No 9"	2631.86	0	"Channel10"	143.47	0.015	0	0	0
"No 10"	2645.03	0	"Channel10"	472.89	0.015	13.91	0	0
"No 11"	2648.24	0	"Channel10"	115.41	0.015	-66.13	0	0
"No 12"	2651.53	0	"Channel10"	118.22	0.015	0	0	0
"No 13"	2655.26	0	"Channel10"	466.14	0.015	0	0	0
"No 14"	2656.61	0	"Channel10"	168.86	0.015	90	0	0
"No 15"	2659.44	0	"Channel10"	565	0.015	0	0	0
"No 16"	2662.94	0	"channel10"	145.16	0.015	0	0	0
"No 18"	2666.75	0	"channel10"	194.84	0.015	0	0	0
"No 20"	2670.81	0	"channel12"	38.03	0.015	0	0	0
"No 21"	2671.71	0	"channel12"	90.08	0.015	34.41	0	0
"No 22"	2675.47	0	"channel12"	375.81	0.015	0	0	0
"No 23"	2676.57	0	"channel12"	109.42	0.015	12.54	0	0
"No 24"	2677.16	0	"channel12"	59.62	0.015	0	0	0
"No 25"	2677.68	0	"channel12"	52.03	0.015	-19.87	0	0
"No 26"	2686	0	"channel12"	616.02	0.015	0	0	0
"No 27"	2700.81	0	"channel12"	251.82	0.023	-20.04	0	0
"No 29"	2710.25	0	"channel 4"	338.86	0.015	-26.97	0	0
"No 30"	2720.45	0	"channel 4"	407.05	0.015	0	0	0
"No 32"	2732.17	0	"channel 4"	613.91	0.015	0	0	0
"No 33"	2734.1	0	"channel 4"	107.29	0.015	40.982	0	0
"No 35"	2738.05	0	"channel 4"	219.12	0.015	0	0	0
"No 36"	2739.62	0	"channel 4"	87.41	0.015	33.388	0	0

[CHANNEL]

**REGULAR TYPES 1-4								
**ID	TYPE	HEIGHT	WIDTH	LEFT	RIGHT	NUMBER	AVG PIER	INVERT
**-----				SLOPE	SLOPE	PIERS	WIDTH	CROSS FALL
"channel 4"	3	10	10	0	0	0	0	0
"channel10"	3	12	25	0	0	1	1	0
"channel16"	4	6	6					
"channel13"	3	8	10	0	0	0	0	0
"channel15"	4	4	4					
"channel111"	3	6	6	0	0	0	0	0
"72 pipe"	4	6	6					
"channel12"	3	12	14	0	0	0	0	0

**IRREGULAR TYPES 5-6

**ID	TYPE	NUMBER	AVG PIER	PIER1	PIER2	PIER3	PIER4	PIER5	PIER6	PIER7	PIER8	PIER9	PIER10
**-----		PIERS	WIDTH	ELEV	ELEV	ELEV	ELEV	ELEV	ELEV	ELEV	ELEV	ELEV	ELEV
"channel14"5		0	0										
"channel15"5		0	0										

[POINT]

**ID	XCOORD	YCOORD
**-----		
"channel14"	0	2648
"channel14"	19.09	2648
"channel14"	50.85	2645
"channel14"	111.11	2621

"channel14"	159.24	2621
"channel14"	186.97	2635.98
"channel14"	248.78	2640

"channel15"	0	2648
"channel15"	11.03	2648
"channel15"	54.93	2638
"channel15"	84.46	2622
"channel15"	136.39	2622
"channel15"	173.21	2640

 Water Surface Profile Gradient (WSPG)
 XP WSPG
 Engine Version 1.3 06/09/2010
 XP Software www.xpsoftware.com

INPUT FILE

 C:\Program Files (x86)\CIVILD\main0626int.wsx
 Computed 06/28/18 12:03:02

TITLE INFORMATION

 GCW #840.050A (The 435 - CCRFCD STORM DRAIN) 0
 MAIN1 TRUNK INTERIM CONDITION
 3rd RTC to TDS

WARNING SUMMARY

 WARNING 47: Junction No 28 has a different channel than its direct downstream element.
 WARNING 15: Invert elevation of element No 5 is not larger than invert elevation of the direct downstream element.
 WARNING 25: Link type element No 16 has different invert elevation than its upstream node.
 WARNING 25: Link type element No 27 has different invert elevation than its upstream node.
 WARNING 25: Link type element No 30 has different invert elevation than its upstream node.
 WARNING 25: Link type element No 33 has different invert elevation than its upstream node.
 WARNING 36: D/S processing stopped in junction No 34 because critical momentum is greater than maximum momentum.
 WARNING 36: D/S processing stopped in junction No 31 because critical momentum is greater than maximum momentum.
 WARNING 36: D/S processing stopped in junction No 28 because critical momentum is greater than maximum momentum.

RESULTS

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Main Line

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Composite Profile:

ELEMENT	TYPE	STATION	INVERT	GROUND	W.S.	DEPTH	Q	VELOC.	VELOC.	ENERGY	SUPER
CRITICAL	FROUDE	SLOPE	NORMAL	CROSS							
NAME			ELEV	ELEV	ELEV				HEAD	GRADE IN	ELEV
DEPTH	NUMBER	DEPTH	SECTION								
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
###											
"No 1"	Outlet	0.00	2621.30	0.00	*2623.898	2.598	4784.00	34.23	18.19	2642.09	0.000
6.118	0.000	0.00000	0.000	Irreg.open							
"No 2"	Transition	24.86	2621.65	0.00	*2624.047	2.397	4784.00	35.27	19.31	2643.36	0.000
5.931	6.015	0.01408	0.000	Irreg.open							
"No 3"	Transition	34.86	2621.81	0.00	*2628.017	6.207	4784.00	32.11	16.01	2644.03	0.000
10.729	2.272	0.01600	0.000	Tr./Rect.closed							
"No 4"	Reach	125.17	2623.18	0.00	*2629.190	6.010	4784.00	33.17	17.08	2646.27	0.000
10.729	2.384	0.01517	7.362	Tr./Rect.closed							
"No 5"	Reach	127.49	2623.00	0.00	*2628.959	5.959	4784.00	33.45	17.37	2646.33	0.000
10.729	2.415	-0.07759	12.000	Tr./Rect.closed							
"No 6"	Reach	198.11	2625.00	0.00	*2630.989	5.989	4784.00	33.28	17.20	2648.19	0.000
10.729	2.397	0.02832	5.810	Tr./Rect.closed							
"No 7"	Reach	215.52	2625.48	0.00	*2631.475	5.995	4784.00	33.25	17.17	2648.64	0.000
10.729	2.393	0.02757	5.869	Tr./Rect.closed							
"No 8"	Reach	300.82	2627.86	0.00	*2633.892	6.032	4784.00	33.04	16.96	2650.85	0.000
10.729	2.371	0.02790	5.843	Tr./Rect.closed							
"No 9"	Reach	444.29	2631.86	0.00	*2637.980	6.120	4784.00	32.57	16.48	2654.45	0.000
10.729	2.320	0.02788	5.845	Tr./Rect.closed							
	"i.p."	650.19	2637.59	0.00	*2643.927	6.333	4784.00	31.48	15.39	2659.31	0.000
10.729	2.204	0.02785	5.847	Tr./Rect.closed							
	"i.p."	813.76	2642.15	0.00	*2648.791	6.642	4784.00	30.01	13.99	2662.78	0.000
10.729	2.052	0.02785	5.847	Tr./Rect.closed							
"No 10"	Reach	917.18	2645.03	0.00	*2651.996	6.966	4784.00	28.62	12.72	2664.71	0.000
10.729	1.911	0.02785	5.847	Tr./Rect.closed							
	"i.p."	976.86	2646.69	0.00	*2653.927	7.237	4784.00	27.54	11.78	2665.71	0.000
10.729	1.804	0.02781	5.850	Tr./Rect.closed							
"No 11"	Reach	1032.59	2648.24	0.00	*2655.830	7.590	4784.00	26.26	10.71	2666.54	0.000
10.729	1.680	0.02781	5.850	Tr./Rect.closed							
	"i.p."	1059.02	2648.98	0.00	*2656.788	7.813	4784.00	25.51	10.11	2666.90	0.000
10.729	1.609	0.02783	5.849	Tr./Rect.closed							
	"i.p."	1093.54	2649.94	0.00	*2658.130	8.194	4784.00	24.33	9.19	2667.32	0.000
10.729	1.498	0.02783	5.849	Tr./Rect.closed							
	"i.p."	1119.18	2650.65	0.00	*2659.244	8.594	4784.00	23.19	8.35	2667.60	0.000
10.729	1.394	0.02783	5.849	Tr./Rect.closed							
	"i.p."	1137.84	2651.17	0.00	*2660.182	9.013	4784.00	22.12	7.59	2667.78	0.000
10.729	1.298	0.02783	5.849	Tr./Rect.closed							

"No 12"	Reach	1150.81	2651.53	0.00	*2660.983	9.453	4784.00	21.09	6.90	2667.89	0.000
10.729	1.209	0.02783	5.849	Tr./Rect.closed							
	"i.p."	1173.26	2651.71	0.00	*2661.163	9.453	4784.00	21.09	6.90	2668.07	0.000
10.729	1.209	0.00800	9.453	Tr./Rect.closed							
"No 13"	Reach	1616.95	2655.26	0.00	*2664.628	9.368	4784.00	21.28	7.03	2671.66	0.000
10.729	1.225	0.00800	9.453	Tr./Rect.closed							
"No 14"	Reach	1785.81	2656.61	0.00	*2665.882	9.272	4784.00	21.50	7.18	2673.06	0.000
10.729	1.244	0.00799	9.457	Tr./Rect.closed							
	"i.p."	1846.72	2656.92	0.00	*2665.824	8.909	4784.00	22.38	7.77	2673.60	0.000
10.729	1.321	0.00501	11.412	Tr./Rect.closed							
	"i.p."	1920.97	2657.29	0.00	*2665.781	8.494	4784.00	23.47	8.55	2674.33	0.000
10.729	1.419	0.00501	11.412	Tr./Rect.closed							
	"i.p."	1995.54	2657.66	0.00	*2665.759	8.099	4784.00	24.61	9.41	2675.17	0.000
10.729	1.524	0.00501	11.412	Tr./Rect.closed							
	"i.p."	2069.51	2658.03	0.00	*2665.753	7.722	4784.00	25.81	10.35	2676.10	0.000
10.729	1.637	0.00501	11.412	Tr./Rect.closed							
	"i.p."	2142.32	2658.40	0.00	*2665.758	7.363	4784.00	27.07	11.38	2677.14	0.000
10.729	1.758	0.00501	11.412	Tr./Rect.closed							
	"i.p."	2213.61	2658.75	0.00	*2665.773	7.020	4784.00	28.40	12.52	2678.29	0.000
10.729	1.889	0.00501	11.412	Tr./Rect.closed							
	"i.p."	2283.15	2659.10	0.00	*2665.794	6.693	4784.00	29.78	13.77	2679.57	0.000
10.729	2.029	0.00501	11.412	Tr./Rect.closed							
"No 15"	Reach	2350.81	2659.44	0.00	*2665.822	6.382	4784.00	31.23	15.15	2680.97	0.000
10.729	2.179	0.00501	11.412	Tr./Rect.closed							
"No 16"	Reach	2495.97	2662.94	0.00	*2669.421	6.481	4784.00	30.76	14.69	2684.11	0.000
10.729	2.129	0.02411	6.172	Tr./Rect.closed							
"No 17"	Junction	2505.97	2663.13	0.00	*2668.751	5.621	4497.00	33.33	17.25	2686.00	0.000
10.295	0.000	0.01900	0.000	Tr./Rect.closed							
	"i.p."	2576.90	2664.45	0.00	*2669.941	5.493	4497.00	34.11	18.07	2688.01	0.000
10.295	2.565	0.01858	6.499	Tr./Rect.closed							
"No 18"	Reach	2700.81	2666.75	0.00	*2671.988	5.238	4497.00	35.77	19.87	2691.86	0.000
10.295	2.755	0.01858	6.499	Tr./Rect.closed							
"No 19"	Transition	2730.81	2668.54	0.00	*2678.801	10.261	4497.00	31.31	15.22	2694.02	0.000
12.000	1.722	0.05967	0.000	Tr./Rect.closed							
	"i.p."	2735.77	2668.84	0.00	*2679.213	10.377	4497.00	30.95	14.88	2694.09	0.000
12.000	1.693	0.05969	6.053	Tr./Rect.closed							
	"i.p."	2754.16	2669.93	0.00	*2680.817	10.883	4497.00	29.51	13.53	2694.34	0.000
12.000	1.577	0.05969	6.053	Tr./Rect.closed							
"No 20"	Reach	2768.84	2670.81	0.00	*2682.225	11.415	4497.00	28.14	12.30	2694.52	0.000
12.000	1.468	0.05969	6.053	Tr./Rect.closed							
"No 21"	Reach	2858.92	2671.71	0.00	*2683.006	11.296	4497.00	28.44	12.56	2695.56	0.000
12.000	1.491	0.00999	12.000	Tr./Rect.closed							
	"i.p."	2968.92	2672.81	0.00	*2683.941	11.131	4497.00	28.86	12.93	2696.87	0.000
12.000	1.524	0.01001	12.000	Tr./Rect.closed							
"No 22"	Reach	3234.73	2675.47	0.00	*2686.083	10.613	4497.00	30.27	14.23	2700.31	0.000
12.000	1.637	0.01001	12.000	Tr./Rect.closed							
"No 23"	Reach	3344.15	2676.57	0.00	*2686.932	10.362	4497.00	31.00	14.92	2701.85	0.000
12.000	1.697	0.01005	12.000	Tr./Rect.closed							
"No 24"	Reach	3403.77	2677.16	0.00	*2687.371	10.211	4497.00	31.46	15.37	2702.74	0.000
12.000	1.735	0.00990	12.000	Tr./Rect.closed							
"No 25"	Reach	3455.80	2677.68	0.00	*2687.756	10.076	4497.00	31.88	15.78	2703.54	0.000
12.000	1.770	0.00999	12.000	Tr./Rect.closed							
	"i.p."	3492.25	2678.17	0.00	*2688.211	10.039	4497.00	32.00	15.90	2704.11	0.000
12.000	1.780	0.01351	10.672	Tr./Rect.closed							
	"i.p."	3833.60	2682.78	0.00	*2692.354	9.572	4497.00	33.56	17.49	2709.84	0.000
12.000	1.912	0.01351	10.672	Tr./Rect.closed							
"No 26"	Reach	4071.82	2686.00	0.00	*2695.126	9.126	4497.00	35.20	19.24	2714.36	0.000
12.000	2.053	0.01351	10.672	Tr./Rect.closed							
	"i.p."	4144.73	2690.29	0.00	*2699.743	9.455	4497.00	33.97	17.92	2717.66	0.000
12.000	1.947	0.05881	8.394	Tr./Rect.closed							
	"i.p."	4209.35	2694.09	0.00	*2704.005	9.917	4497.00	32.39	16.29	2720.30	0.000
12.000	1.813	0.05881	8.394	Tr./Rect.closed							
	"i.p."	4253.21	2696.67	0.00	*2707.069	10.401	4497.00	30.88	14.81	2721.88	0.000
12.000	1.688	0.05881	8.394	Tr./Rect.closed							
	"i.p."	4284.46	2698.51	0.00	*2709.414	10.908	4497.00	29.45	13.46	2722.88	0.000
12.000	1.571	0.05881	8.394	Tr./Rect.closed							
	"i.p."	4307.17	2699.84	0.00	*2711.282	11.441	4497.00	28.08	12.24	2723.52	0.000
12.000	1.463	0.05881	8.394	Tr./Rect.closed							
"No 27"	Reach	4323.64	2700.81	0.00	*2712.809	11.999	4497.00	26.77	11.13	2723.94	0.000
12.000	1.362	0.05881	8.394	Tr./Rect.closed							
"No 28"	Junction	4360.30	2701.73	0.00	*2715.667	13.937	2489.00	24.95	9.67	2725.34	0.000
10.000	0.000	0.02510	0.000	Tr./Rect.closed							
"No 29"	Reach	4699.16	2710.25	0.00	*2723.083	12.833	2489.00	24.95	9.67	2732.75	0.000
10.000	1.392	0.02514	7.593	Tr./Rect.closed							
"No 30"	Reach	5106.21	2720.45	0.00	*2730.719	10.269	2489.00	24.95	9.67	2740.39	0.000
10.000	1.392	0.02506	7.603	Tr./Rect.closed							
"No 31"	Junction	5132.74	2721.11	0.00	*2731.610	10.500	2463.00	24.69	9.47	2741.08	0.000
10.000	0.000	0.02488	0.000	Tr./Rect.closed							
"No 32"	Reach	5746.65	2732.17	0.00	*2742.888	10.718	2463.00	24.69	9.47	2752.35	0.000
10.000	1.378	0.01802	8.599	Tr./Rect.closed							
"No 33"	Reach	5853.94	2734.10	0.00	*2746.137	12.037	2463.00	24.69	9.47	2755.60	0.000
10.000	1.378	0.01799	8.604	Tr./Rect.closed							
"No 34"	Junction	5861.94	2734.24	0.00	*2746.481	12.241	2450.00	24.56	9.37	2755.85	0.000
10.000	0.000	0.01750	0.000	Tr./Rect.closed							
"No 35"	Reach	6081.06	2738.05	0.00	*2750.464	12.414	2450.00	24.56	9.37	2759.83	0.000
10.000	1.370	0.01739	8.685	Tr./Rect.closed							
"No 36"	Reach	6168.47	2739.62	0.00	*2753.194	13.574	2450.00	24.56	9.37	2762.56	0.000

10.000	1.370	0.01796	8.573	Tr./Rect.closed								
"No 37"	Headwrk	6168.47	2739.62	0.00	*2753.194	13.574	2450.00	24.56	9.37	2762.56	0.000	
10.000	0.000	0.00000	0.000	Tr./Rect.closed								

*) in the W.S.ELEV column indicates flooding, it is set whenever W.S.ELEV > GROUND ELEV
i.p. = intermediate point processing results for reaches

BOX CULVERT

20'X14' RCB

INPUT

Width of Box	20.00 ft
Height of Box	14.00 ft
Number of Barrels	1
Length	10.00 ft
Slope	1.10 %
Manning's 'n'	0.015
Flow "Q"	2450 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

45d WWall	12.40 ft
Sq. Edge	13.17 ft
Beveled	12.21 ft
Tapered	11.72 ft

OUTLET

Head Water	12.38 ft
Critical	7.75 ft
Velocity	8.75 ft/s

Non Standard Box Span



13.2-ft below top of RCB, meets headwater criteria.

13.2-ft inlet control headwater is approximately outlet control WSPG WSE: therefore, size of RCB inlet OK.

Section 700 - Open Channels**706.1.1.2 Transition Length**

The length of the transition sections should be long enough to keep the streamlines smooth and nearly parallel throughout the expanding (contracting) section. Experimental data and performance of existing structures have to be used to estimate the minimum transition length necessary to maintain the stated flow conditions. Based on this information, the minimum length of the transition section shall be as follows:

$$L_t = \geq 0.5 L_c (T_w) \quad 0.5 * 4.5 (10) = 22.5 \text{ ft} \quad (739)$$

Where L_t = Minimum Transition Length (ft)

L_c = Length Coefficient

T_w = Difference in the Top Width of the Normal Water Surface Upstream and Downstream of the Transition

For an approach flow velocity less than 12 feet per second, $L_c = 4.5$. This represents a 4.5 (length) to 1.0 (width) wall expansion or contraction with the angle of expansion or contraction of 12.5 degrees from the channel centerline. For an approach flow velocity equal to or greater than 12 feet per second, $L_c = 10.0$. This represents a 10.0 (length) to 1.0 (width) expansion or contraction with the angle of expansion or contraction of about 5.75 degrees from the channel centerline.

The transition length equation is not applicable to cylinder-quadrant or square-ended transitions.

706.1.2 Bends

The allowed radius of curvature in sub-critical channels is based on a theoretical maximum allowed rise in the super-elevated water surface of 0.5 feet. Therefore, the minimum allowed radius of curvature of the channel centerline shall be determined from the following equation:

$$r = C (V^2 T_w) / S_e (g) \quad (740)$$

Where r = Radius of Curvature (ft)

C = Super-Elevation Coefficient (= 1 for Sub-Critical Flow)

T1 THE SEVENTY - THE 435 (PHASE 1), GCW JOB NO. 840-050 0
 T2 3RD RESPONSE TO CLV COMMENTS
 T3 MAIN2 FACILITY (CCRFGD 'APP2' MPU FACILITY)
 SO -2775.6102701.730 1 2715.667
 R -2648.9802712.970 1 .024 64.780 .000 0
 R -2556.6802716.660 1 .015 .000 .000 0
 R -2435.6102721.500 1 .015 -61.936 .000 0
 R -2218.9802726.000 1 .015 .000 .000 0
 R -2160.3602727.220 1 .015 29.988 .000 0
 R -1847.1002733.740 1 .015 .000 .000 0
 R -1764.2102734.560 1 .015 -42.404 .000 0
 R -1468.1802740.500 1 .015 .000 .000 0
 SH -1468.1802740.500 1 .000
 CD 1 3 0 .000 8.000 10.000 .000 .000 .00
 Q 2004.000 .0

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
-2775.610	2701.730	13.937	2715.667	2004.00	25.05	9.74	2725.41	.00	8.00	10.00	8.000	10.000	.00	0 .0
43.633	.0888					.0564	2.46	.00	1.56	5.66	.024	.00	.00	BOX
-2731.977	2705.603	13.096	2718.699	2004.00	25.05	9.74	2728.44	.00	8.00	10.00	8.000	10.000	.00	0 .0
HYDRAULIC JUMP														
-2731.977	2705.603	5.904	2711.507	2004.00	33.94	17.89	2729.40	8.00	8.00	10.00	8.000	10.000	.00	0 .0
82.997	.0888					.0766	6.36	8.00	2.46	5.66	.024	.00	.00	BOX
-2648.980	2712.970	6.084	2719.054	2004.00	32.94	16.85	2735.90	.00	8.00	10.00	8.000	10.000	.00	0 .0
92.300	.0400					.0272	2.51	6.08	2.35	5.37	.015	.00	.00	BOX
-2556.680	2716.660	6.366	2723.026	2004.00	31.48	15.39	2738.41	8.00	8.00	10.00	8.000	10.000	.00	0 .0
3.334	.0400					.0255	.09	8.00	2.20	5.37	.015	.00	.00	BOX
-2553.345	2716.793	6.379	2723.172	2004.00	31.42	15.33	2738.50	8.00	8.00	10.00	8.000	10.000	.00	0 .0
67.630	.0400					.0240	1.62	8.00	2.19	5.37	.015	.00	.00	BOX
-2485.715	2719.497	6.690	2726.187	2004.00	29.96	13.93	2740.12	8.00	8.00	10.00	8.000	10.000	.00	0 .0
50.105	.0400					.0212	1.06	8.00	2.04	5.37	.015	.00	.00	BOX
-2435.610	2721.500	7.016	2728.516	2004.00	28.56	12.67	2741.18	.00	8.00	10.00	8.000	10.000	.00	0 .0
216.630	.0208					.0196	4.24	7.02	1.90	6.90	.015	.00	.00	BOX
-2218.980	2726.000	7.121	2733.121	2004.00	28.14	12.30	2745.42	8.00	8.00	10.00	8.000	10.000	.00	0 .0
58.620	.0208					.0190	1.12	8.00	1.86	6.90	.015	.00	.00	BOX

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
-2160.360	2727.220	7.164	2734.384	2004.00	27.97	12.15	2746.53	8.00	8.00	10.00	8.000	10.000	.00	0 .0
HYDRAULIC DROP														
-2160.360	2727.220	10.763	2737.983	2004.00	25.05	9.74	2747.73	.00	8.00	10.00	8.000	10.000	.00	0 .0
313.260	.0208					.0220	6.91	10.76	1.56	6.90	.015	.00	.00	BOX
-1847.100	2733.740	11.150	2744.890	2004.00	25.05	9.74	2754.63	.00	8.00	10.00	8.000	10.000	.00	0 .0
82.890	.0099					.0220	1.83	.00	1.56	8.00	.015	.00	.00	BOX
-1764.210	2734.560	13.495	2748.055	2004.00	25.05	9.74	2757.80	.00	8.00	10.00	8.000	10.000	.00	0 .0
296.030	.0201					.0220	6.53	13.50	1.56	7.00	.015	.00	.00	BOX
-1468.180	2740.500	14.082	2754.582	2004.00	25.05	9.74	2764.33	.00	8.00	10.00	8.000	10.000	.00	0 .0

FILE: MAIN2024R.WSW
 MAIN2024R.EDT
Date: 6-25-2018 Time: 2:58:14

W S P G W - EDIT LISTING - Version 14.10
 WATER SURFACE PROFILE - CHANNEL DEFINITION LISTING
PAGE 1

CARD	SECT	CHN	NO OF	AVE PIER	HEIGHT 1	BASE	ZL	ZR	INV	Y(1)	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)	Y(10)
CODE	NO	TYPE	PIER/PIP	WIDTH	DIAMETER	WIDTH			DROP										

CD 1 3 0 .000 8.000 10.000 .000 .000 .00
 W S P G W
PAGE NO 1

WATER SURFACE PROFILE - TITLE CARD LISTING

HEADING LINE NO 1 IS - THE SEVENTY - THE 435 (PHASE 1), GCW JOB NO. 840-050

HEADING LINE NO 2 IS - 3RD RESPONSE TO CLV COMMENTS

HEADING LINE NO 3 IS - MAIN2 FACILITY (CCRFGD 'APP2' MPU FACILITY)

W S P G W
 PAGE NO 2

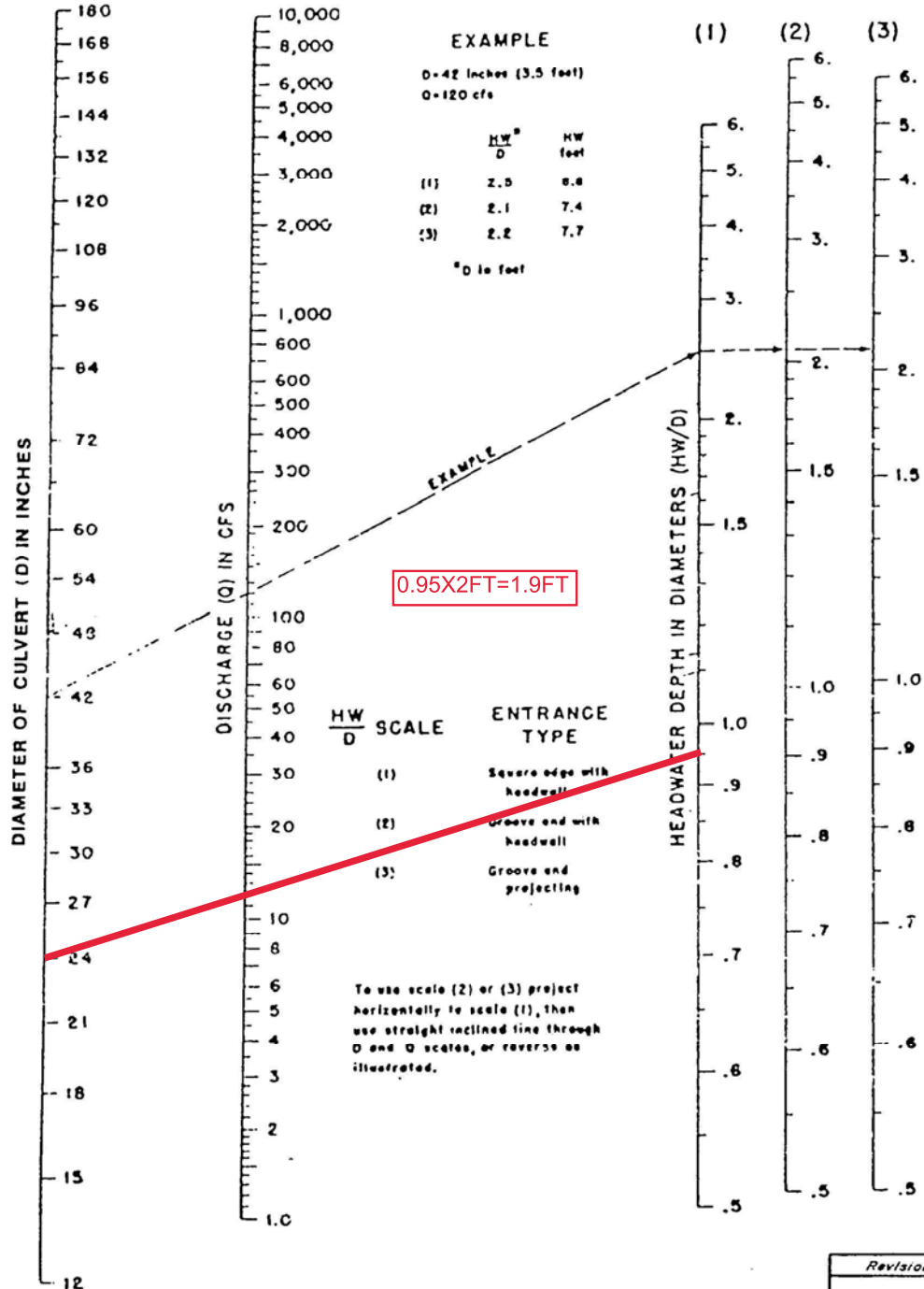
WATER SURFACE PROFILE - ELEMENT CARD LISTING

ELEMENT NO	IS A	SYSTEM OUTLET	U/S DATA	STATION	INVERT	SECT	W S ELEV	RADIUS	ANGLE	ANG PT	MAN H
1	IS A	SYSTEM OUTLET	U/S DATA	STATION	INVERT	SECT	2715.667				
				-2775.610	2701.730	1					
2	IS A	REACH	U/S DATA	STATION	INVERT	SECT					
				-2648.980	2712.970	1					
3	IS A	REACH	U/S DATA	STATION	INVERT	SECT					
				-2556.680	2716.660	1					
4	IS A	REACH	U/S DATA	STATION	INVERT	SECT					
				-2435.610	2721.500	1					
5	IS A	REACH	U/S DATA	STATION	INVERT	SECT					
				-2218.980	2726.000	1					
6	IS A	REACH	U/S DATA	STATION	INVERT	SECT					
				-2160.360	2727.220	1					
7	IS A	REACH	U/S DATA	STATION	INVERT	SECT					
				-1847.100	2733.740	1					
8	IS A	REACH	U/S DATA	STATION	INVERT	SECT					
				-1764.210	2734.560	1					
9	IS A	REACH	U/S DATA	STATION	INVERT	SECT					
				-1468.180	2740.500	1					
10	IS A	SYSTEM HEADWORKS	U/S DATA	STATION	INVERT	SECT					
				-1468.180	2740.500	1					

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

NOMOGRAPH - INLET CONTROL RCP

24-INCH RCP



Revision	Date

WRC
ENGINEERING

REFERENCE:

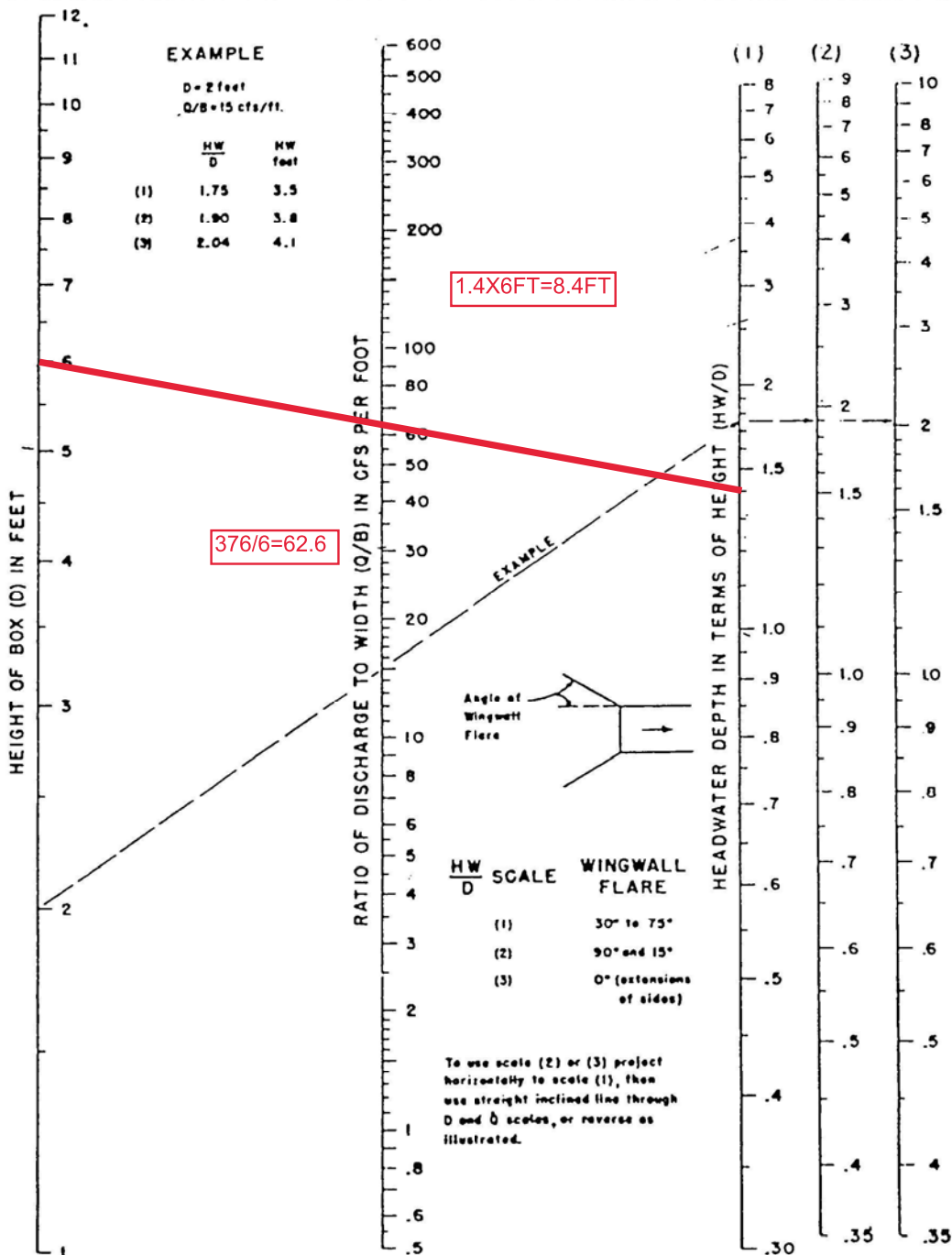
USDOT, FHWA, HDS, No. 5, 1985

FIGURE 1005

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

6'X6' RCB

NOMOGRAPH - INLET CONTROL BOX CULVERT



Revision	Date

WRC
ENGINEERING

REFERENCE:
USDOT, FHWA, HDS No.5, 1985

FIGURE 1004

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

NOMOGRAPH - INLET CONTROL RCP

72-INCH RCP
(FACILITY 10C)

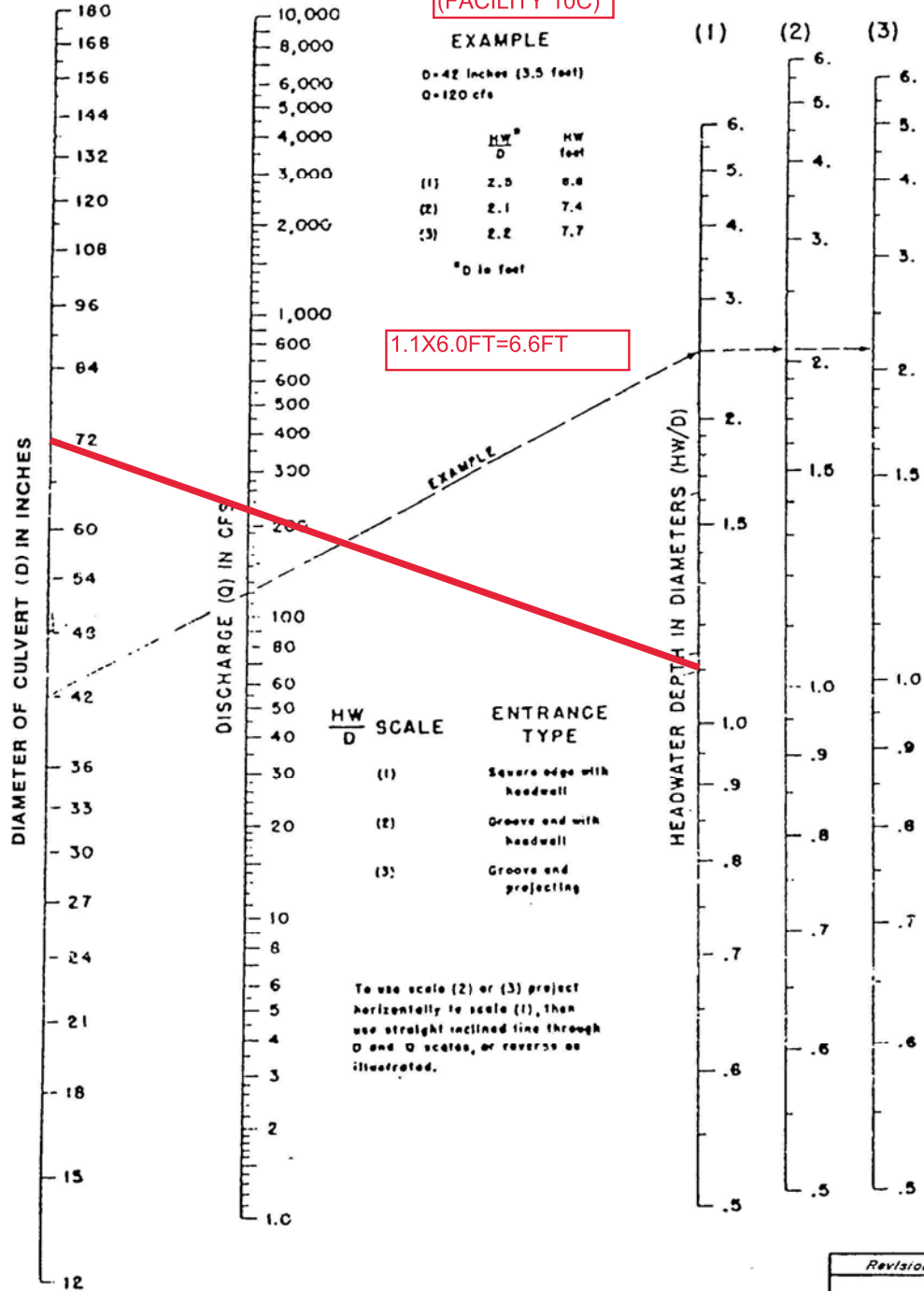
EXAMPLE

D = 42 inches (3.5 feet)
Q = 120 cfs

	$\frac{HW}{D}$	HW feet
(1)	2.5	8.8
(2)	2.1	7.4
(3)	2.2	7.7

^aD in feet

$$1.1 \times 6.0 \text{ FT} = 6.6 \text{ FT}$$



Revision	Date

WRC
ENGINEERING

REFERENCE:

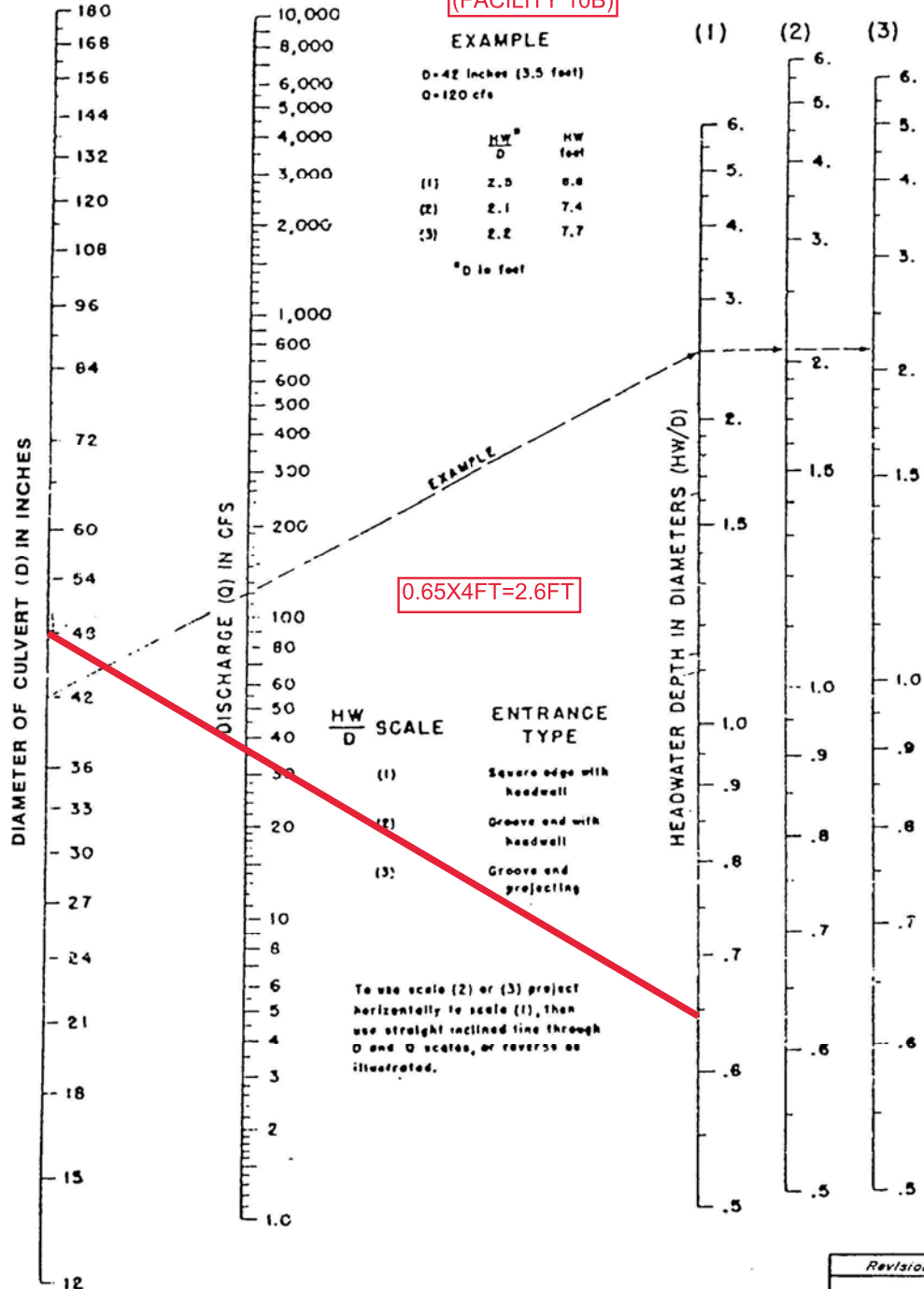
USDOT, FHWA, HDS, No. 5, 1985

FIGURE 1005

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

NOMOGRAPH - INLET CONTROL RCP

48-INCH RCP
(FACILITY 10B)



Revision	Date

WRC
ENGINEERING

REFERENCE:

USDOT, FHWA, HDS, No. 5, 1985

FIGURE 1005

Worksheet for 72-INCH RCP (FACILITY 5)

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	17.09	%
Diameter	6.00	ft
Discharge	377.00	ft³/s

Results

Normal Depth	1.89	ft
Flow Area	7.64	ft²
Wetted Perimeter	7.15	ft
Hydraulic Radius	1.07	ft
Top Width	5.57	ft
Critical Depth	5.22	ft
Percent Full	31.5	%
Critical Slope	0.00723	ft/ft
Velocity	49.37	ft/s
Velocity Head	37.87	ft
Specific Energy	39.76	ft
Froude Number	7.44	
Maximum Discharge	1883.23	ft³/s
Discharge Full	1750.69	ft³/s
Slope Full	0.00793	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	31.51	%
Downstream Velocity	Infinity	ft/s

Worksheet for 72-INCH RCP (FACILITY 5)

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.89	ft
Critical Depth	5.22	ft
Channel Slope	17.09	%
Critical Slope	0.00723	ft/ft

Cross Section for 72-INCH RCP (FACILITY 5)

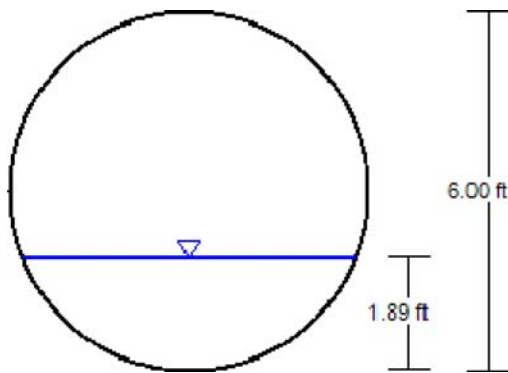
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	17.09 %
Normal Depth	1.89 ft
Diameter	6.00 ft
Discharge	377.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for 72-INCH RCP (FACILITY 6)

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	11.65	%
Diameter	6.00	ft
Discharge	205.00	ft³/s

Results

Normal Depth	1.53	ft
Flow Area	5.67	ft²
Wetted Perimeter	6.34	ft
Hydraulic Radius	0.89	ft
Top Width	5.23	ft
Critical Depth	3.92	ft
Percent Full	25.4	%
Critical Slope	0.00405	ft/ft
Velocity	36.18	ft/s
Velocity Head	20.34	ft
Specific Energy	21.87	ft
Froude Number	6.13	
Maximum Discharge	1554.87	ft³/s
Discharge Full	1445.44	ft³/s
Slope Full	0.00234	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	25.44	%
Downstream Velocity	Infinity	ft/s

Worksheet for 72-INCH RCP (FACILITY 6)

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.53	ft
Critical Depth	3.92	ft
Channel Slope	11.65	%
Critical Slope	0.00405	ft/ft

Cross Section for 72-INCH RCP (FACILITY 6)

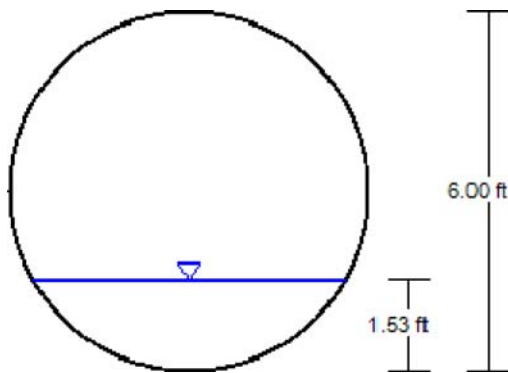
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	11.65 %
Normal Depth	1.53 ft
Diameter	6.00 ft
Discharge	205.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for 24-INCH RCP (FACILITY 7A)

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	11.54	%
Diameter	2.00	ft
Discharge	12.00	ft ³ /s

Results

Normal Depth	0.53	ft
Flow Area	0.67	ft ²
Wetted Perimeter	2.17	ft
Hydraulic Radius	0.31	ft
Top Width	1.77	ft
Critical Depth	1.24	ft
Percent Full	26.7	%
Critical Slope	0.00558	ft/ft
Velocity	17.80	ft/s
Velocity Head	4.92	ft
Specific Energy	5.46	ft
Froude Number	5.08	
Maximum Discharge	82.66	ft ³ /s
Discharge Full	76.85	ft ³ /s
Slope Full	0.00281	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	26.71	%
Downstream Velocity	Infinity	ft/s

Worksheet for 24-INCH RCP (FACILITY 7A)

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.53	ft
Critical Depth	1.24	ft
Channel Slope	11.54	%
Critical Slope	0.00558	ft/ft

Cross Section for 24-INCH RCP (FACILITY 7A)

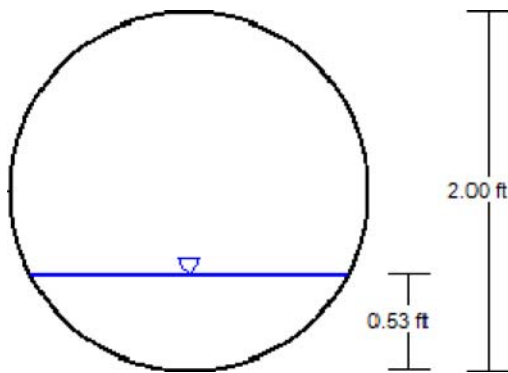
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	11.54 %
Normal Depth	0.53 ft
Diameter	2.00 ft
Discharge	12.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for 6'X6' RCB

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	20.81	%
Height	6.00	ft
Bottom Width	6.00	ft
Discharge	376.00	ft³/s

Results

Normal Depth	1.29	ft
Flow Area	7.73	ft²
Wetted Perimeter	8.58	ft
Hydraulic Radius	0.90	ft
Top Width	6.00	ft
Critical Depth	4.96	ft
Percent Full	21.5	%
Critical Slope	0.00530	ft/ft
Velocity	48.65	ft/s
Velocity Head	36.78	ft
Specific Energy	38.07	ft
Froude Number	7.56	
Discharge Full	2459.71	ft³/s
Slope Full	8.90563	ft/ft
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	21.47	%
Downstream Velocity	Infinity	ft/s

Worksheet for 6'X6' RCB

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.29	ft
Critical Depth	4.96	ft
Channel Slope	20.81	%
Critical Slope	0.00530	ft/ft

Cross Section for 6'X6' RCB

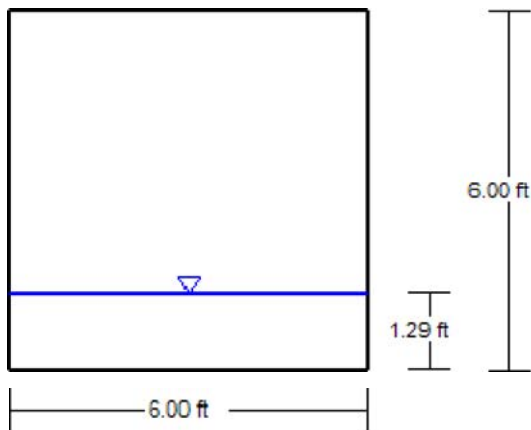
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	20.81 %
Normal Depth	1.29 ft
Height	6.00 ft
Bottom Width	6.00 ft
Discharge	376.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for 48-INCH RCP (FACILITY 8A)

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	12.79	%
Diameter	4.00	ft
Discharge	34.00	ft ³ /s

Results

Normal Depth	0.70	ft
Flow Area	1.47	ft ²
Wetted Perimeter	3.45	ft
Hydraulic Radius	0.43	ft
Top Width	3.03	ft
Critical Depth	1.73	ft
Percent Full	17.4	%
Critical Slope	0.00369	ft/ft
Velocity	23.16	ft/s
Velocity Head	8.34	ft
Specific Energy	9.03	ft
Froude Number	5.87	
Maximum Discharge	552.57	ft ³ /s
Discharge Full	513.69	ft ³ /s
Slope Full	0.00056	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	17.43	%
Downstream Velocity	Infinity	ft/s

Worksheet for 48-INCH RCP (FACILITY 8A)

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.70	ft
Critical Depth	1.73	ft
Channel Slope	12.79	%
Critical Slope	0.00369	ft/ft

Cross Section for 48-INCH RCP (FACILITY 8A)

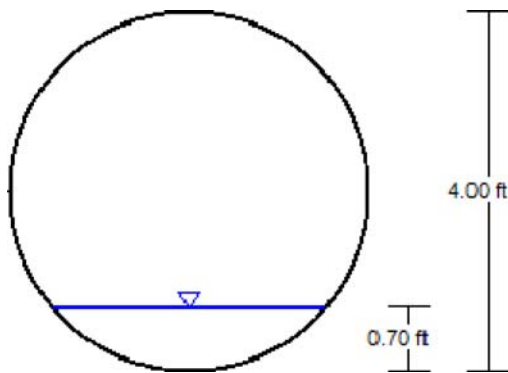
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	12.79 %
Normal Depth	0.70 ft
Diameter	4.00 ft
Discharge	34.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for 72-INCH RCP (FACILITY 10C)

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	3.30	%
Diameter	6.00	ft
Discharge	236.00	ft³/s

Results

Normal Depth	2.28	ft
Flow Area	9.86	ft²
Wetted Perimeter	7.97	ft
Hydraulic Radius	1.24	ft
Top Width	5.82	ft
Critical Depth	4.21	ft
Percent Full	38.0	%
Critical Slope	0.00441	ft/ft
Velocity	23.93	ft/s
Velocity Head	8.90	ft
Specific Energy	11.18	ft
Froude Number	3.24	
Maximum Discharge	827.54	ft³/s
Discharge Full	769.30	ft³/s
Slope Full	0.00311	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	38.01	%
Downstream Velocity	Infinity	ft/s

Worksheet for 72-INCH RCP (FACILITY 10C)

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	2.28	ft
Critical Depth	4.21	ft
Channel Slope	3.30	%
Critical Slope	0.00441	ft/ft

Cross Section for 72-INCH RCP (FACILITY 10C)

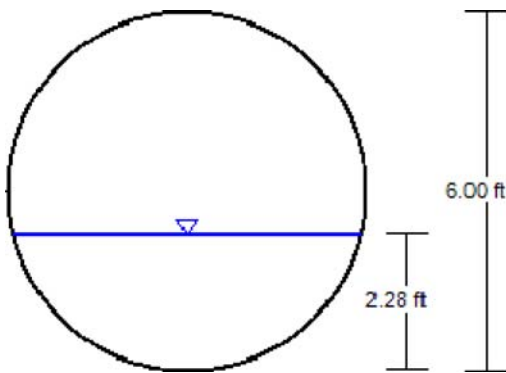
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	3.30 %
Normal Depth	2.28 ft
Diameter	6.00 ft
Discharge	236.00 ft³/s

Cross Section Image



V: 1
H: 1

Worksheet for 48-INCH RCP (FACILITY 10B)

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	8.19	%
Diameter	4.00	ft
Discharge	36.00	ft ³ /s

Results

Normal Depth	0.80	ft
Flow Area	1.79	ft ²
Wetted Perimeter	3.71	ft
Hydraulic Radius	0.48	ft
Top Width	3.20	ft
Critical Depth	1.79	ft
Percent Full	20.0	%
Critical Slope	0.00372	ft/ft
Velocity	20.12	ft/s
Velocity Head	6.29	ft
Specific Energy	7.09	ft
Froude Number	4.74	
Maximum Discharge	442.18	ft ³ /s
Discharge Full	411.06	ft ³ /s
Slope Full	0.00063	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	20.00	%
Downstream Velocity	Infinity	ft/s

Worksheet for 48-INCH RCP (FACILITY 10B)

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.80	ft
Critical Depth	1.79	ft
Channel Slope	8.19	%
Critical Slope	0.00372	ft/ft

Cross Section for 48-INCH RCP (FACILITY 10B)

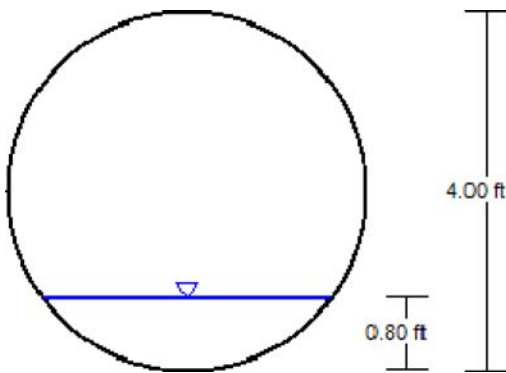
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	8.19 %
Normal Depth	0.80 ft
Diameter	4.00 ft
Discharge	36.00 ft³/s

Cross Section Image



V: 1
H: 1

Worksheet for 18-INCH RCP

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	13.51	%
Diameter	2.00	ft
Discharge	2.00	ft ³ /s

Results

Normal Depth	0.21	ft
Flow Area	0.18	ft ²
Wetted Perimeter	1.33	ft
Hydraulic Radius	0.14	ft
Top Width	1.24	ft
Critical Depth	0.49	ft
Percent Full	10.7	%
Critical Slope	0.00448	ft/ft
Velocity	11.07	ft/s
Velocity Head	1.91	ft
Specific Energy	2.12	ft
Froude Number	5.11	
Maximum Discharge	89.44	ft ³ /s
Discharge Full	83.15	ft ³ /s
Slope Full	0.00008	ft/ft
Flow Type	SuperCritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	10.70	%
Downstream Velocity	Infinity	ft/s

Worksheet for 18-INCH RCP

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	0.21	ft
Critical Depth	0.49	ft
Channel Slope	13.51	%
Critical Slope	0.00448	ft/ft

Cross Section for 18-INCH RCP

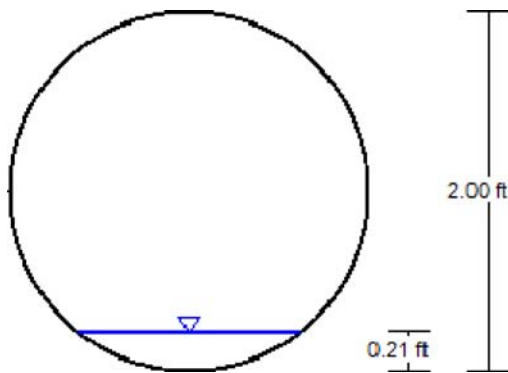
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	13.51 %
Normal Depth	0.21 ft
Diameter	2.00 ft
Discharge	2.00 ft ³ /s

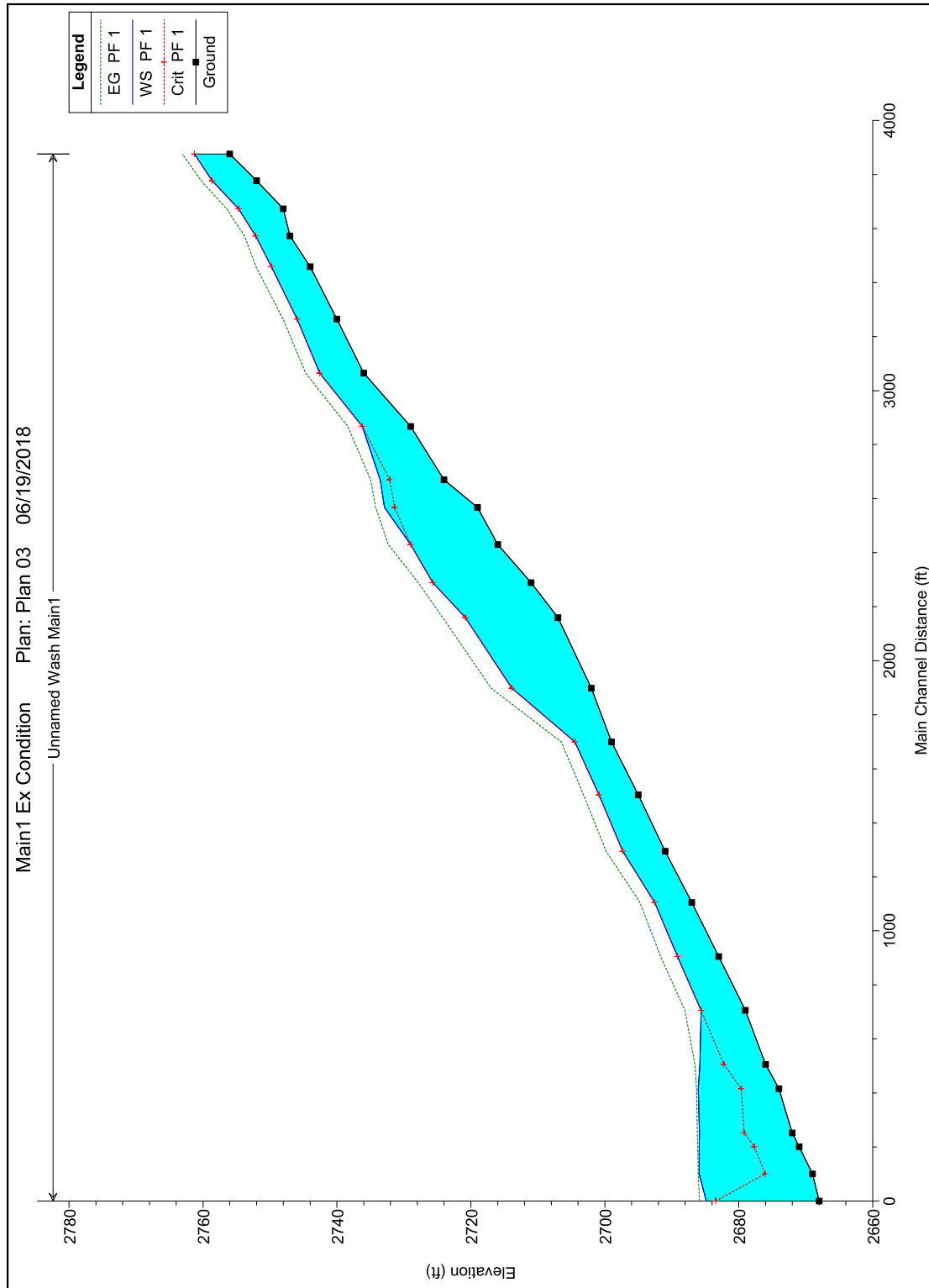
Cross Section Image



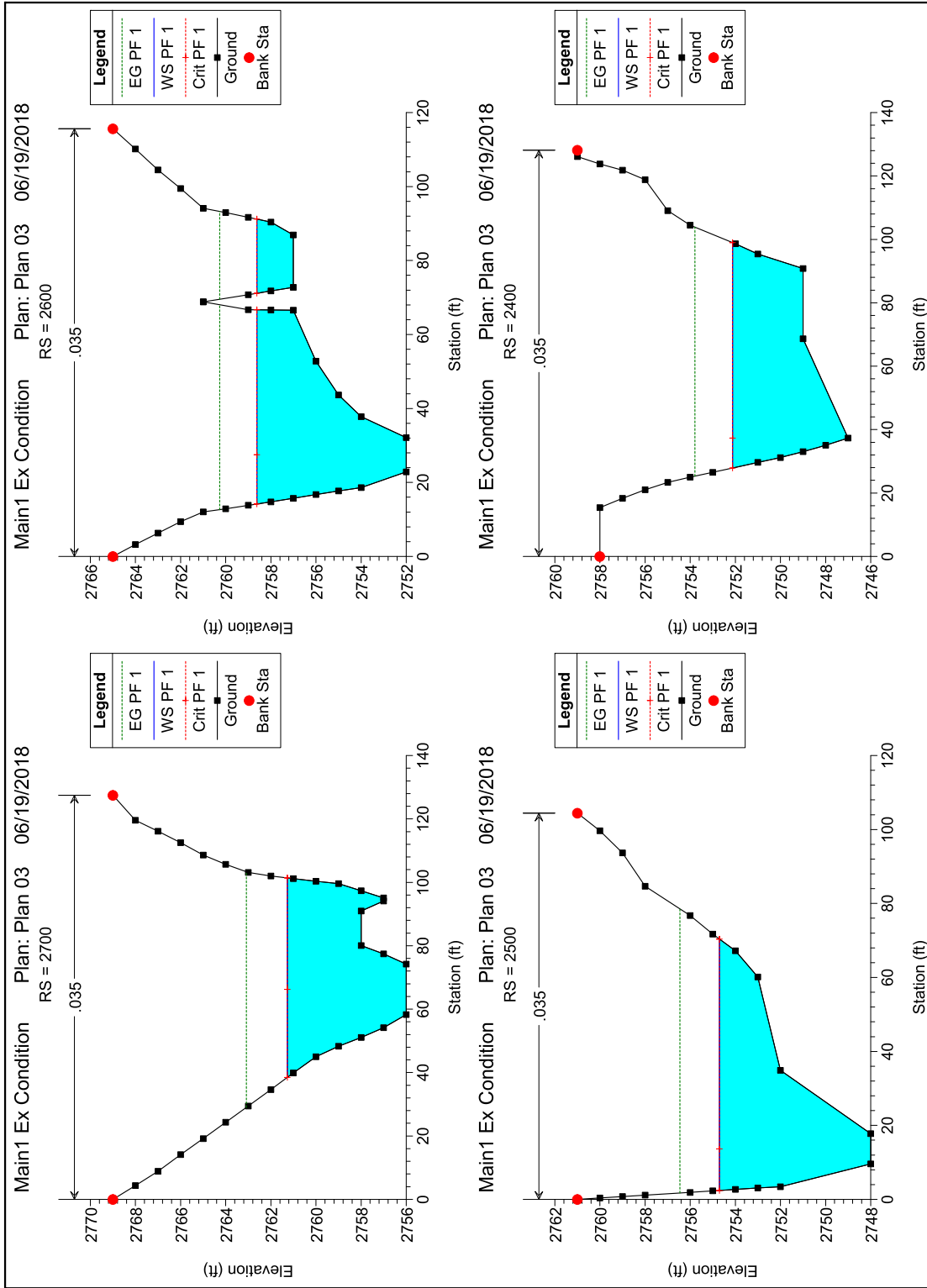
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H: 1

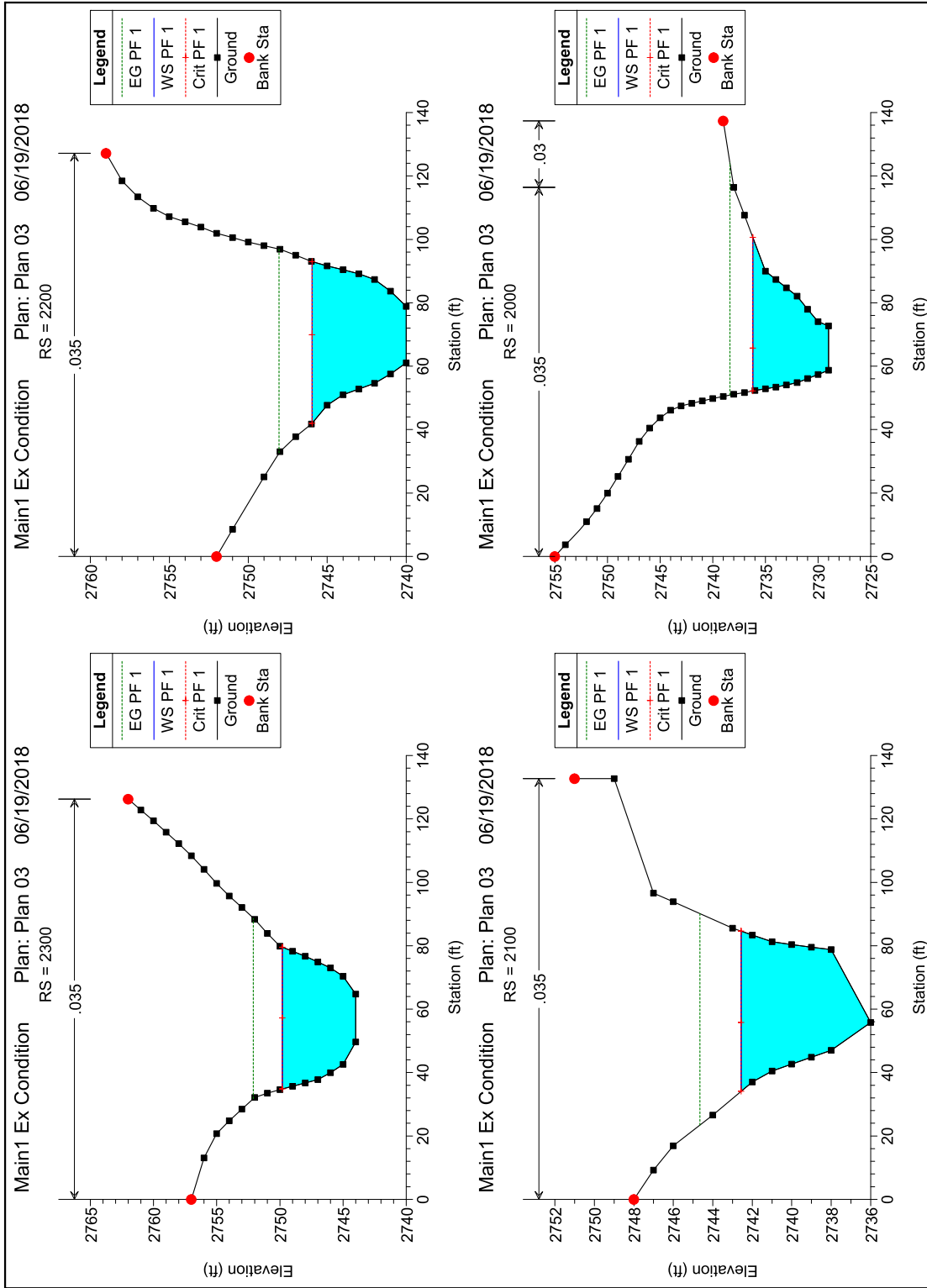
HEC-RAS Plan: Plan 03 River: Unnamed Wash Reach: Main1 Profile: PF 1

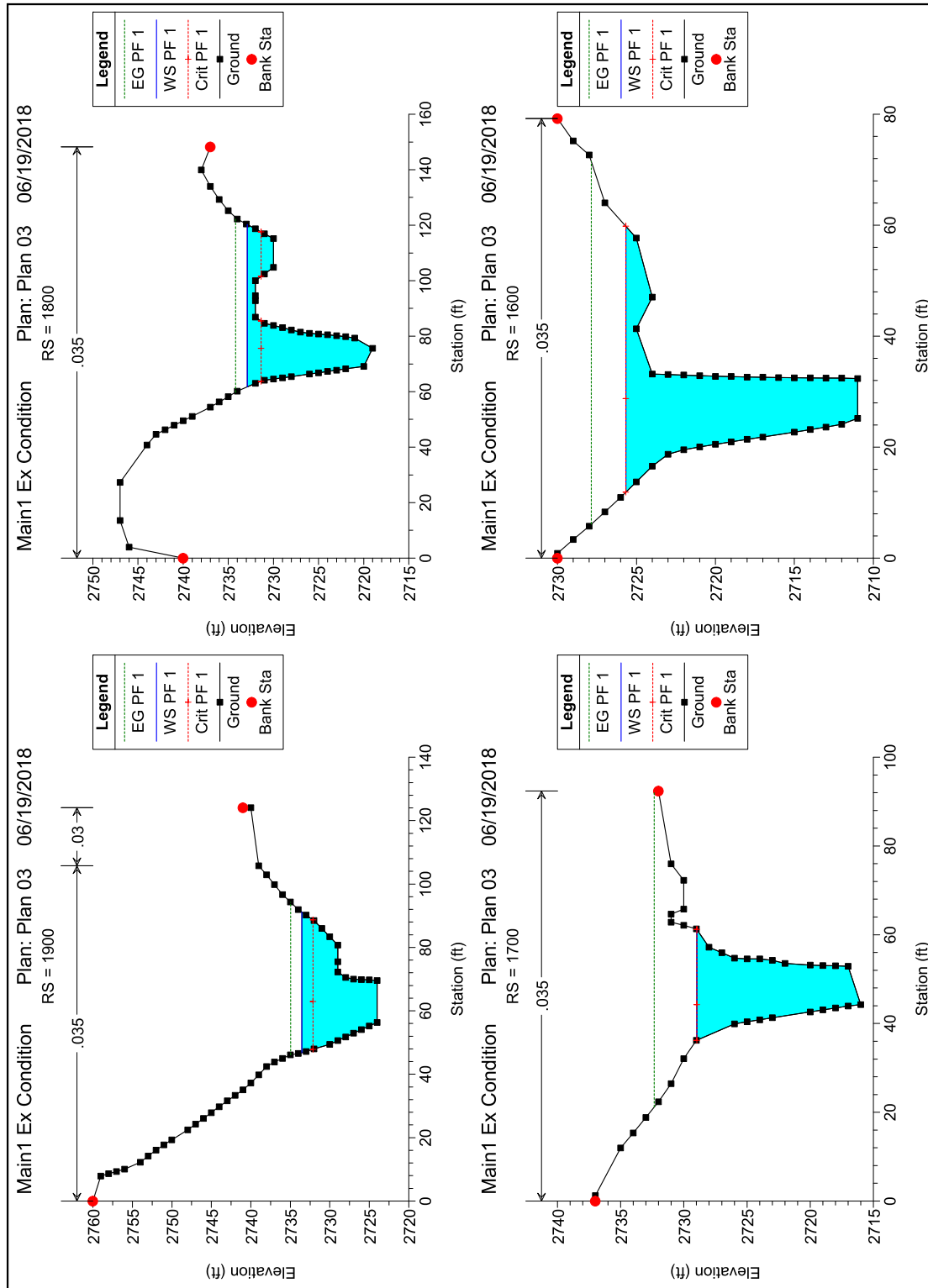
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Main1	2700	PF 1	2450.00	2756.00	2761.27	2761.27	2763.09	0.012477	10.82	226.36	62.92	1.01
Main1	2600	PF 1	2450.00	2752.00	2758.62	2758.62	2760.27	0.013351	10.31	237.64	72.53	1.00
Main1	2500	PF 1	2450.00	2748.00	2754.71	2754.71	2756.45	0.013086	10.60	231.12	67.98	1.01
Main1	2400	PF 1	2450.00	2747.00	2752.13	2752.13	2753.79	0.012416	10.35	236.63	71.11	1.00
Main1	2300	PF 1	2450.00	2744.00	2749.80	2749.80	2752.10	0.011946	12.15	201.63	44.68	1.01
Main1	2200	PF 1	2450.00	2740.00	2745.96	2745.96	2748.05	0.011983	11.60	211.22	51.01	1.00
Main1	2100	PF 1	2450.00	2736.00	2742.56	2742.56	2744.65	0.011963	11.61	211.10	50.49	1.00
Main1	2000	PF 1	2450.00	2729.00	2736.21	2736.21	2738.37	0.012530	11.81	207.49	48.41	1.01
Main1	1900	PF 1	2450.00	2724.00	2733.55	2732.13	2734.97	0.006206	9.58	255.84	44.35	0.70
Main1	1800	PF 1	2450.00	2719.00	2732.90	2731.38	2734.20	0.008452	9.16	267.48	58.50	0.76
Main1	1700	PF 1	2450.00	2716.00	2728.98	2728.98	2732.34	0.018525	14.71	166.57	24.98	1.00
Main1	1600	PF 1	2450.00	2711.00	2725.67	2725.67	2727.86	0.017884	11.87	206.39	47.95	1.01
Main1	1500	PF 1	2489.00	2707.00	2720.81	2720.81	2724.20	0.018477	14.77	168.48	25.05	1.00
Main1	1400	PF 1	2489.00	2702.00	2713.88	2713.88	2716.96	0.016221	14.09	176.69	28.90	1.00
Main1	1300	PF 1	2489.00	2699.00	2704.47	2704.47	2706.49	0.011922	11.40	218.43	54.21	1.00
Main1	1200	PF 1	2489.00	2695.00	2700.89	2700.89	2703.19	0.012029	12.16	204.67	44.53	1.00
Main1	1100	PF 1	2489.00	2691.00	2697.33	2697.33	2699.79	0.012207	12.59	197.73	40.63	1.01
Main1	1000	PF 1	2489.00	2687.00	2692.56	2692.56	2694.75	0.012148	11.86	209.87	48.09	1.00
Main1	900	PF 1	2489.00	2683.00	2689.16	2689.16	2691.66	0.012067	12.70	196.06	39.51	1.00
Main1	800	PF 1	2489.00	2679.00	2685.65	2685.65	2688.04	0.011842	12.42	200.44	41.87	1.00
Main1	700	PF 1	2489.00	2676.00	2685.81	2682.23	2686.54	0.002171	6.83	364.34	50.31	0.45
Main1	600	PF 1	2489.00	2674.00	2686.07	2679.62	2686.31	0.000531	3.92	634.70	133.80	0.23
Main1	500	PF 1	4497.00	2672.00	2685.87	2679.19	2686.19	0.000744	4.54	990.97	145.62	0.31
Main1	400	PF 1	4497.00	2671.00	2685.91	2677.65	2686.13	0.000570	3.71	1210.76	213.92	0.28
Main1	300	PF 1	4497.00	2669.00	2685.91	2676.07	2686.07	0.000323	3.20	1407.24	183.10	0.20
Main1	200	PF 1	4497.00	2668.00	2684.83	2683.47	2685.89	0.005239	8.27	543.77	110.66	0.66

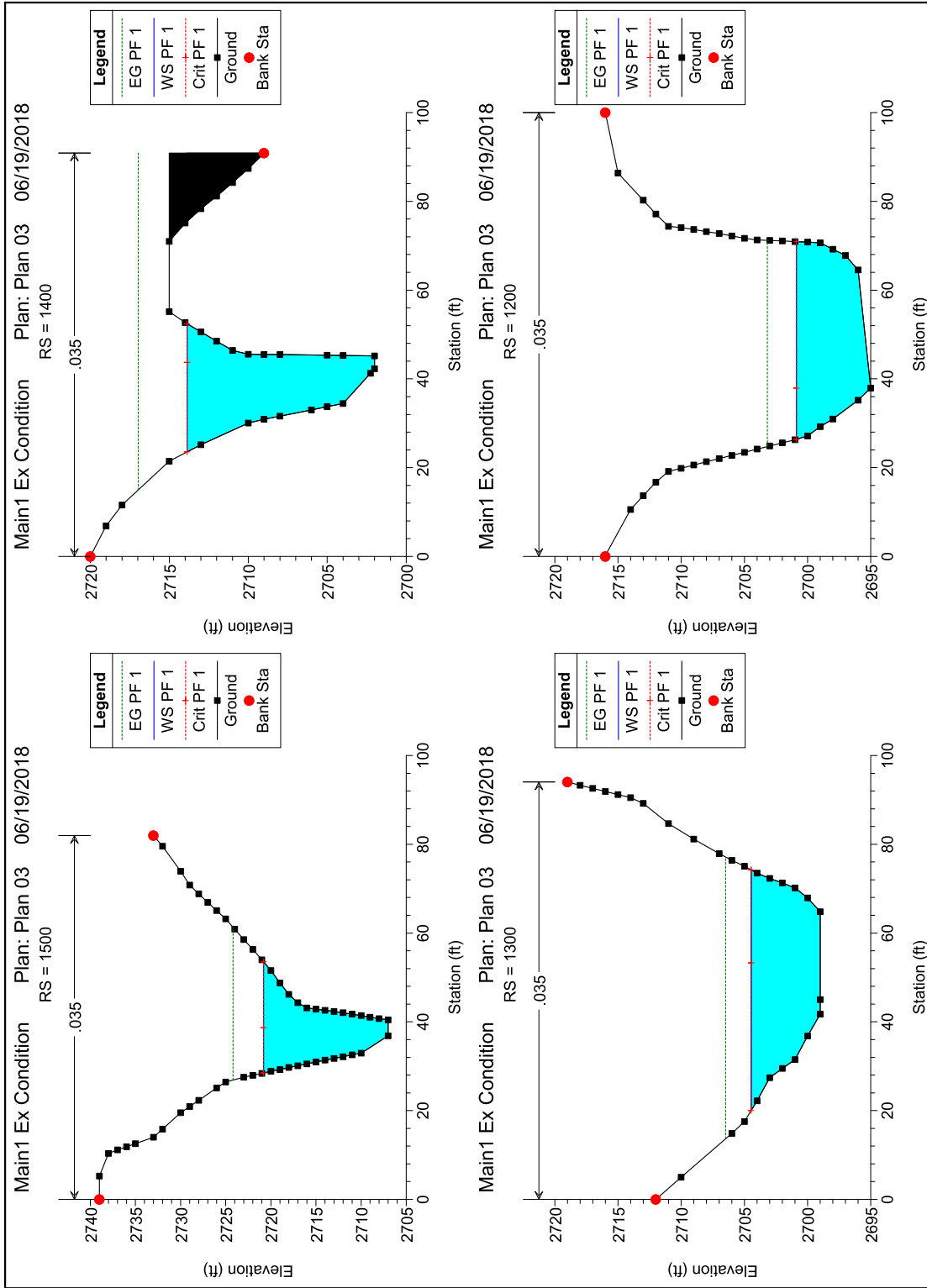


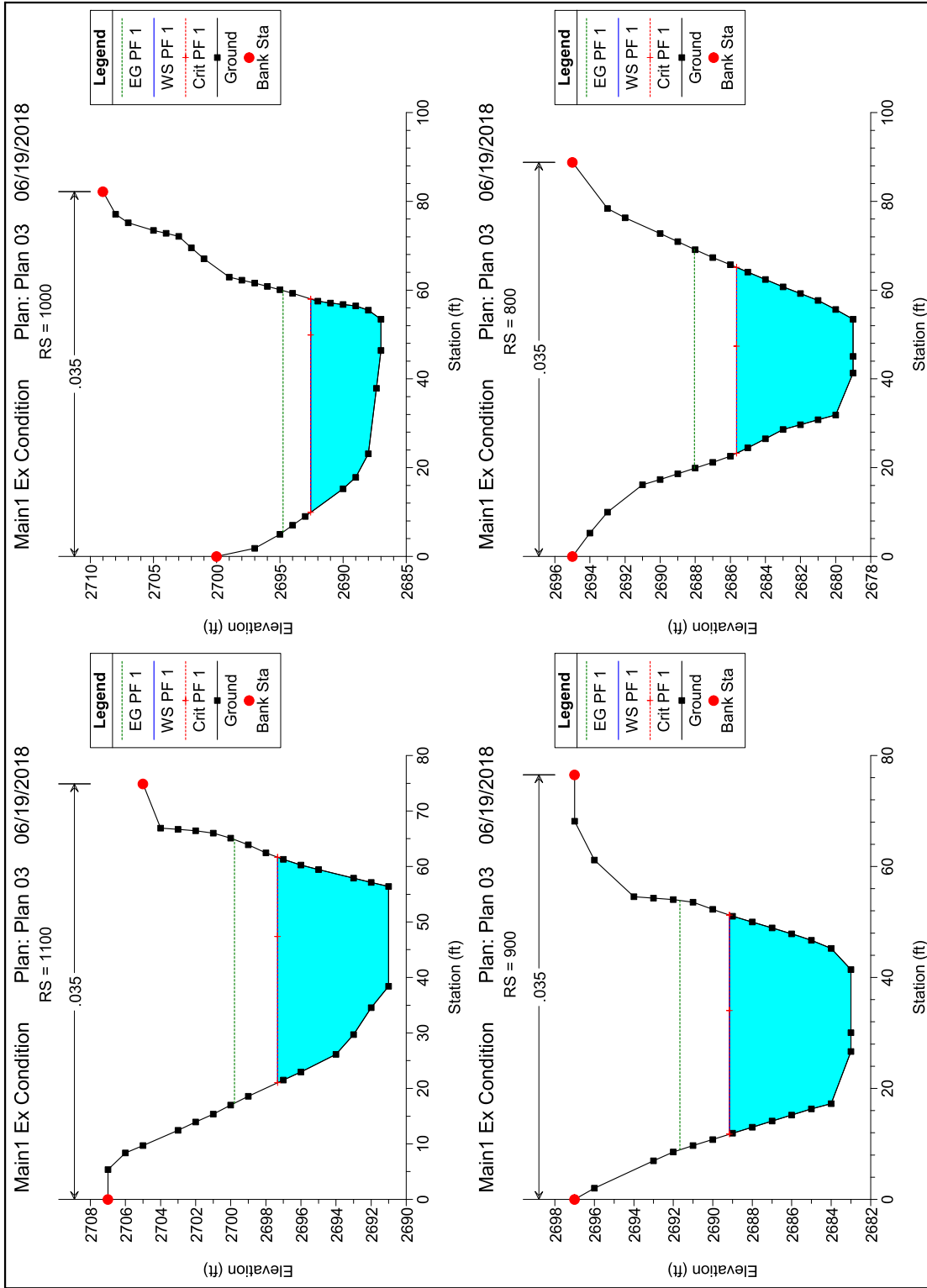
REPLY APP 1360

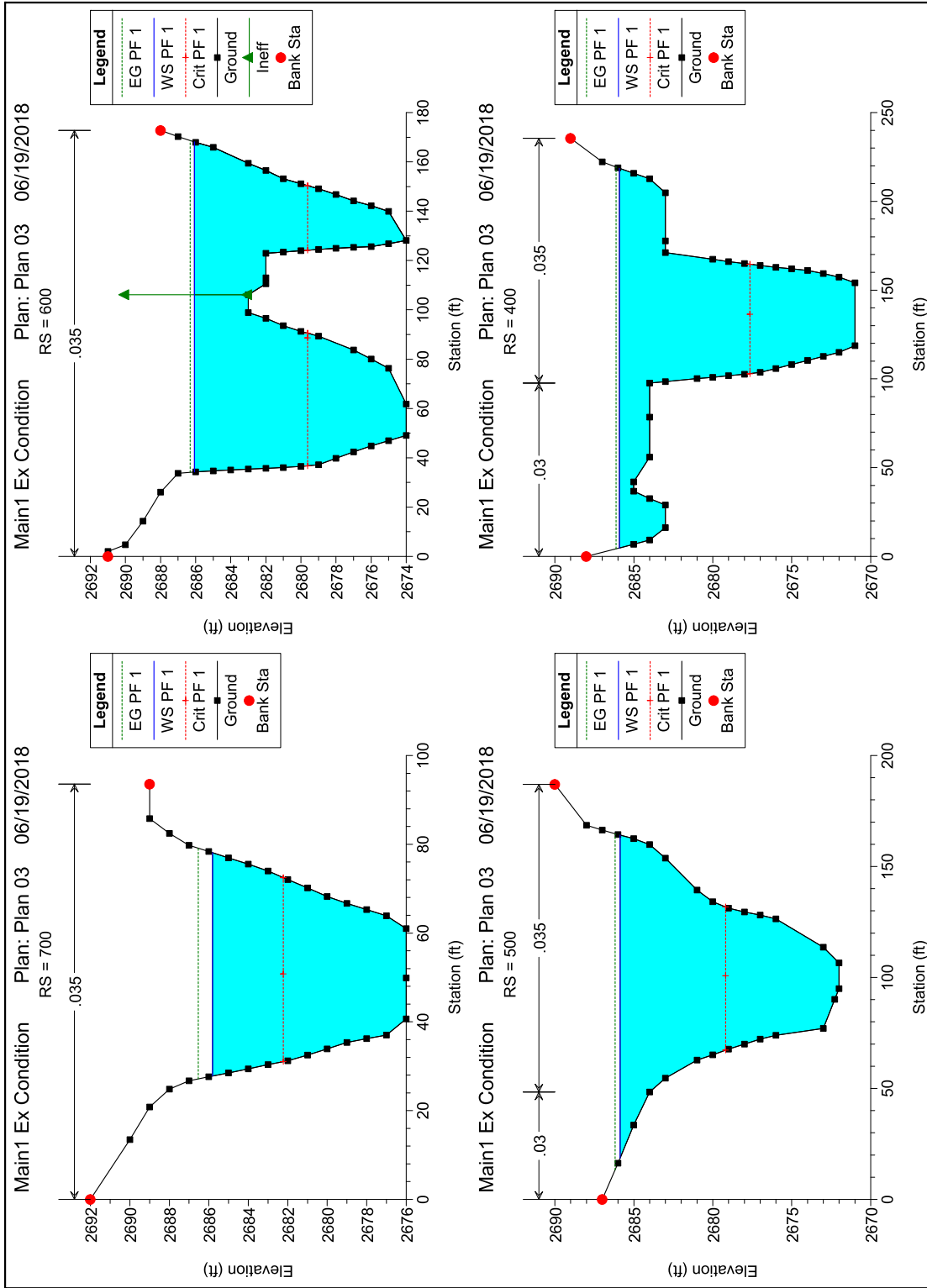


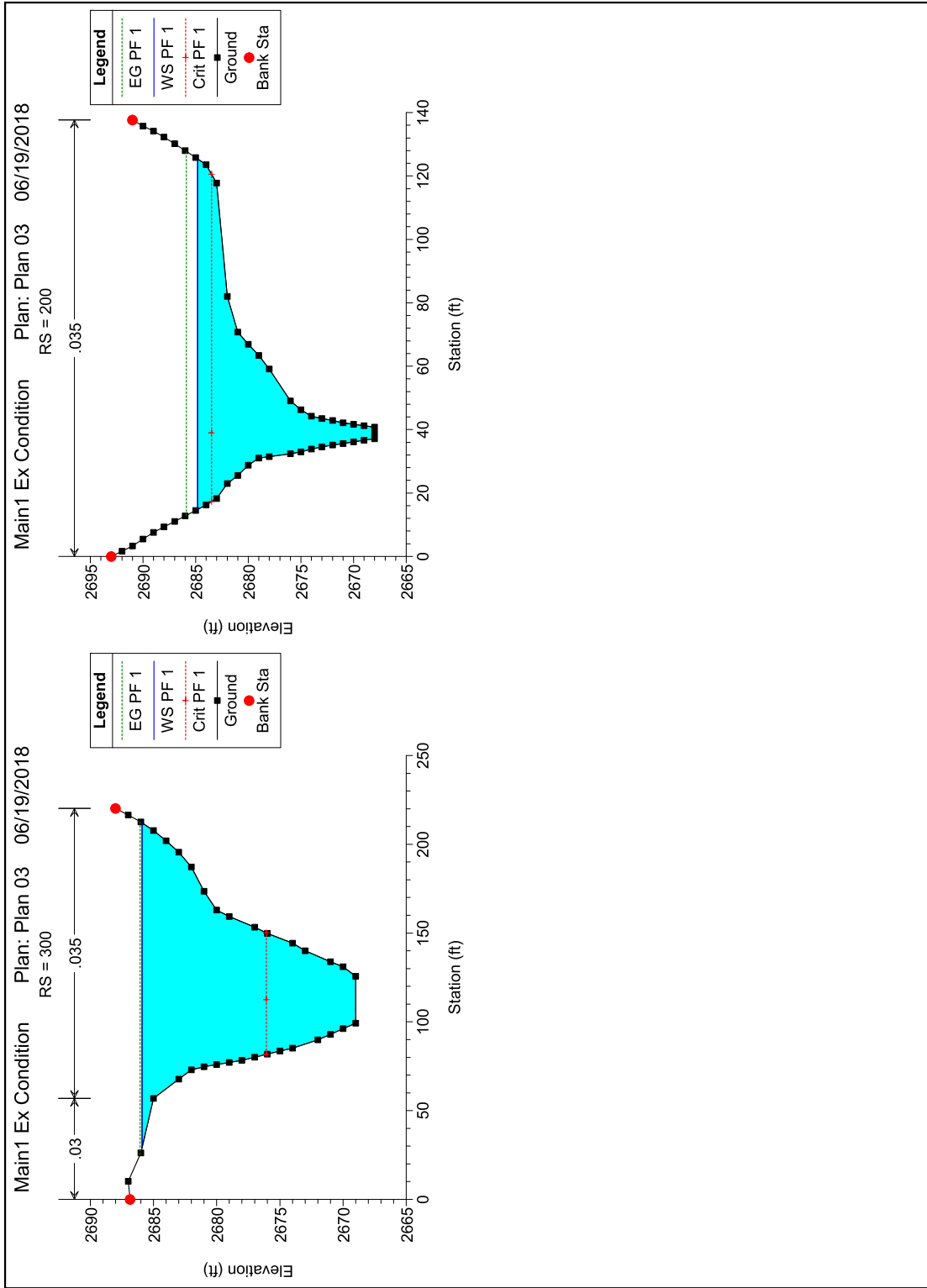












HEC-RAS HEC-RAS 5.0.3 September 2016
 U.S. Army Corps of Engineers
 Hydrologic Engineering Center
 609 Second Street
 Davis, California

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X   X   XXXXXX   XXXX   XXXX   XX   XXXX
X   X   X       X   X   X   X   X   X   X
X   X   X       X   X   X   X   X   X   X
XXXXXXX XXXX   X       XXX XXXX   XXXXXX   XXXX
X   X   X       X   X   X   X   X       X
X   X   X       X   X   X   X   X   X   X
X   X   XXXXXX   XXXX   X   X   X   X   XXXXX

```

PROJECT DATA

Project Title: Main1 Ex Condition
 Project File : Main1ExCondition.prj
 Run Date and Time: 06/19/2018 02:03:38 PM

Project in English units

PLAN DATA

Plan Title: Plan 03
 Plan File : f:\Projects\800\840-050\Division\Fctl\Calcs\RTC3\Main1ExCondition.p03

Geometry Title: Main1
 Geometry File : f:\Projects\800\840-050\Division\Fctl\Calcs\RTC3\Main1ExCondition.G01

Flow Title : Main1REV
 Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\RTC3\Main1ExCondition.f01

Plan Summary Information:

Number of: Cross Sections =	26	Multiple Openings =	0
Culverts =	0	Inline Structures =	0
Bridges =	0	Lateral Structures =	0

Computational Information

Water surface calculation tolerance =	0.01
Critical depth calculation tolerance =	0.01
Maximum number of iterations =	20
Maximum difference tolerance =	0.3
Flow tolerance factor =	0.001

Computation Options

Critical depth computed at all cross sections
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: Main1REV
 Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\RTC3\Main1ExCondition.f01

Flow Data (cfs)

River	Reach	RS	PF 1
Unnamed Wash	Main1	2700	2450
Unnamed Wash	Main1	1500	2489
Unnamed Wash	Main1	500	4497

Boundary Conditions

River	Reach	Profile	Upstream	Downstream
Unnamed Wash	Main1	PF 1	Critical	Known WS = 2684.83

GEOMETRY DATA

Geometry Title: Main1
 Geometry File : f:\Projects\800\840-050\Division\Fctl\Calcs\RTC3\Main1ExCondition.G01

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 2700

INPUT

Description:

Station	Elevation	Data	num=	32
Sta	Elev	Sta	Elev	Sta
0	2769	4.32	2768	8.89
24.32	2764	29.44	2763	34.62
48.3	2759	51.08	2758	54.15
77.45	2757	80.08	2758	90.95
97.37	2758	99.58	2759	100.37
103.09	2763	105.64	2764	108.63
119.56	2768	127.49	2769	

Manning's n	Values	num=	3
Sta	n Val	Sta	n Val
0	.035	0	.035
		127.49	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	127.49		95.75	98.69	107.97	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2763.09	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.82	Wt. n-Val.		0.035	
W.S. Elev (ft)	2761.27	Reach Len. (ft)	95.75	98.69	107.97
Crit W.S. (ft)	2761.27	Flow Area (sq ft)		226.36	
E.G. Slope (ft/ft)	0.012477	Area (sq ft)		226.36	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	62.92	Top Width (ft)		62.92	
Vel Total (ft/s)	10.82	Avg. Vel. (ft/s)		10.82	
Max Chl Dpth (ft)	5.26	Hydr. Depth (ft)		3.60	
Conv. Total (cfs)	21934.0	Conv. (cfs)		21934.0	
Length Wtd. (ft)	98.69	Wetted Per. (ft)		65.65	
Min Ch El (ft)	2756.00	Shear (lb/sq ft)		2.69	
Alpha	1.00	Stream Power (lb/ft s)		29.07	
Frctn Loss (ft)	1.27	Cum Volume (acre-ft)		28.22	
C & E Loss (ft)	0.05	Cum SA (acres)		5.28	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 2600

INPUT

Description:

Station	Elevation	Data	num=	34
Sta	Elev	Sta	Elev	Sta
0	2765	3.19	2764	6.31
12.88	2760	13.83	2759	14.76
17.69	2755	18.58	2754	22.83
43.67	2755	52.8	2756	66.54
68.82	2761	68.85	2761	70.78
86.93	2757	90.38	2758	91.7
99.48	2762	104.49	2763	110.14
			2764	115.64
			2765	

Manning's n	Values	num=	3
Sta	n Val	Sta	n Val
0	.035	0	.035
		115.64	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	115.64		101.86	103.65	108.71	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2760.27	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.65	Wt. n-Val.		0.035	
W.S. Elev (ft)	2758.62	Reach Len. (ft)	101.86	103.65	108.71
Crit W.S. (ft)	2758.62	Flow Area (sq ft)		237.64	
E.G. Slope (ft/ft)	0.013351	Area (sq ft)		237.64	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	72.53	Top Width (ft)		72.53	
Vel Total (ft/s)	10.31	Avg. Vel. (ft/s)		10.31	
Max Chl Dpth (ft)	6.62	Hydr. Depth (ft)		3.28	
Conv. Total (cfs)	21203.6	Conv. (cfs)		21203.6	
Length Wtd. (ft)	103.65	Wetted Per. (ft)		78.00	
Min Ch El (ft)	2752.00	Shear (lb/sq ft)		2.54	

Page 2

Alpha	1.00	Stream Power (lb/ft s)	26.18
Frctn Loss (ft)	1.37	Cum Volume (acre-ft)	27.69
C & E Loss (ft)	0.01	Cum SA (acres)	5.13

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 2500

INPUT

Description:

Station Elevation Data		num= 20									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2761	.38	2760	.75	2759	1.17	2758	1.89	2756		
2.3	2755	2.68	2754	3.06	2753	3.44	2752	9.58	2748		
17.77	2748	34.89	2752	60.1	2753	67.24	2754	71.71	2755		
76.74	2756	84.67	2758	93.68	2759	99.64	2760	104.45	2761		

Manning's n Values		num= 3									
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	104.45	.035						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	104.45		108.74	100.43	96.31	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2756.45	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.75	Wt. n-Val.		0.035	
W.S. Elev (ft)	2754.71	Reach Len. (ft)	108.74	100.43	96.31
Crit W.S. (ft)	2754.71	Flow Area (sq ft)		231.12	
E.G. Slope (ft/ft)	0.013086	Area (sq ft)		231.12	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	67.98	Top Width (ft)		67.98	
Vel Total (ft/s)	10.60	Avg. Vel. (ft/s)		10.60	
Max Chl Dpth (ft)	6.71	Hydr. Depth (ft)		3.40	
Conv. Total (cfs)	21417.3	Conv. (cfs)		21417.3	
Length Wtd. (ft)	100.43	Wetted Per. (ft)		71.67	
Min Ch El (ft)	2748.00	Shear (lb/sq ft)		2.63	
Alpha	1.00	Stream Power (lb/ft s)		27.93	
Frctn Loss (ft)	1.28	Cum Volume (acre-ft)		27.13	
C & E Loss (ft)	0.02	Cum SA (acres)		4.96	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 2400

INPUT

Description:

Station Elevation Data		num= 23									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2758	15.42	2758	18.34	2757	21.01	2756	23.33	2755		
24.99	2754	26.51	2753	29.64	2751	31.2	2750	33.06	2749		
35.06	2748	37.36	2747	68.67	2749	90.83	2749	95.4	2751		
98.61	2752	104.46	2754	109.02	2755	118.84	2756	121.79	2757		
123.77	2758	126.1	2759	128.13	2759						

Manning's n Values		num= 3									
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	128.13	.035						

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	128.13		109.52	114.22	121.17	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2753.79	Element	Left OB	Channel	Right OB
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Vel Head (ft)	1.67	Wt. n-Val.	0.035		
W.S. Elev (ft)	2752.13	Reach Len. (ft)	109.52	114.22	121.17
Crit W.S. (ft)	2752.13	Flow Area (sq ft)		236.63	
E.G. Slope (ft/ft)	0.012416	Area (sq ft)		236.63	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	71.11	Top Width (ft)		71.11	
Vel Total (ft/s)	10.35	Avg. Vel. (ft/s)		10.35	
Max Chl Dpth (ft)	5.13	Hydr. Depth (ft)		3.33	
Conv. Total (cfs)	21987.2	Conv. (cfs)		21987.2	
Length Wtd. (ft)	114.22	Wetted Per. (ft)		73.08	
Min Ch El (ft)	2747.00	Shear (lb/sq ft)		2.51	
Alpha	1.00	Stream Power (lb/ft s)		25.99	
Frctn Loss (ft)	1.39	Cum Volume (acre-ft)		26.59	
C & E Loss (ft)	0.06	Cum SA (acres)		4.80	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1 RS: 2300

INPUT

Description:

Station Elevation Data		num= 33									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2757	13.08	2756	20.71	2755	24.77	2754	28.47	2753		
32.13	2752	33.53	2751	34.62	2750	35.7	2749	36.76	2748		
37.76	2747	39.95	2746	42.62	2745	49.66	2744	64.78	2744		
70.38	2745	73.02	2746	74.87	2747	76.67	2748	78.26	2749		
79.83	2750	83.9	2751	88.3	2752	92.1	2753	95.71	2754		
99.67	2755	104.09	2756	108.38	2757	112.21	2758	115.85	2759		
119.41	2760	122.82	2761	126.24	2762						

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	126.24	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	126.24		191.53	193.81	198.19	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2752.10	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.29	Wt. n-Val.		0.035	
W.S. Elev (ft)	2749.80	Reach Len. (ft)	191.53	193.81	198.19
Crit W.S. (ft)	2749.80	Flow Area (sq ft)		201.63	
E.G. Slope (ft/ft)	0.011946	Area (sq ft)		201.63	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	44.68	Top Width (ft)		44.68	
Vel Total (ft/s)	12.15	Avg. Vel. (ft/s)		12.15	
Max Chl Dpth (ft)	5.80	Hydr. Depth (ft)		4.51	
Conv. Total (cfs)	22416.0	Conv. (cfs)		22416.0	
Length Wtd. (ft)	193.81	Wetted Per. (ft)		47.58	
Min Ch El (ft)	2744.00	Shear (lb/sq ft)		3.16	
Alpha	1.00	Stream Power (lb/ft s)		38.40	
Frctn Loss (ft)	2.32	Cum Volume (acre-ft)		26.02	
C & E Loss (ft)	0.06	Cum SA (acres)		4.65	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1 RS: 2200

INPUT

Description:

Station Elevation Data		num= 32									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2752	8.53	2751	25.12	2749	33.08	2748	37.76	2747		

Main1ExCondition.rep

41.77	2746	47.66	2745	50.99	2744	52.82	2743	54.58	2742
57.55	2741	61.05	2740	78.87	2740	83.65	2741	87.38	2742
89.14	2743	90.4	2744	91.6	2745	93.05	2746	95	2747
96.89	2748	98.01	2749	99.17	2750	100.55	2751	101.91	2752
103.89	2753	105.52	2754	107.21	2755	109.78	2756	113.41	2757
118.47	2758	127.18	2759						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	127.18	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

0	127.18	113.96	200.13	254.43	.1	.3
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CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2748.05	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.09	Wt. n-Val.		0.035	
W.S. Elev (ft)	2745.96	Reach Len. (ft)	113.96	200.13	254.43
Crit W.S. (ft)	2745.96	Flow Area (sq ft)		211.22	
E.G. Slope (ft/ft)	0.011983	Area (sq ft)		211.22	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	51.01	Top Width (ft)		51.01	
Vel Total (ft/s)	11.60	Avg. Vel. (ft/s)		11.60	
Max Chl Dpth (ft)	5.96	Hydr. Depth (ft)		4.14	
Conv. Total (cfs)	22381.2	Conv. (cfs)		22381.2	
Length Wtd. (ft)	200.13	Wetted Per. (ft)		53.57	
Min Ch El (ft)	2740.00	Shear (lb/sq ft)		2.95	
Alpha	1.00	Stream Power (lb/ft s)		34.21	
Frctn Loss (ft)	2.40	Cum Volume (acre-ft)		25.10	
C & E Loss (ft)	0.00	Cum SA (acres)		4.44	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 2100

INPUT

Description:

Station Elevation Data num= 20

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2748	9.24	2747	16.89	2746	26.59	2744	37.05	2742
40.48	2741	42.68	2740	44.83	2739	47.03	2738	55.78	2736
78.8	2738	79.56	2739	80.33	2740	81.25	2741	83.37	2742
85.58	2743	93.92	2746	96.58	2747	132.68	2749	132.68	2751

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	132.68	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

0	132.68	231.94	197.1	162.04	.1	.3
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CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2744.65	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.09	Wt. n-Val.		0.035	
W.S. Elev (ft)	2742.56	Reach Len. (ft)	231.94	197.10	162.04
Crit W.S. (ft)	2742.56	Flow Area (sq ft)		211.10	
E.G. Slope (ft/ft)	0.011963	Area (sq ft)		211.10	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	50.49	Top Width (ft)		50.49	
Vel Total (ft/s)	11.61	Avg. Vel. (ft/s)		11.61	
Max Chl Dpth (ft)	6.56	Hydr. Depth (ft)		4.18	
Conv. Total (cfs)	22399.5	Conv. (cfs)		22399.5	
Length Wtd. (ft)	197.10	Wetted Per. (ft)		53.43	
Min Ch El (ft)	2736.00	Shear (lb/sq ft)		2.95	
Alpha	1.00	Stream Power (lb/ft s)		34.25	
Frctn Loss (ft)	2.41	Cum Volume (acre-ft)		24.13	
C & E Loss (ft)	0.01	Cum SA (acres)		4.20	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1 RS: 2000

INPUT

Description:

Station Elevation Data			num= 36		
Sta	Elev	Sta	Elev	Sta	Elev
0	2755	3.69	2754	10.93	2752
25.24	2749	30.66	2748	36.25	2747
46.08	2744	47.48	2743	48.3	2742
50.49	2739	51.12	2738	51.7	2737
53.42	2734	54.05	2733	54.84	2732
58.7	2729	72.73	2729	74.05	2730
84.74	2733	87.34	2734	89.95	2735
137.36	2739				

Manning's n Values				num= 2	
Sta	n Val	Sta	n Val		
0	.035	116.39	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
0	137.36		231.62	197.66	162.89	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2738.37	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.17	Wt. n-Val.		0.035	
W.S. Elev (ft)	2736.21	Reach Len. (ft)	231.62	197.66	162.89
Crit W.S. (ft)	2736.21	Flow Area (sq ft)		207.49	
E.G. Slope (ft/ft)	0.012530	Area (sq ft)		207.49	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	48.41	Top Width (ft)		48.41	
Vel Total (ft/s)	11.81	Avg. Vel. (ft/s)		11.81	
Max Chl Dpth (ft)	7.21	Hydr. Depth (ft)		4.29	
Conv. Total (cfs)	21886.8	Conv. (cfs)		21886.8	
Length Wtd. (ft)	197.66	Wetted Per. (ft)		52.98	
Min Ch El (ft)	2729.00	Shear (lb/sq ft)		3.06	
Alpha	1.00	Stream Power (lb/ft s)		36.17	
Frctn Loss (ft)	1.69	Cum Volume (acre-ft)		23.18	
C & E Loss (ft)	0.22	Cum SA (acres)		3.98	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1 RS: 1900

INPUT

Description:

Station Elevation Data			num= 54		
Sta	Elev	Sta	Elev	Sta	Elev
0	2760	7.86	2759	8.62	2758
12.21	2754	14.17	2753	16.04	2752
22.45	2748	24.24	2747	26.07	2746
31.59	2743	33.35	2742	35.09	2741
42.41	2738	43.87	2737	44.98	2736
47.14	2733	47.96	2732	49.45	2730
52.93	2727	54.04	2726	55.19	2725
69.74	2725	69.88	2726	70.03	2727
75.51	2729	80.71	2729	83.34	2730
90.22	2733	91.95	2734	94.33	2735
102.86	2738	105.74	2739	124.05	2740

Manning's n Values				num= 2	
Sta	n Val	Sta	n Val		
0	.035	105.74	.03		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
0	124.05		122.47	101.94	85.19	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2734.97	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.43	Wt. n-Val.		0.035	

Main1ExCondition.rep

W.S. Elev (ft)	2733.55	Reach Len. (ft)	122.47	101.94	85.19
Crit W.S. (ft)	2732.13	Flow Area (sq ft)		255.84	
E.G. Slope (ft/ft)	0.006206	Area (sq ft)		255.84	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	44.35	Top Width (ft)		44.35	
Vel Total (ft/s)	9.58	Avg. Vel. (ft/s)		9.58	
Max Chl Dpth (ft)	9.55	Hydr. Depth (ft)		5.77	
Conv. Total (cfs)	31100.6	Conv. (cfs)		31100.6	
Length Wtd. (ft)	101.94	Wetted Per. (ft)		52.80	
Min Ch El (ft)	2724.00	Shear (lb/sq ft)		1.88	
Alpha	1.00	Stream Power (lb/ft s)		17.98	
Frctn Loss (ft)	0.73	Cum Volume (acre-ft)		22.13	
C & E Loss (ft)	0.04	Cum SA (acres)		3.77	

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 1800

INPUT

Description:

Station	Elevation	Data	num=	53						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2740	3.91	2746	13.58	2747	27.29	2747	40.79	2744	
44.66	2743	46.27	2742	47.87	2741	49.53	2740	51.08	2739	
54.43	2737	56.3	2736	58.22	2735	60.13	2734	63.04	2732	
64.1	2731	64.52	2730	64.99	2729	65.44	2728	66.35	2726	
66.79	2725	67.28	2724	67.73	2723	68.2	2722	69.12	2720	
75.66	2719	79.29	2721	79.87	2722	80.21	2723	80.48	2724	
80.76	2725	81.02	2726	81.44	2727	82.21	2728	83.08	2729	
83.9	2730	84.67	2731	86.85	2732	92.81	2732	94.63	2732	
100.04	2732	102.44	2731	104.77	2730	115.2	2730	116.94	2731	
118.67	2732	120.41	2733	122.2	2734	125.27	2735	129.23	2736	
133.96	2737	139.92	2738	148.25	2737					

Manning's n	Values	num=	3						
Sta	n Val	Sta	n Val	Sta	n Val				
0	.035	0	.035	148.25	.035				

Bank Sta: Left	Right	Lengths: Left	Channel	Right	Coeff Contr.	Expan.
0	148.25	140.2	137.49	140.54	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2734.20	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.30	Wt. n-Val.		0.035	
W.S. Elev (ft)	2732.90	Reach Len. (ft)	140.20	137.49	140.54
Crit W.S. (ft)	2731.38	Flow Area (sq ft)		267.48	
E.G. Slope (ft/ft)	0.008452	Area (sq ft)		267.48	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	58.50	Top Width (ft)		58.50	
Vel Total (ft/s)	9.16	Avg. Vel. (ft/s)		9.16	
Max Chl Dpth (ft)	13.90	Hydr. Depth (ft)		4.57	
Conv. Total (cfs)	26649.1	Conv. (cfs)		26649.1	
Length Wtd. (ft)	137.49	Wetted Per. (ft)		74.40	
Min Ch El (ft)	2719.00	Shear (lb/sq ft)		1.90	
Alpha	1.00	Stream Power (lb/ft s)		17.38	
Frctn Loss (ft)	1.66	Cum Volume (acre-ft)		21.52	
C & E Loss (ft)	0.21	Cum SA (acres)		3.65	

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 1700

INPUT

Description:

Station	Elevation	Data	num=	37						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2737	1.25	2737	11.94	2735	15.37	2734	18.84	2733	
22.36	2732	26.44	2731	32.09	2730	36.2	2729	39.93	2726	
40.4	2725	40.83	2724	41.29	2723	42.62	2720	43.08	2719	
43.53	2718	43.95	2717	44.26	2716	52.91	2717	52.98	2718	
53.05	2719	53.18	2720	53.54	2722	54.25	2723	54.56	2724	
54.58	2725	54.7	2726	55.93	2727	57.21	2728	61.3	2729	
62.1	2730	62.82	2731	64.63	2731	65.76	2730	72.27	2730	
75.99	2731	92.39	2732							

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .035 0 .035 92.39 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 92.39 145.9 141.68 135.05 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2732.34	Element	Left OB	Channel	Right OB
Vel Head (ft)	3.36	Wt. n-Val.		0.035	
W.S. Elev (ft)	2728.98	Reach Len. (ft)	145.90	141.68	135.05
Crit W.S. (ft)	2728.98	Flow Area (sq ft)		166.57	
E.G. Slope (ft/ft)	0.018525	Area (sq ft)		166.57	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	24.98	Top Width (ft)		24.98	
Vel Total (ft/s)	14.71	Avg. Vel. (ft/s)		14.71	
Max Chl Dpth (ft)	12.98	Hydr. Depth (ft)		6.67	
Conv. Total (cfs)	18000.5	Conv. (cfs)		18000.5	
Length Wtd. (ft)	141.68	Wetted Per. (ft)		41.01	
Min Ch El (ft)	2716.00	Shear (lb/sq ft)		4.70	
Alpha	1.00	Stream Power (lb/Ft s)		69.08	
Frctn Loss (ft)	2.58	Cum Volume (acre-ft)		20.84	
C & E Loss (ft)	0.35	Cum SA (acres)		3.52	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 1600

INPUT

Description:

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2730	.84	2730	3.34	2729	5.76	2728	8.34	2727
10.96	2726	13.73	2725	16.56	2724	18.7	2723	19.54	2722
20.05	2721	20.5	2720	20.95	2719	21.4	2718	21.81	2717
22.7	2715	23.18	2714	23.61	2713	24.1	2712	25.18	2711
32.35	2711	32.43	2712	32.46	2713	32.51	2714	32.51	2715
32.55	2716	32.61	2717	32.63	2718	32.73	2719	32.76	2720
32.87	2721	33	2722	33.08	2723	33.17	2724	41.32	2725
47.05	2724	57.68	2725	64.05	2727	72.68	2728	75.19	2729
79.21	2730								

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .035 0 .035 79.21 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 79.21 132.22 129.11 128.4 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2727.86	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.19	Wt. n-Val.		0.035	
W.S. Elev (ft)	2725.67	Reach Len. (ft)	132.22	129.11	128.40
Crit W.S. (ft)	2725.67	Flow Area (sq ft)		206.39	
E.G. Slope (ft/ft)	0.017884	Area (sq ft)		206.39	
Q Total (cfs)	2450.00	Flow (cfs)		2450.00	
Top Width (ft)	47.95	Top Width (ft)		47.95	
Vel Total (ft/s)	11.87	Avg. Vel. (ft/s)		11.87	
Max Chl Dpth (ft)	14.67	Hydr. Depth (ft)		4.30	
Conv. Total (cfs)	18320.3	Conv. (cfs)		18320.3	
Length Wtd. (ft)	129.11	Wetted Per. (ft)		68.27	
Min Ch El (ft)	2711.00	Shear (lb/sq ft)		3.38	
Alpha	1.00	Stream Power (lb/Ft s)		40.07	
Frctn Loss (ft)	2.35	Cum Volume (acre-ft)		20.23	
C & E Loss (ft)	0.12	Cum SA (acres)		3.40	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1 RS: 1500

INPUT

Description:

Station Elevation Data		num= 54	
Sta	Elev	Sta	Elev
0	2739	5.25	2739
12.54	2735	13.99	2733
22.3	2728	25.12	2726
28.38	2721	28.86	2720
30.55	2716	30.96	2715
32.55	2711	32.96	2710
41.04	2709	41.4	2710
42.61	2714	42.89	2715
48.75	2719	51.54	2720
60.88	2724	63.2	2725
70.84	2729	73.94	2730

Manning's n Values		num= 3	
Sta	n Val	Sta	n Val
0	.035	0	.035
81.97	.035		

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff Contr.	Expan.
0	81.97	270.26	260.99	251.15	.1

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2724.20	Element	Left OB	Channel	Right OB
Vel Head (ft)	3.39	Wt. n-Val.		0.035	
W.S. Elev (ft)	2720.81	Reach Len. (ft)	270.26	260.99	251.15
Crit W.S. (ft)	2720.81	Flow Area (sq ft)		168.48	
E.G. Slope (ft/ft)	0.018477	Area (sq ft)		168.48	
Q Total (cfs)	2489.00	Flow (cfs)		2489.00	
Top Width (ft)	25.05	Top Width (ft)		25.05	
Vel Total (ft/s)	14.77	Avg. Vel. (ft/s)		14.77	
Max Chl Dpth (ft)	13.81	Hydr. Depth (ft)		6.72	
Conv. Total (cfs)	18311.1	Conv. (cfs)		18311.1	
Length Wtd. (ft)	260.99	Wetted Per. (ft)		41.14	
Min Ch El (ft)	2707.00	Shear (lb/sq ft)		4.72	
Alpha	1.00	Stream Power (lb/ft s)		69.79	
Frctn Loss (ft)	4.51	Cum Volume (acre-ft)		19.67	
C & E Loss (ft)	0.09	Cum SA (acres)		3.29	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1 RS: 1400

INPUT

Description:

Station Elevation Data		num= 31	
Sta	Elev	Sta	Elev
0	2720	6.86	2719
30.02	2710	30.88	2709
34.42	2704	41.24	2702.26
45.32	2705	45.5	2708
48.5	2712	50.57	2713
75.09	2714	78.35	2713
90.89	2709		

Manning's n Values		num= 3	
Sta	n Val	Sta	n Val
0	.035	0	.035
90.89	.035		

Bank Sta: Left	Right	Lengths: Left Channel	Right	Coeff Contr.	Expan.
0	90.89	197.2	199.44	199.87	.1

Blocked Obstructions		num= 1	
Sta L	Sta R	Elev	
70.98	90.89	2715	

CROSS SECTION OUTPUT Profile #PF 1

Main1ExCondition.rep					
		Element	Left OB	Channel	Right OB
E.G. Elev (ft)	2716.96	Wt. n-Val.		0.035	
Vel Head (ft)	3.08	Reach Len. (ft)	197.20	199.44	199.87
W.S. Elev (ft)	2713.88	Flow Area (sq ft)		176.69	
Crit W.S. (ft)	2713.88	Area (sq ft)		176.69	
E.G. Slope (ft/ft)	0.016221	Flow (cfs)		2489.00	
Q Total (cfs)	2489.00	Top Width (ft)		28.90	
Top Width (ft)	28.90	Avg. Vel. (ft/s)		14.09	
Vel Total (ft/s)	14.09	Hydr. Depth (ft)		6.11	
Max Chl Dpth (ft)	11.88	Conv. (cfs)		19543.0	
Conv. Total (cfs)	19543.0	Wetted Per. (ft)		42.02	
Length Wtd. (ft)	199.44	Shear (lb/sq ft)		4.26	
Min Ch El (ft)	2702.00	Stream Power (lb/ft s)		59.99	
Alpha	1.00	Cum Volume (acre-ft)		18.64	
Frctn Loss (ft)	2.76	Cum SA (acres)		3.13	
C & E Loss (ft)	0.32				

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 1300

INPUT

Description:

Station	Elevation	Data	num=	29						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2712	4.99	2710	14.86	2706	17.55	2705	22.21	2704	
27.42	2703	29.49	2702	31.48	2701	36.81	2700	41.74	2699	
45.01	2699	64.83	2699	67.91	2700	70.18	2701	71.28	2702	
72.3	2703	73.52	2704	75.03	2705	76.39	2706	77.9	2707	
81.18	2709	84.68	2711	89.2	2713	90.51	2714	91.21	2715	
91.91	2716	92.61	2717	93.31	2718	94.06	2719			

Manning's n Values				num=	3
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	94.06	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
0	94.06		170	195.8	223.9	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

		Element	Left OB	Channel	Right OB
E.G. Elev (ft)	2706.49	Wt. n-Val.		0.035	
Vel Head (ft)	2.02	Reach Len. (ft)	170.00	195.80	223.90
W.S. Elev (ft)	2704.47	Flow Area (sq ft)		218.43	
Crit W.S. (ft)	2704.47	Area (sq ft)		218.43	
E.G. Slope (ft/ft)	0.011922	Flow (cfs)		2489.00	
Q Total (cfs)	2489.00	Top Width (ft)		54.21	
Top Width (ft)	54.21	Avg. Vel. (ft/s)		11.40	
Vel Total (ft/s)	11.40	Hydr. Depth (ft)		4.03	
Max Chl Dpth (ft)	5.47	Conv. (cfs)		22795.8	
Conv. Total (cfs)	22795.8	Wetted Per. (ft)		56.67	
Length Wtd. (ft)	195.80	Shear (lb/sq ft)		2.87	
Min Ch El (ft)	2699.00	Stream Power (lb/ft s)		32.69	
Alpha	1.00	Cum Volume (acre-ft)		17.74	
Frctn Loss (ft)	2.34	Cum SA (acres)		2.94	
C & E Loss (ft)	0.03				

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 1200

INPUT

Description:

Station	Elevation	Data	num=	41					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2716	.24	2716	10.59	2714	13.66	2713	16.72	2712

Main1ExCondition.rep									
19.16	2711	19.86	2710	20.62	2709	21.34	2708	22.05	2707
22.77	2706	23.47	2705	24.18	2704	24.9	2703	25.61	2702
26.28	2701	27.17	2700	29.23	2699	30.97	2698	35.17	2696
37.91	2695	64.52	2696	67.8	2697	69.22	2698	70.64	2699
70.83	2700	70.92	2701	71.09	2702	71.2	2703	71.31	2704
71.7	2705	72.21	2706	72.72	2707	73.17	2708	73.65	2709
74.08	2710	74.34	2711	77.17	2712	80.26	2713	86.35	2715
100	2716								

Manning's n Values		num=		3	
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	100	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	100		199.59	208.99	220.51	.1 .3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2703.19	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.30	Wt. n-Val.		0.035	
W.S. Elev (ft)	2700.89	Reach Len. (ft)	199.59	208.99	220.51
Crit W.S. (ft)	2700.89	Flow Area (sq ft)		204.67	
E.G. Slope (ft/ft)	0.012029	Area (sq ft)		204.67	
Q Total (cfs)	2489.00	Flow (cfs)		2489.00	
Top Width (ft)	44.53	Top Width (ft)		44.53	
Vel Total (ft/s)	12.16	Avg. Vel. (ft/s)		12.16	
Max Chl Dpth (ft)	5.89	Hydr. Depth (ft)		4.60	
Conv. Total (cfs)	22693.5	Conv. (cfs)		22693.5	
Length Wtd. (ft)	208.99	Wetted Per. (ft)		48.49	
Min Ch El (ft)	2695.00	Shear (lb/sq ft)		3.17	
Alpha	1.00	Stream Power (lb/ft s)		38.55	
Frctn Loss (ft)	2.53	Cum Volume (acre-ft)		16.78	
C & E Loss (ft)	0.02	Cum SA (acres)		2.72	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 1100

INPUT

Description:

Station Elevation Data		num=		29	
Sta	Elev	Sta	Elev	Sta	Elev
0	2707	5.35	2707	8.38	2706
13.93	2702	15.38	2701	17.01	2700
22.94	2696	26.14	2694	29.68	2693
56.38	2691	57.13	2692	57.9	2693
61.29	2697	62.43	2698	63.9	2699
66.45	2702	66.68	2703	66.92	2704

Manning's n Values		num=		3	
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	74.91	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	74.91		173.12	189.13	202.7	.1 .3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2699.79	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.46	Wt. n-Val.		0.035	
W.S. Elev (ft)	2697.33	Reach Len. (ft)	173.12	189.13	202.70
Crit W.S. (ft)	2697.33	Flow Area (sq ft)		197.73	
E.G. Slope (ft/ft)	0.012207	Area (sq ft)		197.73	
Q Total (cfs)	2489.00	Flow (cfs)		2489.00	
Top Width (ft)	40.63	Top Width (ft)		40.63	
Vel Total (ft/s)	12.59	Avg. Vel. (ft/s)		12.59	
Max Chl Dpth (ft)	6.33	Hydr. Depth (ft)		4.87	
Conv. Total (cfs)	22527.9	Conv. (cfs)		22527.9	
Length Wtd. (ft)	189.13	Wetted Per. (ft)		44.98	
Min Ch El (ft)	2691.00	Shear (lb/sq ft)		3.35	
Alpha	1.00	Stream Power (lb/ft s)		42.17	
Frctn Loss (ft)	2.30	Cum Volume (acre-ft)		15.82	
C & E Loss (ft)	0.08	Cum SA (acres)		2.51	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate

the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 1000

INPUT

Description:

Station	Elevation	Data	num=	30						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2700	1.85	2697	4.99	2695	7.03	2694	9.01	2693	
15.23	2690	17.81	2689	23.14	2688	37.9	2687.36	46.38	2687	
53.45	2687	55.47	2688	56.45	2689	56.76	2690	57.1	2691	
57.5	2692	59.29	2694	60.1	2695	60.84	2696	61.57	2697	
62.25	2698	62.94	2699	67.06	2701	69.55	2702	72.11	2703	
72.82	2704	73.47	2705	75.18	2707	77.09	2708	82.18	2709	

Manning's n	Values	num=	3		
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	82.18	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	82.18		200.05	199.88	200.05	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2694.75	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.19	Wt. n-Val.		0.035	
W.S. Elev (ft)	2692.56	Reach Len. (ft)	200.05	199.88	200.05
Crit W.S. (ft)	2692.56	Flow Area (sq ft)		209.87	
E.G. Slope (ft/ft)	0.012148	Area (sq ft)		209.87	
Q Total (cfs)	2489.00	Flow (cfs)		2489.00	
Top Width (ft)	48.09	Top Width (ft)		48.09	
Vel Total (ft/s)	11.86	Avg. Vel. (ft/s)		11.86	
Max Chl Dpth (ft)	5.56	Hydr. Depth (ft)		4.36	
Conv. Total (cfs)	22582.1	Conv. (cfs)		22582.1	
Length Wtd. (ft)	199.88	Wetted Per. (ft)		52.01	
Min Ch El (ft)	2687.00	Shear (lb/sq ft)		3.06	
Alpha	1.00	Stream Power (lb/ft s)		36.29	
Frctn Loss (ft)	2.42	Cum Volume (acre-ft)		14.93	
C & E Loss (ft)	0.03	Cum SA (acres)		2.32	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 900

INPUT

Description:

Station	Elevation	Data	num=	29						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2697	2.01	2696	6.96	2693	8.56	2692	9.68	2691	
10.78	2690	11.92	2689	13	2688	14.12	2687	15.2	2686	
16.3	2685	17.24	2684	26.67	2683	30.04	2683	41.4	2683	
45.22	2684	46.68	2685	47.87	2686	48.94	2687	50.02	2688	
51.05	2689	52.27	2690	53.58	2691	54.05	2692	54.3	2693	
54.53	2694	61.14	2696	68.17	2697	76.52	2697			

Manning's n	Values	num=	3		
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	76.52	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	76.52		200.06	199.87	200.06	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2691.66	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.50	Wt. n-Val.		0.035	
W.S. Elev (ft)	2689.16	Reach Len. (ft)	200.06	199.87	200.06
Crit W.S. (ft)	2689.16	Flow Area (sq ft)		196.06	
E.G. Slope (ft/ft)	0.012067	Area (sq ft)		196.06	
Q Total (cfs)	2489.00	Flow (cfs)		2489.00	
Top Width (ft)	39.51	Top Width (ft)		39.51	

Vel Total (ft/s)	12.70	Avg. Vel. (ft/s)	12.70
Max Chl Dpth (ft)	6.16	Hydr. Depth (ft)	4.96
Conv. Total (cfs)	22657.9	Conv. (cfs)	22657.9
Length Wtd. (ft)	199.87	Wetted Per. (ft)	43.65
Min Ch El (ft)	2683.00	Shear (lb/sq ft)	3.38
Alpha	1.00	Stream Power (lb/ft s)	42.95
Frctn Loss (ft)	2.39	Cum Volume (acre-ft)	14.00
C & E Loss (ft)	0.03	Cum SA (acres)	2.12

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 800

INPUT

Description:

Station Elevation Data				num=	32				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2695	5.28	2694	9.97	2693	16.15	2691	17.35	2690
18.64	2689	19.91	2688	21.18	2687	22.6	2686	24.45	2685
26.51	2684	28.59	2683	29.67	2682	30.77	2681	31.87	2680
41.31	2679	45.06	2679	53.43	2679	55.64	2680	57.69	2681
59.22	2682	60.74	2683	62.39	2684	64.07	2685	65.7	2686
67.32	2687	69.12	2688	70.94	2689	72.73	2690	76.3	2692
78.37	2693	88.81	2695						

Manning's n Values				num=	3				
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	88.81	.035				

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	88.81	200	199.91	200	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2688.04	Element	Left OB	Channel	Right OB
Vel Head (ft)	2.40	Wt. n-Val.		0.035	
W.S. Elev (ft)	2685.65	Reach Len. (ft)	200.00	199.91	200.00
Crit W.S. (ft)	2685.65	Flow Area (sq ft)		200.44	
E.G. Slope (ft/ft)	0.011842	Area (sq ft)		200.44	
Q Total (cfs)	2489.00	Flow (cfs)		2489.00	
Top Width (ft)	41.87	Top Width (ft)		41.87	
Vel Total (ft/s)	12.42	Avg. Vel. (ft/s)		12.42	
Max Chl Dpth (ft)	6.65	Hydr. Depth (ft)		4.79	
Conv. Total (cfs)	22872.7	Conv. (cfs)		22872.7	
Length Wtd. (ft)	199.91	Wetted Per. (ft)		45.49	
Min Ch El (ft)	2679.00	Shear (lb/sq ft)		3.26	
Alpha	1.00	Stream Power (lb/ft s)		40.45	
Frctn Loss (ft)	0.85	Cum Volume (acre-ft)		13.09	
C & E Loss (ft)	0.50	Cum SA (acres)		1.93	

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 700

INPUT

Description:

Station Elevation Data				num=	32				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2692	13.46	2690	20.83	2689	24.82	2688	26.72	2687
27.64	2686	28.5	2685	29.4	2684	30.34	2683	31.24	2682
32.5	2681	33.91	2680	35.36	2679	36.22	2678	37	2677
40.67	2676	49.89	2676	60.98	2676	63.89	2677	65.31	2678
66.7	2679	68.22	2680	70.18	2681	72.05	2682	73.98	2683

Main1ExCondition.rep
75.51 2684 76.92 2685 78.38 2686 79.79 2687 82.47 2688
85.76 2689 93.54 2689

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .035 0 .035 93.54 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 93.54 105.58 90.05 91.05 .1 .3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2686.54	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.73	Wt. n-Val.		0.035	
W.S. Elev (ft)	2685.81	Reach Len. (ft)	105.58	90.05	91.05
Crit W.S. (ft)	2682.23	Flow Area (sq ft)		364.34	
E.G. Slope (ft/ft)	0.002171	Area (sq ft)		364.34	
Q Total (cfs)	2489.00	Flow (cfs)		2489.00	
Top Width (ft)	50.31	Top Width (ft)		50.31	
Vel Total (ft/s)	6.83	Avg. Vel. (ft/s)		6.83	
Max Chl Dpth (ft)	9.81	Hydr. Depth (ft)		7.24	
Conv. Total (cfs)	53419.9	Conv. (cfs)		53419.9	
Length Wtd. (ft)	90.05	Wetted Per. (ft)		56.77	
Min Ch El (ft)	2676.00	Shear (lb/sq ft)		0.87	
Alpha	1.00	Stream Power (lb/ft s)		5.94	
Frctn Loss (ft)	0.09	Cum Volume (acre-ft)		11.80	
C & E Loss (ft)	0.15	Cum SA (acres)		1.72	

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 600

INPUT

Description:

Station	Elevation	Data	num=	53					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2691	2.03	2691	4.75	2690	14.29	2689	26.04	2688
33.69	2687	34.32	2686	34.69	2685	35.04	2684	35.4	2683
35.71	2682	36.05	2681	36.46	2680	37.14	2679	39.75	2678
42.44	2677	44.85	2676	46.95	2675	49.06	2674	61.8	2674
76.28	2675	80.1	2676	83.77	2677	89.32	2679	91.29	2680
93.62	2681	96.54	2682	98.84	2683	106.09	2683	110.53	2682
112.97	2682	122.92	2682	123.43	2681	124.01	2680	124.46	2679
124.94	2678	125.31	2677	125.68	2676	126.77	2675	128.15	2674
139.97	2675	142.29	2676	144.19	2677	146.82	2678	149.09	2679
151.09	2680	153.17	2681	156.53	2682	159.47	2683	165.89	2685
167.92	2686	170.23	2687	172.74	2688				

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .035 0 .035 172.74 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 172.74 165.96 163.56 169.79 .1 .3

Ineffective Flow num= 1
Sta L Sta R Elev Permanent
106.09 172.74 2690 F

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2686.31	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.24	Wt. n-Val.		0.035	
W.S. Elev (ft)	2686.07	Reach Len. (ft)	165.96	163.56	169.79
Crit W.S. (ft)	2679.62	Flow Area (sq ft)		634.70	
E.G. Slope (ft/ft)	0.000531	Area (sq ft)		1031.37	
Q Total (cfs)	2489.00	Flow (cfs)		2489.00	
Top Width (ft)	133.80	Top Width (ft)		133.80	
Vel Total (ft/s)	3.92	Avg. Vel. (ft/s)		3.92	
Max Chl Dpth (ft)	12.07	Hydr. Depth (ft)		8.84	
Conv. Total (cfs)	108008.9	Conv. (cfs)		108008.9	
Length Wtd. (ft)	163.56	Wetted Per. (ft)		79.09	
Min Ch El (ft)	2674.00	Shear (lb/sq ft)		0.27	
Alpha	1.00	Stream Power (lb/ft s)		1.04	
Frctn Loss (ft)	0.11	Cum Volume (acre-ft)		10.35	
C & E Loss (ft)	0.01	Cum SA (acres)		1.53	

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 500

INPUT

Description:

Station	Elevation	Data	num=	29
Sta	Elev	Sta	Elev	Sta
0	2687	16.29	2686	33.47
62.81	2681	65.1	2680	67.73
73.94	2676	77.08	2673	90.18
113.63	2673	126.37	2676	128.11
134.08	2680	139.43	2681	153.77
164.37	2686	166.37	2687	168.53

Manning's n	Values	num=	2
Sta	n Val	Sta	n Val
0	.03	48.37	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
0	187.05		58.23	51.31	62.51	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2686.19	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.32	Wt. n-Val.		0.035	
W.S. Elev (ft)	2685.87	Reach Len. (ft)	58.23	51.31	62.51
Crit W.S. (ft)	2679.19	Flow Area (sq ft)		990.97	
E.G. Slope (ft/ft)	0.000744	Area (sq ft)		990.97	
Q Total (cfs)	4497.00	Flow (cfs)		4497.00	
Top Width (ft)	145.62	Top Width (ft)		145.62	
Vel Total (ft/s)	4.54	Avg. Vel. (ft/s)		4.54	
Max Chl Dpth (ft)	13.87	Hydr. Depth (ft)		6.81	
Conv. Total (cfs)	164900.3	Conv. (cfs)		164900.3	
Length Wtd. (ft)	51.31	Wetted Per. (ft)		150.48	
Min Ch El (ft)	2672.00	Shear (lb/sq ft)		0.31	
Alpha	1.00	Stream Power (lb/ft s)		1.39	
Frctn Loss (ft)	0.03	Cum Volume (acre-ft)		6.56	
C & E Loss (ft)	0.03	Cum SA (acres)		1.01	

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 400

INPUT

Description:

Station	Elevation	Data	num=	41
Sta	Elev	Sta	Elev	Sta
0	2688.01	6.8	2685	9.24
32.59	2684	36.71	2685	41.98
97.61	2684	98.46	2683	100.13
102.54	2678	103.66	2677	105.88
112.62	2673	114.93	2672	118.66
159.33	2673	161.13	2674	161.97
164.96	2678	166.09	2679	167.41
204.74	2683	212.73	2684	215.85
235.52	2689			

Manning's n	Values	num=	2
Sta	n Val	Sta	n Val
0	.03	97.61	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
0	235.52		116.72	99.89	88.03	.1	.3	

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2686.13	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.21	Wt. n-Val.		0.035	
W.S. Elev (ft)	2685.91	Reach Len. (ft)	116.72	99.89	88.03
Crit W.S. (ft)	2677.65	Flow Area (sq ft)		1210.76	
E.G. Slope (ft/ft)	0.000570	Area (sq ft)		1210.76	
Q Total (cfs)	4497.00	Flow (cfs)		4497.00	
Top Width (ft)	213.92	Top Width (ft)		213.92	
Vel Total (ft/s)	3.71	Avg. Vel. (ft/s)		3.71	
Max Chl Dpth (ft)	14.91	Hydr. Depth (ft)		5.66	
Conv. Total (cfs)	188290.2	Conv. (cfs)		188290.2	
Length Wtd. (ft)	99.89	Wetted Per. (ft)		223.58	
Min Ch El (ft)	2671.00	Shear (lb/sq ft)		0.19	
Alpha	1.00	Stream Power (lb/ft s)		0.72	
Frctn Loss (ft)	0.04	Cum Volume (acre-ft)		5.26	
C & E Loss (ft)	0.02	Cum SA (acres)		0.80	

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1

RS: 300

INPUT

Description:

Station	Elevation	Data	num=	35
Sta	Elev	Sta	Elev	Sta
0	2686.85	10.18	2687	26.16
72.93	2682	74.69	2681	75.93
80.13	2677	81.83	2676	83.53
92.95	2671	96.11	2670	99.27
133.85	2671	140.06	2673	144.25
159.33	2679	162.93	2680	173.51
202	2684	207.73	2685	212.52

Manning's n	Values	num=	2
Sta	n Val	Sta	n Val
0	.03	56.92	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
0	220.29		145.1	100.88	52	.1	.3

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2686.07	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.16	Wt. n-Val.		0.035	
W.S. Elev (ft)	2685.91	Reach Len. (ft)	145.10	100.88	52.00
Crit W.S. (ft)	2676.07	Flow Area (sq ft)		1407.24	
E.G. Slope (ft/ft)	0.000323	Area (sq ft)		1407.24	
Q Total (cfs)	4497.00	Flow (cfs)		4497.00	
Top Width (ft)	183.10	Top Width (ft)		183.10	
Vel Total (ft/s)	3.20	Avg. Vel. (ft/s)		3.20	
Max Chl Dpth (ft)	16.91	Hydr. Depth (ft)		7.69	
Conv. Total (cfs)	250291.7	Conv. (cfs)		250291.7	
Length Wtd. (ft)	100.88	Wetted Per. (ft)		188.75	
Min Ch El (ft)	2669.00	Shear (lb/sq ft)		0.15	
Alpha	1.00	Stream Power (lb/ft s)		0.48	
Frctn Loss (ft)	0.08	Cum Volume (acre-ft)		2.26	
C & E Loss (ft)	0.09	Cum SA (acres)		0.34	

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1

RS: 200

INPUT

Description:

Station	Elevation	Data	num=	49
Sta	Elev	Sta	Elev	Sta
0	2693	1.64	2692	3.32
9.35	2688	11.06	2687	12.77
18.24	2683	23	2682	25.51
31.44	2678	32.35	2676	33
35.14	2672	35.58	2671	36.12
38.91	2668	40.82	2668	41.23
42.85	2672	43.48	2673	44.25
59.12	2678	63.36	2679	66.9
117.78	2683	123.57	2684	125.81
132.3	2688	134.11	2689	135.75

Manning's n	Values	num=	3
Sta	n Val	Sta	n Val
0	.035	0	.035
		137.7	.035

Bank Sta:	Left	Right	Coeff Contr.	Expan.
0	137.7		.3	.5

CROSS SECTION OUTPUT Profile #PF 1

E.G. Elev (ft)	2685.89	Element	Left OB	Channel	Right OB
Vel Head (ft)	1.06	Wt. n-Val.		0.035	
W.S. Elev (ft)	2684.83	Reach Len. (ft)			
Crit W.S. (ft)	2683.47	Flow Area (sq ft)		543.77	
E.G. Slope (ft/ft)	0.005239	Area (sq ft)		543.77	
Q Total (cfs)	4497.00	Flow (cfs)		4497.00	
Top Width (ft)	110.66	Top Width (ft)		110.66	
Vel Total (ft/s)	8.27	Avg. Vel. (ft/s)		8.27	
Max Chl Dpth (ft)	16.83	Hydr. Depth (ft)		4.91	
Conv. Total (cfs)	62128.5	Conv. (cfs)		62128.5	
Length Wtd. (ft)		Wetted Per. (ft)		123.17	
Min Ch El (ft)	2668.00	Shear (lb/sq ft)		1.44	

Alpha
Frctn Loss (ft)
C & E Loss (ft)

1.00

Stream Power (lb/Ft s)
Cum Volume (acre-ft)
Cum SA (acres)

Main1ExCondition.rep
11.94

SUMMARY OF MANNING'S N VALUES

River:Unnamed Wash

Reach	River Sta.	n1	n2	n3
Main1	2700	.035	.035	.035
Main1	2600	.035	.035	.035
Main1	2500	.035	.035	.035
Main1	2400	.035	.035	.035
Main1	2300	.035	.035	.035
Main1	2200	.035	.035	.035
Main1	2100	.035	.035	.035
Main1	2000	.035	.03	
Main1	1900	.035	.03	
Main1	1800	.035	.035	.035
Main1	1700	.035	.035	.035
Main1	1600	.035	.035	.035
Main1	1500	.035	.035	.035
Main1	1400	.035	.035	.035
Main1	1300	.035	.035	.035
Main1	1200	.035	.035	.035
Main1	1100	.035	.035	.035
Main1	1000	.035	.035	.035
Main1	900	.035	.035	.035
Main1	800	.035	.035	.035
Main1	700	.035	.035	.035
Main1	600	.035	.035	.035
Main1	500	.03	.035	
Main1	400	.03	.035	
Main1	300	.03	.035	
Main1	200	.035	.035	.035

SUMMARY OF REACH LENGTHS

River: Unnamed Wash

Reach	River Sta.	Left	Channel	Right
Main1	2700	95.75	98.69	107.97
Main1	2600	101.86	103.65	108.71
Main1	2500	108.74	100.43	96.31
Main1	2400	109.52	114.22	121.17
Main1	2300	191.53	193.81	198.19
Main1	2200	113.96	200.13	254.43
Main1	2100	231.94	197.1	162.04
Main1	2000	231.62	197.66	162.89
Main1	1900	122.47	101.94	85.19
Main1	1800	140.2	137.49	140.54
Main1	1700	145.9	141.68	135.05
Main1	1600	132.22	129.11	128.4
Main1	1500	270.26	260.99	251.15
Main1	1400	197.2	199.44	199.87
Main1	1300	170	195.8	223.9
Main1	1200	199.59	208.99	220.51
Main1	1100	173.12	189.13	202.7
Main1	1000	200.05	199.88	200.05
Main1	900	200.06	199.87	200.06
Main1	800	200	199.91	200
Main1	700	105.58	90.05	91.05
Main1	600	165.96	163.56	169.79
Main1	500	58.23	51.31	62.51
Main1	400	116.72	99.89	88.03
Main1	300	145.1	100.88	52
Main1	200			

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Unnamed Wash

Reach	River Sta.	Contr.	Expan.
Main1	2700	.1	.3
Main1	2600	.1	.3
Main1	2500	.1	.3
Main1	2400	.1	.3

Main1	2300	.1	.3
Main1	2200	.1	.3
Main1	2100	.1	.3
Main1	2000	.1	.3
Main1	1900	.1	.3
Main1	1800	.1	.3
Main1	1700	.1	.3
Main1	1600	.1	.3
Main1	1500	.1	.3
Main1	1400	.1	.3
Main1	1300	.1	.3
Main1	1200	.1	.3
Main1	1100	.1	.3
Main1	1000	.1	.3
Main1	900	.1	.3
Main1	800	.1	.3
Main1	700	.1	.3
Main1	600	.1	.3
Main1	500	.1	.3
Main1	400	.1	.3
Main1	300	.1	.3
Main1	200	.3	.5

ERRORS WARNINGS AND NOTES

Errors Warnings and Notes for Plan : Plan 03

River: Unnamed Wash Reach: Main1 RS: 2700 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2600 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:Divided flow computed for this cross-section.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2500 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2400 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2300 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2200 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2100 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2000 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth

[illegible]

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 700 Profile: PF 1

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

River: Unnamed Wash Reach: Main1 RS: 600 Profile: PF 1

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

River: Unnamed Wash Reach: Main1 RS: 300 Profile: PF 1

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Project Description

Input Data

Station (ft)	Elevation (ft)
100	100
200	100
300	100
400	100
500	100
600	100
700	100
800	100
900	100
1000	100
1100	100
1200	100
1300	100
1400	100
1500	100
1600	100
1700	100
1800	100
1900	100
2000	100
2100	100
2200	100
2300	100
2400	100
2500	100
2600	100
2700	100
2800	100
2900	100
3000	100
3100	100
3200	100
3300	100
3400	100
3500	100
3600	100
3700	100
3800	100
3900	100
4000	100
4100	100
4200	100
4300	100
4400	100
4500	100
4600	100
4700	100
4800	100
4900	100
5000	100
5100	100
5200	100
5300	100
5400	100
5500	100
5600	100
5700	100
5800	100
5900	100
6000	100
6100	100
6200	100
6300	100
6400	100
6500	100
6600	100
6700	100
6800	100
6900	100
7000	100
7100	100
7200	100
7300	100
7400	100
7500	100
7600	100
7700	100
7800	100
7900	100
8000	100
8100	100
8200	100
8300	100
8400	100
8500	100
8600	100
8700	100
8800	100
8900	100
9000	100
9100	100
9200	100
9300	100
9400	100
9500	100
9600	100
9700	100
9800	100
9900	100
10000	100

Roughness Segment Definitions

(0+00, 2.00)	(0+12, 2.00)	0.037
--------------	--------------	-------

Options

Results

Bentley Systems, Inc. **Bentley FlowMaster V8i (SELECTseries 1) [08.11.01.03]**

Worksheet for INTERIM DITCH SECTION 1

Results

Velocity Head	0.30	ft
Specific Energy	0.97	ft
Froude Number	1.33	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.68	ft
Critical Depth	0.76	ft
Channel Slope	5.40	%
Critical Slope	0.02958	ft/ft

Cross Section for INTERIM DITCH SECTION 1

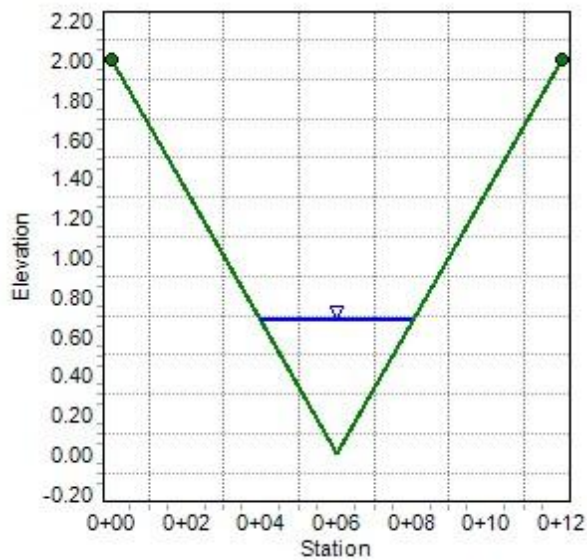
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Channel Slope 5.40 %
Normal Depth 0.68 ft
Discharge 6.00 ft³/s

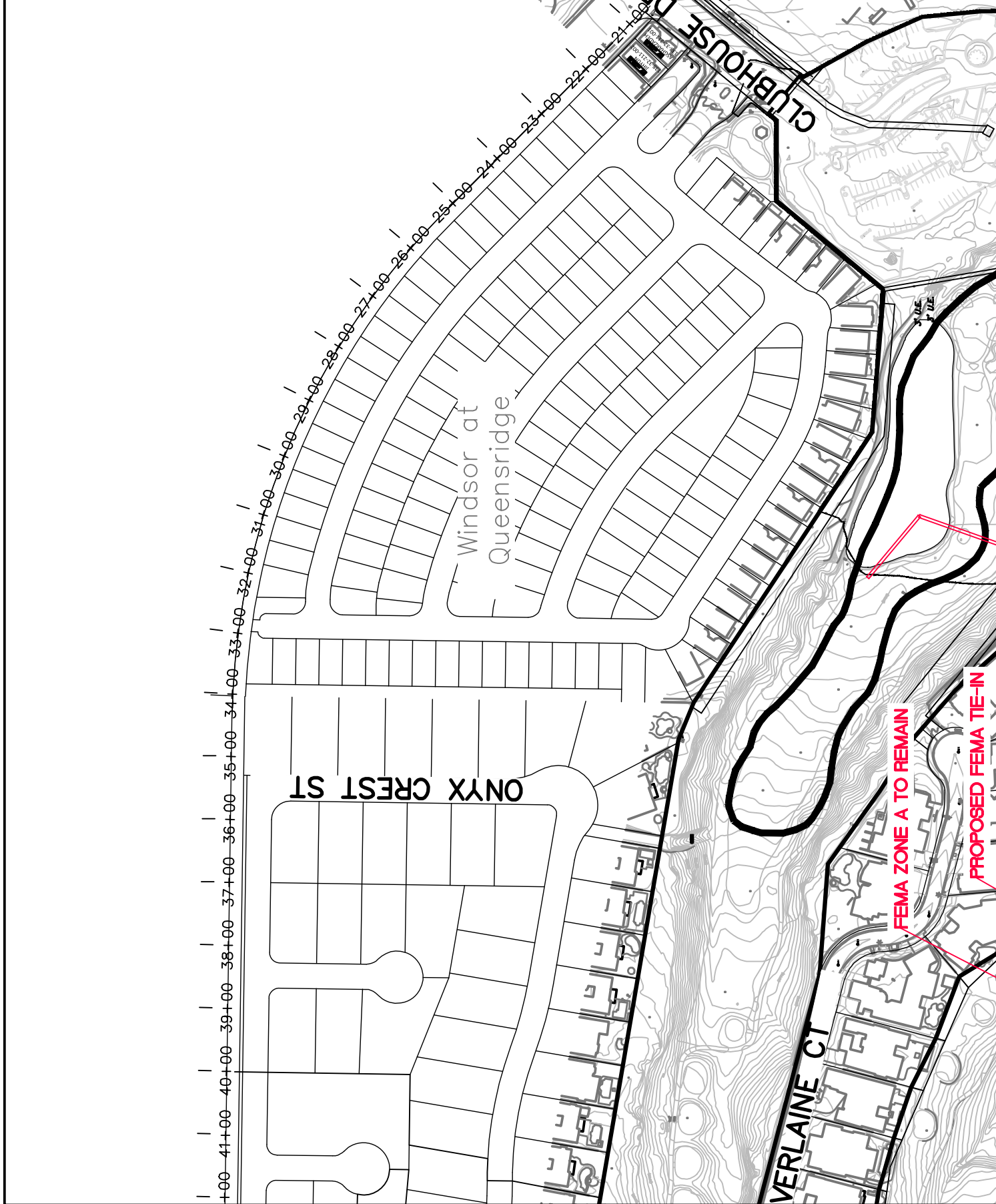
Cross Section Image

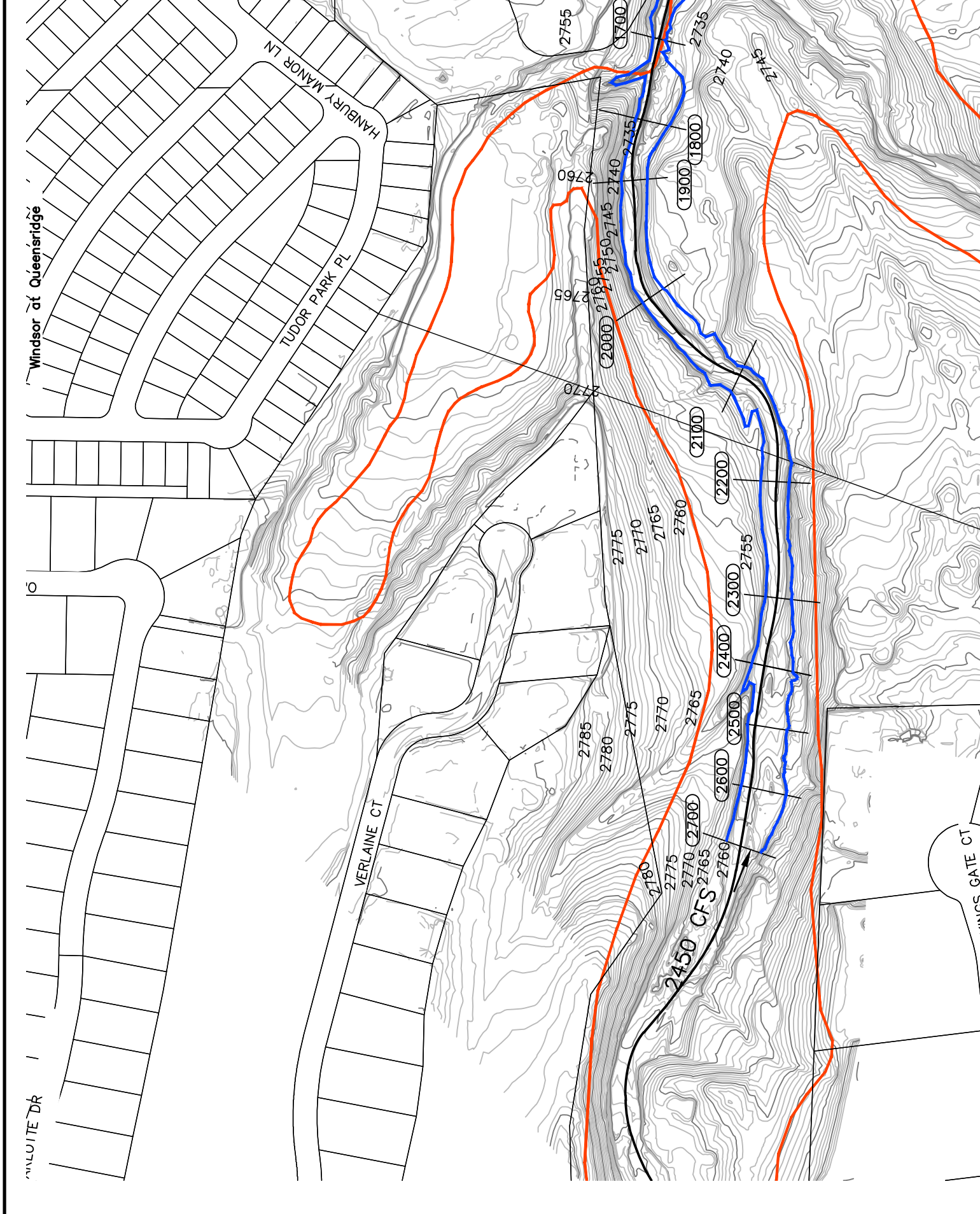


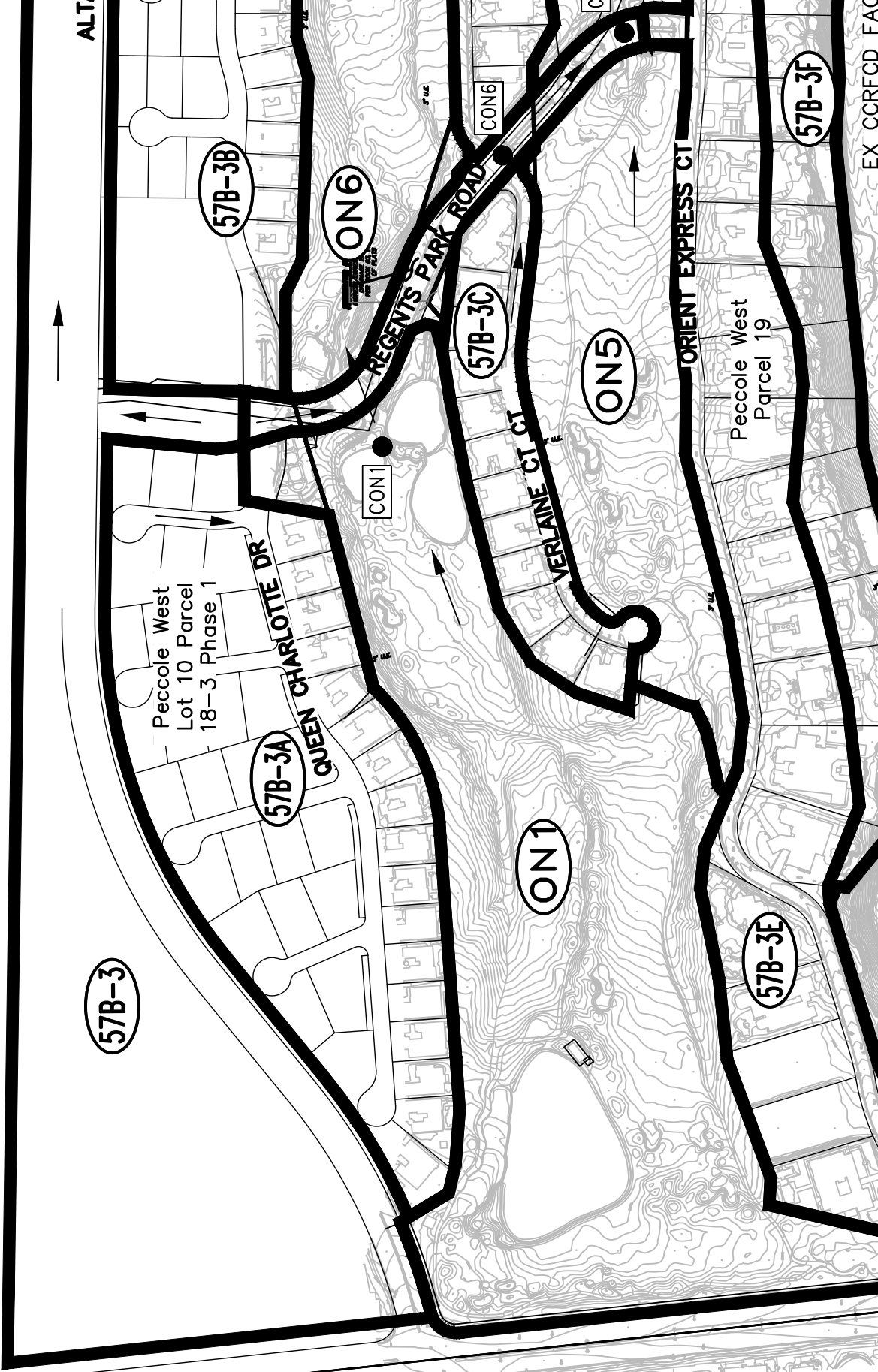
APPENDIX E

Reference Material









ALT

EX CORFCD FAC

APPENDIX D

Drainage Exhibits

* 308.41

**SUPPLEMENT NO. 1 TO THE
2nd UPDATE TO THE
TECHNICAL DRAINAGE STUDY
FOR
QUEENS BOROUGH CULVERT**

619.295

MARCH 2006

Prepared for:

**JMA Architecture Studios
10150 Covington Cross Drive
Las Vegas, Nevada 89144
Phone: (702) 731- 2033
Fax: (702) 731- 2039**



619.295
RECEIVED

CITY OF LAS VEGAS		DATE: APR 26 2006
INTER-OFFICE MEMORANDUM		April 21, 2006 G.C. WALLACE
TO: Land Development Services Department of Public Works		FROM: Albert Sung, P.E. Flood Control Project Engineer Department of Public Works
SUBJECT:	Technical Drainage Study for:	COPIES TO:
Queens Borough Culvert (Plans AKA : The Village at Queensridge Culvert)		G. C. Wallace, Inc.
Cross Streets:	NEC of Alta Drive & Rampart Boulevard	JMA Architecture
File Number:	F:\Depot\DSMEMOS\DS3674F.ZNA.doc	Bart Anderson, P.E., DevCo
Parcel Number:	138-32-601-003	CCRFGD
FEMA Flood Zone	YES X NO	
Proposed Storm Drain	YES X NO	

HISTORY	DATE RECEIVED	DATE REVIEWED	COMMENTS	REVIEW FEES	FEES PAID Trn. No.
1 st Submittal	10/25/2004	11/9/2004	Not Approved	\$400.00	11413: \$400
2 nd Submittal	12/6/2004	12/20/2004	See Comments Below	\$400.00	13199: \$400
3 rd Submittal	3/4/2005	3/18/2005	Conditionally Approved	N/C	--
4 th Submittal	8/9/2005	8/23/2005	See Comments Below	\$400.00	27281: \$400
5 th Submittal	12/15/2005	12/30/2005	See Comments Below	\$400.00	35359: \$400
6 th Submittal	2/28/2006 3/30/2006 & 4/20/2006	4/21/2006	See Comments Below	N/C	N/C
TOTAL FEES (LDDRS):				\$1,600.00	----

REMARKS: 6th Submittal: Revised the on-site RCB alignment at the northeast corner of the site. Revised the RCB outfall structure, to include additional grading within Angel Park and the relocation of the concrete access road.

The Drainage Study for the subject project has been reviewed and:

X	is approved subject to conformance to all City standards and the following conditions:
	must be resubmitted or supplemented including the following:
	is conditionally approved subject to Clark County Regional Flood Control District concurrence.

1. The existing 48'-public drainage easement (Doc # 20051129:04185) must be vacated and a new easement dedicated to reflect the revised storm drain location. Provide a new legal description and exhibit to the Right-of-Way Section with a copy to Flood Control for review and approval. The revised easement must record concurrently with the vacated easement. The new easement must record prior to the final approval of the future technical drainage study needed for onsite development or approval of any final maps. **It is noted that the public drainage easement must be privately maintained both on the surface and within the box culvert.**
2. The revised plans for the storm drain system (CLV # 107y4889-CUL) must be submitted to Land Development for approval of this proposed revision.

3. The engineer has provided a copy of the FEMA Conditional Letter of Map Revision (CLOMR), Case No. 05-09-0420R for the subject project. The engineer is advised that they are required to obtain FEMA approval for this revision as well as the completed "As-Built" condition in order to obtain the Letter of Map Revision (LOMR). **The approved LOMR must be submitted to the City of Las Vegas prior to the release of the bond.**

NOTE: The engineer must submit the drainage study to FEMA for a Conditional Letter of Map Revision (CLOMR). A favorable CLOMR must be obtained prior to the issuance of any permits. This site is located in a FEMA Zone A. Clark County Regional Flood Control District (CCRFCD) review and approval is required prior to recordation of final map or issuance of building/grading permits. The Engineer must send a copy of the report to the CCRFCD for review. The developer/engineer must also obtain a Letter of Map Revision (LOMR) using the approved drainage study as technical support to inform FEMA of the modifications within the flood zone. The approved LOMR must be submitted to the City of Las Vegas prior to the release of the bond. FEMA Elevation Certificates, showing as-built finish floor elevations, must be completed for each building in the FEMA A Zone. The certificate must be submitted to the City of Las Vegas Flood Control Section prior to scheduling a framing inspection.

NOTE: Please be advised that all land surface area disturbances over 1 acre or any area adjacent to a water way must submit to the Nevada Division of Environmental Protection a "Notice of Intent" to discharge that certifies a stormwater pollution prevention plan has been developed and is maintained on site; for inclusion in the Stormwater General Permit No. NVR100000. A phased construction unit in a contiguous subdivision is considered under construction until all stripped or disturbed surface areas have been covered by paving, building construction or planting. For more information, including forms and applications see <http://ndep.nv.gov/bwpc/storm01.htm> or call (775) 687-9429.

END OF REMARKS
B&H/ays/pbj

T/R/S: T20S/R60E/32
AREA L-32

619.295

March 30, 2006



G. C. WALLACE, INC.

Albert Sung, PE
Flood Control Project Manager
City of Las Vegas Land Development Services
731 South Fourth Street
Las Vegas, Nevada 89101

Writer's Contact Information:
804-2029

**Re: Supplement No. 1 to the 2nd Update to the Technical Drainage Study for
Queens Borough Culvert (DS3674)**

Dear Mr. Sung:

The purpose of this letter is to amend the design submitted within the 2nd *Update to the Technical Drainage Study for Queens Borough Culvert* (DS3674). The proposed amendments are at the City of Las Vegas' request and are as follows:

→ The existing embankment, located approximately 180 feet east of the RCB headwall, will be removed. Since removal of this embankment section produces increased flow velocity within the channel, a 95-foot long riprap pad (d50 = 24-inches; thickness = 48-inches) is proposed at the RCB outlet. The WSPGW calculations have been revised to model the embankment removal.

As a result of the proposed channel improvements, the RCB access road alignment has been shifted. The revised access road cross-section detail and profile are provided with the grading packet. The proposed revisions do not adversely impact the adjacent properties or downstream facilities and are in agreement with the City of Las Vegas' drainage criteria.

Copies of the water surface profile model, RCB outlet protection calculations, and proposed grading plans are provided in the Appendix.

If you have any questions or require additional information, please contact me at 804-2029.

Very truly yours,

G. C. WALLACE, INC.

Cindy Kinzer, EI
Designer

CML/CK/jj

Christopher M. Luquette, PE, CFM
Project Manager
Flood Control Division

Enc.

c: Roy Clark, GCW

G:\619-295\admin\lrv\clv-Suplmt1-2UPDATE-QueensBoro-ck-cl-3-30-06.doc

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top width	Height/Dia. - FT	Base Wt or I.D.	ZL	No wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-3625.000	14.000	7.834	21.834	4497.00	17.38	4.69	26.53	.00	9.28	62.96		1		0 .0
TRANS STR	.0400					.0187	1.41	7.83	1.51		.035			IR-
OPEN														
-3550.000	17.000	8.266	25.266	4497.00	13.55	2.85	28.12	.00	8.27	58.19		2		0 .0
TRANS STR	.0100					.0070	.35	8.27	1.00		.035			IR-
OPEN														
-3500.000	17.500	10.031	27.531	4497.00	8.46	1.11	28.64	.00	7.33	75.12		3		0 .0
TRANS STR	.0328							10.031	.561		.040			IR-
OPEN														
-3401.010	20.750	2.481	23.231	4497.00	31.66	15.56	38.79	.00	5.67	63.50		4		0 .0
TRANS STR	.0110					.0371	1.86	2.48	3.73		.015			IR-
OPEN														
-3350.810	21.300	2.522	23.822	4497.00	33.25	17.16	40.99	.00	5.89	59.13		5		0 .0
TRANS STR	.0141					.0413	1.03	2.52	3.87		.015			IR-
OPEN														
-3325.950	21.650	2.323	23.973	4497.00	34.29	18.26	42.23	.00	5.71	60.97		6		0 .0
TRANS STR	.0160					.0340	.34	2.32	4.12		.015			IR-
OPEN														
-3315.950	21.810	5.925	27.735	4497.00	31.62	15.53	43.26	.00	10.29	25.00	12.000	25.000	.00	1 1.0
90.310	.0152					.0249	2.24	5.93	2.34	7.02	.015	.00	.00	BOX
-3225.640	23.180	5.731	28.911	4497.00	32.69	16.60	45.51	.00	10.29	25.00	12.000	25.000	.00	1 1.0
2.320	-.0776					.0263	.06	5.73	2.46	.00	.015	.00	.00	BOX
-3223.320	23.000	5.682	28.682	4497.00	32.98	16.89	45.57	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
70.620	.0283					.0264	1.86	12.00	2.49	5.55	.015	.00	.00	BOX

Starting WSE

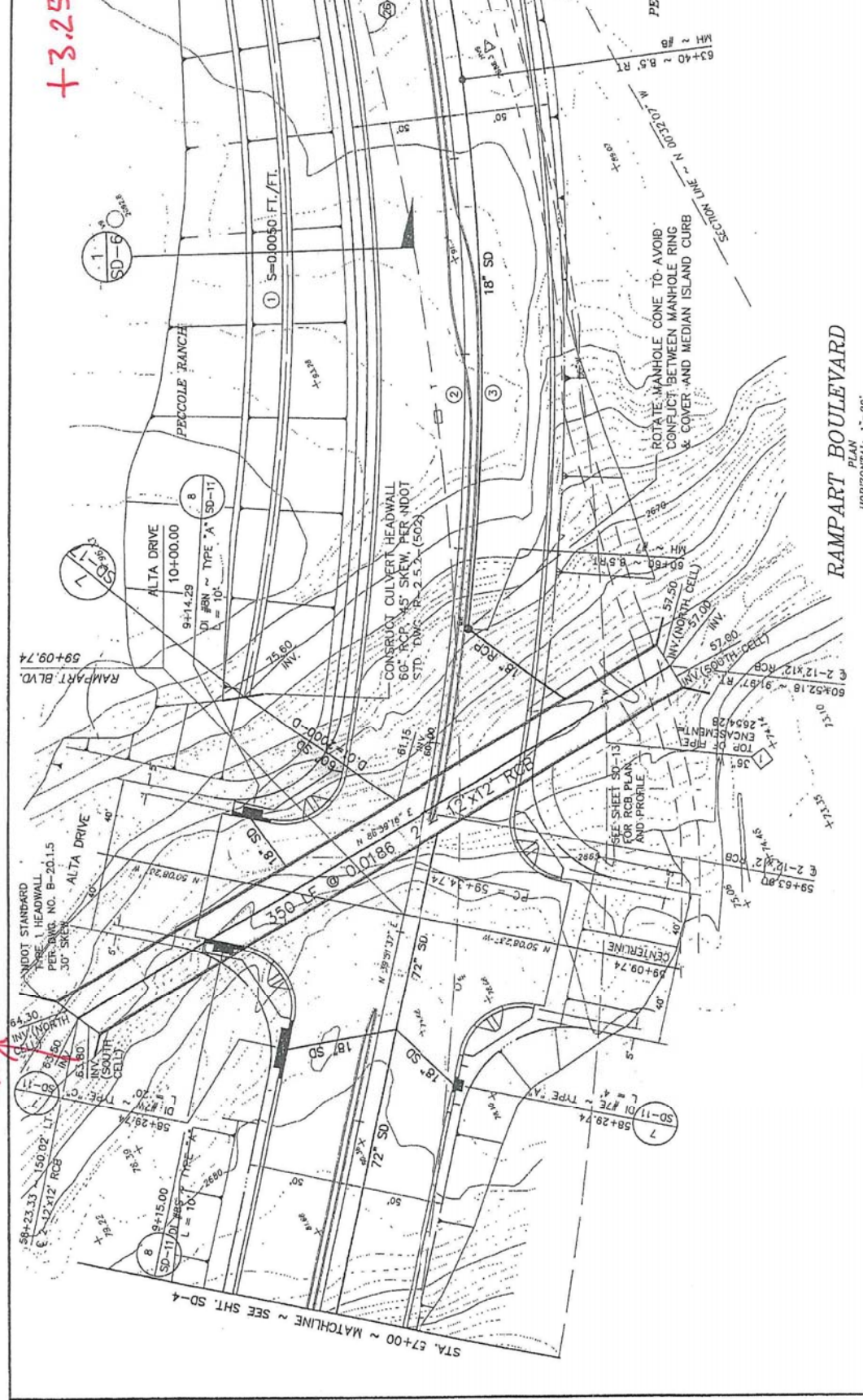
Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia. - FT	Base wt or I.D.	ZL	No wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-3152.700	25.000	5.709	30.709	4497.00	32.82	16.73	47.44	.00	10.29	25.00	12.000	25.000	.00	1 1.0
17.410	.0276					.0262	.46	5.71	2.47	5.60	.015	.00	.00	BOX
-3135.290	25.480	5.714	31.194	4497.00	32.79	16.70	47.89	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
85.300	.0279					.0260	2.21	12.00	2.47	5.58	.015	.00	.00	BOX
-3049.990	27.860	5.748	33.608	4497.00	32.60	16.50	50.11	.00	10.29	25.00	12.000	25.000	.00	1 1.0
143.470	.0279					.0253	3.63	5.75	2.45	5.58	.015	.00	.00	BOX
-2906.520	31.860	5.829	37.689	4497.00	32.15	16.05	53.73	.40	10.29	25.00	12.000	25.000	.00	1 1.0
203.401	.0278					.0238	4.83	6.22	2.39	5.58	.015	.00	.00	BOX
-2703.119	37.523	6.024	43.546	4497.00	31.11	15.02	58.57	.37	10.29	25.00	12.000	25.000	.00	1 1.0
165.794	.0278					.0214	3.54	6.39	2.28	5.58	.015	.00	.00	BOX
-2537.325	42.138	6.318	48.456	4497.00	29.66	13.66	62.11	.34	10.29	25.00	12.000	25.000	.00	1 1.0
103.695	.0278					.0188	1.95	6.65	2.12	5.58	.015	.00	.00	BOX
-2433.630	45.025	6.626	51.651	4497.00	28.28	12.42	64.07	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
60.182	.0278					.0168	1.01	12.00	1.98	5.58	.015	.00	.00	BOX
-2373.448	46.700	6.888	53.588	4497.00	27.20	11.49	65.08	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
55.228	.0278					.0150	.83	12.00	1.86	5.58	.015	.00	.00	BOX
-2318.220	48.238	7.224	55.462	4497.00	25.94	10.45	65.91	.00	10.29	25.00	12.000	25.000	.00	1 1.0
26.702	.0278					.0136	.36	7.22	1.74	5.58	.015	.00	.00	BOX

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top width	Height/Dia. -FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-2291.518	48.982	7.440	56.421	4497.00	25.19	9.85	66.27	.00	10.29	25.00	12.000	25.000	.00	1 1.0
34.206	.0278					.0123	.42	7.44	1.66	5.58	.015	.00	.00	BOX
-2257.313	49.934	7.803	57.737	4497.00	24.01	8.95	66.69	.00	10.29	25.00	12.000	25.000	.00	1 1.0
25.506	.0278					.0109	.28	7.80	1.55	5.58	.015	.00	.00	BOX
-2231.807	50.644	8.184	58.828	4497.00	22.90	8.14	66.97	.00	10.29	25.00	12.000	25.000	.00	1 1.0
18.679	.0278					.0096	.18	8.18	1.44	5.58	.015	.00	.00	BOX
-2213.128	51.164	8.583	59.748	4497.00	21.83	7.40	67.15	.00	10.29	25.00	12.000	25.000	.00	1 1.0
13.128	.0278					.0085	.11	8.58	1.34	5.58	.015	.00	.00	BOX
-2200.000	51.530	9.002	60.532	4497.00	20.81	6.73	67.26	.00	10.29	25.00	12.000	25.000	.00	1 1.0
60.785	.0080					.0080	.49	9.00	1.25	9.00	.015	.00	.00	BOX
-2139.215	52.016	9.002	61.018	4497.00	20.81	6.73	67.75	.00	10.29	25.00	12.000	25.000	.00	1 1.0
405.355	.0080					.0077	3.13	9.00	1.25	9.00	.015	.00	.00	BOX
-1733.860	55.259	9.255	64.514	4497.00	20.24	6.36	70.88	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
54.700	.0080					.0074	.40	12.00	1.20	9.00	.015	.00	.00	BOX
-1679.160	55.697	9.355	65.051	4497.00	20.03	6.23	71.28	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
95.423	.0080					.0069	.65	12.00	1.18	9.00	.015	.00	.00	BOX
-1583.737	56.460	9.811	66.271	4497.00	19.10	5.66	71.93	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
18.737	.0080					.0061	.11	12.00	1.10	9.00	.015	.00	.00	BOX

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top width	Height/Dia. - FT	Base Wt or I.D.	ZL	No wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-1565.000	56.610	10.291	66.901	4497.00	18.21	5.15	72.05	.00	10.29	25.00	12.000	25.000	.00	1 1.0
88.377	.0050					.0051	.45	10.29	1.02	10.85	.015	.00	.00	BOX
-1476.623	57.053	10.793	67.846	4497.00	17.36	4.68	72.53	.00	10.29	25.00	12.000	25.000	.00	1 1.0
257.531	.0050					.0050	1.29	10.79	.95	10.85	.015	.00	.00	BOX
-1219.092	58.343	10.853	69.196	4497.00	17.26	4.63	73.82	.00	10.29	25.00	12.000	25.000	.00	1 1.0
219.092	.0050					.0050	1.10	10.85	.94	10.85	.015	.00	.00	BOX
----- WARNING - Flow depth near top of box conduit -----														
-1000.000	59.440	10.853	70.293	4497.00	17.26	4.63	74.92	.00	10.29	25.00	12.000	25.000	.00	1 1.0

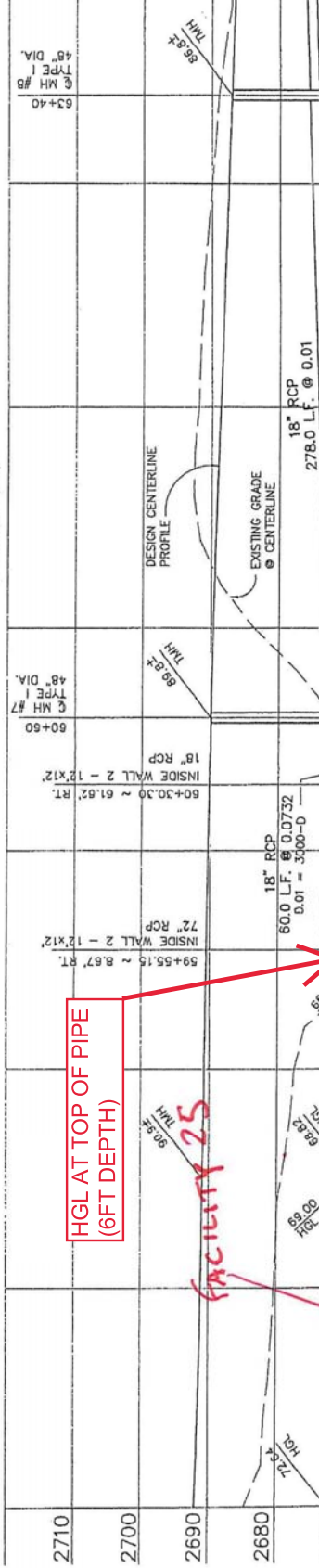
+3.25

TIE IN = 2966.75'



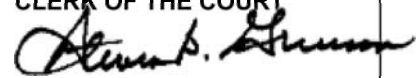
RAMPART BOULEVARD

PLAN
HORIZONTAL: 1" = 30'



APPENDIX F

Improvement Plans



1 **APEN**

2 Bryan K. Scott (NV Bar No. 4381)
3 Philip R. Byrnes (NV Bar No. 166)
4 Rebecca Wolfson (NV Bar No. 14132)
5 LAS VEGAS CITY ATTORNEY'S OFFICE
6 495 South Main Street, 6th Floor
7 Las Vegas, Nevada 89101
8 Telephone: (702) 229-6629
9 Facsimile: (702) 386-1749
10 bscott@lasvegasnevada.gov
11 pbyrnes@lasvegasnevada.gov

12 (Additional Counsel Identified on Signature Page)

13 *Attorneys for Defendant City of Las Vegas*

14 **DISTRICT COURT**

15 **CLARK COUNTY, NEVADA**

16 FORE STARS, LTD, SEVENTY ACRES, LLC, a
17 Nevada limited liability company, DOE
18 INDIVIDUALS I through X, DOE
19 CORPORATIONS I through X, DOE LIMITED
20 LIABILITY COMPANIES I through X,

21 Plaintiffs,

22 CITY OF LAS VEGAS, political subdivision of the
23 State of Nevada, THE EIGHTH JUDICIAL
24 DISTRICT COURT, County of Clark, State of
25 Nevada, DEPARTMENT 24 (the HONORABLE JIM
26 CROCKETT, DISTRICT COURT JUDGE, IN HIS
27 OFFICIAL CAPACITY), ROE government entities I
28 through X, ROE Corporations I through X, ROE
INDIVIDUALS I through X, ROE LIMITED
LIABILITY COMPANIES I through X, ROE quasi-
governmental entities I through X,

Defendants.

Case No. A-18-773268-C
Dept. No. XXIX

**SUPPLEMENTAL APPENDIX OF
EXHIBITS IN SUPPORT OF CITY'S
COUNTERMOTION FOR SUMMARY
JUDGMENT ON JUST COMPENSATION**

VOLUME 39

23 The City of Las Vegas ("City") submits this Supplemental Appendix of Exhibits in support of its
24 Countermotion for Summary Judgment on Just Compensation. This appendix supplements the Appendix
25 of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine filed
26 August 11, 2022 (Volumes 1 through 25); the Supplemental Appendix of Exhibits in Support of City's
27 Renewed Motion for Summary Judgment and Motions in Limine filed August 24, 2022 (Volumes 26
28

through 27); the Second Supplemental Appendix of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine filed September 12, 2022 (Volumes 28 through 32); and the Third Supplemental Appendix of Exhibits in Support of City's Renewed Motion for Summary Judgment and Motions in Limine filed September 14, 2022 (Volume 33).

Exhibit	Exhibit Description	Vol.	Bates No.
A	City records regarding William Peccole's Petition to Annex 2,246 acres to the City of Las Vegas	1	0001-0011
B	City records regarding the Peccole Land Use Plan and the Z-34-81 rezoning application	1	0012-0030
C	City records regarding the Venetian Foothills Master Plan and the Z-30-86 rezoning application	1	0031-0050
D	Excerpts of the 1985 City of Las Vegas General Plan	1	0051-0061
E	City records regarding Peccole Ranch Master Plan and phase I rezoning application (Z-139-88)	1	0062-0106
F	City records regarding Z-40-89 rezoning application	1	0107-0113
G	Ordinance No. 3472 (establishing the Gaming Enterprise District) and related records	1	0114-0137
H	City records regarding the Amended Peccole Ranch Master Plan and phase II rezoning application (Z-17-90)	1	0138-0194
I	Excerpts of 1992 City of Las Vegas General Plan	2	0195-0248
J	City records related to Badlands Golf Course expansion	2	0249-0254
K	Excerpt of land use case files for GPA-24-98 and GPA-6199	2	0255-0257
L	Ordinance No. 5250 and Excerpts of Las Vegas 2020 Master Plan	2	0258-0273
M	Miscellaneous Southwest Sector Land Use Maps from 2002-2005	2	0274-0277
N	Ordinance No. 5787 and Excerpts of 2005 Land Use Element	2	0278-0291
O	Ordinance No. 6056 and Excerpts of 2009 Land Use & Rural Neighborhoods Preservation Element	2	0292-0301
P	Ordinance No. 6152 and Excerpts of 2012 Land Use & Rural Neighborhoods Preservation Element	2	0302-0317
Q	Ordinance No. 6622 and Excerpts of 2018 Land Use & Rural Neighborhoods Preservation Element	2	0318-0332
R	Ordinance No. 1582	2	0333-0339
S	Ordinance No. 4073 and Excerpt of the 1997 City of Las Vegas Zoning Code	2	0340-0341

Exhibit	Exhibit Description	Vol.	Bates No.
T	Ordinance No. 5353	2	0342-0361
U	Ordinance No. 6135 and Excerpts of City of Las Vegas Unified Development Code adopted March 16, 2011	2	0362-0364
V	Deeds transferring ownership of the Badlands Golf Course	2	0365-0377
W	Third Revised Justification Letter regarding the Major Modification to the 1990 Conceptual Peccole Ranch Master Plan	2	0378-0381
X	Parcel maps recorded by the Developer subdividing the Badlands Golf Course	3	0382-0410
Y	EHB Companies promotional materials	3	0411-0445
Z	General Plan Amendment (GPA-62387), Rezoning (ZON-62392) and Site Development Plan Review (SDR-62393) applications	3	0446-0466
AA	Staff Report regarding 17-Acre Applications	3	0467-0482
BB	Major Modification (MOD-63600), Rezoning (ZON-63601), General Plan Amendment (GPA-63599), and Development Agreement (DIR-63602) applications	3	0483-0582
CC	Letter requesting withdrawal of MOD-63600, GPA-63599, ZON-63601, DIR-63602 applications	4	0583
DD	Transcript of February 15, 2017 City Council meeting	4	0584-0597
EE	Judge Crockett's March 5, 2018 order granting Queensridge homeowners' petition for judicial review, Case No. A-17-752344-J	4	0598-0611
FF	Docket for NSC Case No. 75481	4	0612-0623
GG	Complaint filed by Fore Stars Ltd. and Seventy Acres LLC, Case No. A-18-773268-C	4	0624-0643
HH	General Plan Amendment (GPA-68385), Site Development Plan Review (SDR-68481), Tentative Map (TMP-68482), and Waiver (68480) applications	4	0644-0671
II	June 21, 2017 City Council meeting minutes and transcript excerpt regarding GPA-68385, SDR-68481, TMP-68482, and 68480.	4	0672-0679
JJ	Docket for Case No. A-17-758528-J	4	0680-0768
KK	Judge Williams' Findings of Fact and Conclusions of Law, Case No. A-17-758528-J	5	0769-0793
LL	Development Agreement (DIR-70539) application	5	0794-0879
MM	August 2, 2017 City Council minutes regarding DIR-70539	5	0880-0882

Exhibit	Exhibit Description	Vol.	Bates No.
NN	Judge Sturman's February 15, 2019 minute order granting City's motion to dismiss, Case No. A-18-775804-J	5	0883
OO	Excerpts of August 2, 2017 City Council meeting transcript	5	0884-0932
PP	Final maps for Amended Peccole West and Peccole West Lot 10	5	0933-0941
QQ	Excerpt of the 1983 Edition of the Las Vegas Municipal Code	5	0942-0951
RR	Ordinance No. 2185	5	0952-0956
SS	1990 aerial photograph identifying Phase I and Phase II boundaries, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0957
TT	1996 aerial photograph identifying Phase I and Phase II boundaries, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0958
UU	1998 aerial photograph identifying Phase I and Phase II boundaries, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0959
VV	2015 aerial photograph identifying Phase I and Phase II boundaries, retail development, hotel/casino, and Developer projects, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0960
WW	2015 aerial photograph identifying Phase I and Phase II boundaries, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0961
XX	2019 aerial photograph identifying Phase I and Phase II boundaries, and current assessor parcel numbers for the Badlands property, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0962
YY	2019 aerial photograph identifying Phase I and Phase II boundaries, and areas subject to inverse condemnation litigation, produced by the City's Planning & Development Department, Office of Geographic Information Systems (GIS)	5	0963
ZZ	2019 aerial photograph identifying areas subject to proposed development agreement (DIR-70539), produced by the City's Planning & Development	5	0964

Exhibit	Exhibit Description	Vol.	Bates No.
	Department, Office of Geographic Information Systems (GIS)		
AAA	Membership Interest Purchase and Sale Agreement	6	0965-0981
BBB	Transcript of May 16, 2018 City Council meeting	6	0982-0998
CCC	City of Las Vegas' Amicus Curiae Brief, <i>Seventy Acres, LLC v. Binion</i> , Nevada Supreme Court Case No. 75481	6	0999-1009
DDD	Nevada Supreme Court March 5, 2020 Order of Reversal, <i>Seventy Acres, LLC v. Binion</i> , Nevada Supreme Court Case No. 75481	6	1010-1016
EEE	Nevada Supreme Court August 24, 2020 Remittitur, <i>Seventy Acres, LLC v. Binion</i> , Nevada Supreme Court Case No. 75481	6	1017-1018
FFF	March 26, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Entitlements on 17 Acres	6	1019-1020
GGG	September 1, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Final Entitlements for 435-Unit Housing Development Project in Badlands	6	1021-1026
HHH	Complaint Pursuant to 42 U.S.C. § 1983, <i>180 Land Co. LLC et al. v. City of Las Vegas, et al.</i> , 18-cv-00547 (2018)	6	1027-1122
III	9th Circuit Order in <i>180 Land Co. LLC; et al v. City of Las Vegas, et al.</i> , 18-cv-0547 (Oct. 19, 2020)	6	1123-1127
JJJ	Plaintiff Landowners' Second Supplement to Initial Disclosures Pursuant to NRCP 16.1 in 65-Acre case	6	1128-1137
LLL	Bill No. 2019-48: Ordinance No. 6720	7	1138-1142
MMM	Bill No. 2019-51: Ordinance No. 6722	7	1143-1150
NNN	March 26, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Entitlement Requests for 65 Acres	7	1151-1152
OOO	March 26, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Entitlement Requests for 133 Acres	7	1153-1155

Exhibit	Exhibit Description	Vol.	Bates No.
PPP	April 15, 2020 Letter from City of Las Vegas Office of the City Attorney to Counsel for the Developer Re: Entitlement Requests for 35 Acres	7	1156-1157
QQQ	Valbridge Property Advisors, Lubawy & Associates Inc., Appraisal Report (Aug. 26, 2015)	7	1158-1247
RRR	Notice of Entry of Order Adopting the Order of the Nevada Supreme Court and Denying Petition for Judicial Review	7	1248-1281
SSS	Letters from City of Las Vegas Approval Letters for 17-Acre Property (Feb. 16, 2017)	8	1282-1287
TTT	Reply Brief of Appellants 180 Land Co. LLC, Fore Stars, LTD., Seventy Acres LLC, and Yohan Lowie in <i>180 Land Co LLC et al v. City of Las Vegas</i> , Court of Appeals for the Ninth Circuit Case No. 19-16114 (June 23, 2020)	8	1288-1294
UUU	Excerpt of Reporter's Transcript of Hearing on City of Las Vegas' Motion to Compel Discovery Responses, Documents and Damages Calculation and Related Documents on Order Shortening Time in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (Nov. 17, 2020)	8	1295-1306
VVV	Plaintiff Landowners' Sixteenth Supplement to Initial Disclosures in <i>180 Land Co., LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (Nov. 10, 2020)	8	1307-1321
WWW	Excerpt of Transcript of Las Vegas City Council Meeting (Aug. 2, 2017)	8	1322-1371
XXX	Notice of Entry of Findings of Facts and Conclusions of Law on Petition for Judicial Review in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (Nov. 26, 2018)	8	1372-1399
YYY	Notice of Entry of Order <i>Nunc Pro Tunc</i> Regarding Findings of Fact and Conclusion of Law Entered November 21, 2019 in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528 (Feb. 6, 2019)	8	1400-1405
ZZZ	City of Las Vegas Agenda Memo – Planning, for City Council Meeting June 21, 2017, Re: GPA-68385, WVR-68480, SDR-68481, and TMP-68482 [PRJ-67184]	8	1406-1432

Exhibit	Exhibit Description	Vol.	Bates No.
AAAA	Excerpts from the Land Use and Rural Neighborhoods Preservation Element of the City's 2020 Master Plan adopted by the City Council of the City on September 2, 2009	8	1433-1439
BBBB	Summons and Complaint for Declaratory Relief and Injunctive Relief, and Verified Claims in Inverse Condemnation in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No.A-18-780184-C	8	1440-1477
CCCC	Notice of Entry of Findings of Fact and Conclusions of Law Granting City of Las Vegas' Motion for Summary Judgment in <i>180 Land Co. LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No.A-18-780184-C (Dec. 30, 2020)	8	1478-1515
DDDD	Peter Lowenstein Declaration	9	1516-1522
DDDD-1	Exhibit 1 to Peter Lowenstein Declaration: Diagram of Existing Access Points	9	1523-1526
DDDD-2	Exhibit 2 to Peter Lowenstein Declaration: July 5, 2017 Email from Mark Colloton	9	1527-1531
DDDD-3	Exhibit 3 to Peter Lowenstein Declaration: June 28, 2017 Permit application	9	1532-1533
DDDD-4	Exhibit 4 to Peter Lowenstein Declaration: June 29, 2017 Email from Mark Colloton re Rampart and Hualapai	9	1534-1536
DDDD-5	Exhibit 5 to Peter Lowenstein Declaration: August 24, 2017 Letter from City Department of Planning	9	1537
DDDD-6	Exhibit 6 to Peter Lowenstein Declaration: July 26, 2017 Email from Peter Lowenstein re Wall Fence	9	1538
DDDD-7	Exhibit 7 to Peter Lowenstein Declaration: August 10, 2017 Application for Walls, Fences, or Retaining Walls; related materials	9	1539-1546
DDDD-8	Exhibit 8 to Peter Lowenstein Declaration: August 24, 2017 Email from Steve Gebeke	9	1547-1553
DDDD-9	Exhibit 9 to Peter Lowenstein Declaration: Bill No. 2018-24	9	1554-1569
DDDD-10	Exhibit 10 to Peter Lowenstein Declaration: Las Vegas City Council Ordinance No. 6056 and excerpts from Land Use & Rural Neighborhoods Preservation Element	9	1570-1577

Exhibit	Exhibit Description	Vol.	Bates No.
DDDD-11	Exhibit 11 to Peter Lowenstein Declaration: documents submitted to Las Vegas Planning Commission by Jim Jimmerson at February 14, 2017 Planning Commission meeting	9	1578-1587
EEEE	GPA-72220 application form	9	1588-1590
FFFF	Chris Molina Declaration	9	1591-1605
FFFF-1	Fully Executed Copy of Membership Interest Purchase and Sale Agreement for Fore Stars Ltd.	9	1606-1622
FFFF-2	Summary of Communications between Developer and Peccole family regarding acquisition of Badlands Property	9	1623-1629
FFFF-3	Reference map of properties involved in transactions between Developer and Peccole family	9	1630
FFFF-4	Excerpt of appraisal for One Queensridge place dated October 13, 2005	9	1631-1632
FFFF-5	Site Plan Approval for One Queensridge Place (SDR-4206)	9	1633-1636
FFFF-6	Securities Redemption Agreement dated September 14, 2005	9	1637-1654
FFFF-7	Securities Purchase Agreement dated September 14, 2005	9	1655-1692
FFFF-8	Badlands Golf Course Clubhouse Improvement Agreement dated September 6, 2005	9	1693-1730
FFFF-9	Settlement Agreement and Mutual Release dated June 28, 2013	10	1731-1782
FFFF-10	June 12, 2014 emails and Letter of Intent regarding the Badlands Golf Course	10	1783-1786
FFFF-11	July 25, 2014 email and initial draft of Golf Course Purchase Agreement	10	1787-1813
FFFF-12	August 26, 2014 email from Todd Davis and revised purchase agreement	10	1814-1843
FFFF-13	August 27, 2014 email from Billy Bayne regarding purchase agreement	10	1844-1846
FFFF-14	September 15, 2014 email and draft letter to BGC Holdings LLC regarding right of first refusal	10	1847-1848

Exhibit	Exhibit Description	Vol.	Bates No.
FFFF-15	November 3, 2014 email regarding BGC Holdings LLC	10	1849-1851
FFFF-16	November 26, 2014 email and initial draft of stock purchase and sale agreement	10	1852-1870
FFFF-17	December 1, 2015 emails regarding stock purchase agreement	10	1871-1872
FFFF-18	December 1, 2015 email and fully executed signature page for stock purchase agreement	10	1873-1874
FFFF-19	December 23, 2014 emails regarding separation of Fore Stars Ltd. and WRL LLC acquisitions into separate agreements	10	1875-1876
FFFF-20	February 19, 2015 emails regarding notes and clarifications to purchase agreement	10	1877-1879
FFFF-21	February 26, 2015 email regarding revised purchase agreements for Fore Stars Ltd. and WRL LLC	10	1880
FFFF-22	February 27, 2015 emails regarding revised purchase agreements for Fore Stars Ltd. and WRL LLC	10	1881-1882
FFFF-23	Fully executed Membership Interest Purchase Agreement for WRL LLC	10	1883-1890
FFFF-24	June 12, 2015 email regarding clubhouse parcel and recorded parcel map	10	1891-1895
FFFF-25	Quitclaim deed for Clubhouse Parcel from Queensridge Towers LLC to Fore Stars Ltd.	10	1896-1900
FFFF-26	Record of Survey for Hualapai Commons Ltd.	10	1901
FFFF-27	Deed from Hualapai Commons Ltd. to EHC Hualapai LLC	10	1902-1914
FFFF-28	Purchase Agreement between Hualapai Commons Ltd. and EHC Hualapai LLC	10	1915-1931
FFFF-29	City of Las Vegas' First Set of Interrogatories to Plaintiff	10	1932-1945
FFFF-30	Plaintiff 180 Land Company LLC's Responses to City of Las Vegas' First Set of Interrogatories to Plaintiff, 3 rd Supplement	10	1946-1973
FFFF-31	City of Las Vegas' Second Set of Requests for Production of Documents to Plaintiff	11	1974-1981

Exhibit	Exhibit Description	Vol.	Bates No.
FFFF-32	Plaintiff 180 Land Company LLC's Response to Defendant City of Las Vegas' Second Set of Requests for Production of Documents to Plaintiff	11	1982-1989
FFFF-33	September 14, 2020 Letter to Plaintiff regarding Response to Second Set of Requests for Production of Documents	11	1990-1994
FFFF-34	First Supplement to Plaintiff Landowners Response to Defendant City of Las Vegas' Second Set of Requests for Production of Documents to Plaintiff	11	1995-2002
FFFF-35	Motion to Compel Discovery Responses, Documents and Damages Calculation, and Related Documents on Order Shortening Time	11	2003-2032
FFFF-36	Transcript of November 17, 2020 hearing regarding City's Motion to Compel Discovery Responses, Documents and Damages Calculation, and Related Documents on Order Shortening Time	11	2033-2109
FFFF-37	February 24, 2021 Order Granting in Part and denying in part City's Motion to Compel Discovery Responses, Documents and Damages Calculation, and Related Documents on Order Shortening Time	11	2110-2118
FFFF-38	April 1, 2021 Letter to Plaintiff regarding February 24, 2021 Order	11	2119-2120
FFFF-39	April 6, 2021 email from Elizabeth Ghanem Ham regarding letter dated April 1, 2021	11	2121-2123
FFFF-40	Hydrologic Criteria and Drainage Design Manual, Section 200	11	2124-2142
FFFF-41	Hydrologic Criteria and Drainage Design Manual, Standard Form 1	11	2143
FFFF-42	Hydrologic Criteria and Drainage Design Manual, Standard Form 2	11	2144-2148
FFFF-43	Email correspondence regarding minutes of August 13, 2018 meeting with GCW regarding Technical Drainage Study	11	2149-2152
FFFF-44	Excerpts from Peccole Ranch Master Plan Phase II regarding drainage and open space	11	2153-2159
FFFF-45	Aerial photos and demonstrative aids showing Badlands open space and drainage system	11	2160-2163
FFFF-46	August 16, 2016 letter from City Streets & Sanitation Manager regarding Badlands Golf Course Drainage Maintenance	11	2164-2166

Exhibit	Exhibit Description	Vol.	Bates No.
FFFF-47	Excerpt from EHB Companies promotional materials regarding security concerns and drainage culverts	11	2167
GGGG	Landowners' Reply in Support of Countermotion for Judicial Determination of Liability on the Landowners' Inverse Condemnation Claims Etc. in <i>180 Land Co., LLC v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (March 21, 2019)	11	2168-2178
HHHH	June 28, 2016 Letter from Mark Colloton re: Reasons for Access Points Off Hualapai Way and Rampart Blvd.	12	2179-2184
IIII	Transcript of City Council Meeting (May 16, 2018)	12	2185-2260
JJJJ	Excerpt of April 8, 2021 Transcript of Hearing re Plaintiffs' Motion for a New Trial and to Amend (March 11, 2021), Case No. A-18-780184-C	12	2261-2266
KKKK	Affidavit of Donald Richards and accompanying photographs submitted by the Developer on April 15, 2021 in Case No. A-18-780184-C	13	2267-2428
LLLL	Supplemental Declaration of Seth T. Floyd	14	2429-2432
LLLL-1	1981 Peccole Property Land Use Plan	14	2433-
LLLL-2	1985 Las Vegas General Plan	14	2434-2515
LLLL-3	1975 General Plan	14	2516-2611
LLLL-4	Planning Commission meeting records regarding 1985 General Plan	15	2612-2839
LLLL-5	1986 Venetian Foothills Master Plan	15	2840
LLLL-6	1989 Peccole Ranch Master Plan	15	2841
LLLL-7	1990 Master Development Plan Amendment	15	2842
LLLL-8	Citizen's Advisory Committee records regarding 1992 General Plan	15	2843-2860
LLLL-9	1992 Las Vegas General Plan	16-17	2861-3310
LLLL-10	1992 Southwest Sector Map	18	3311
LLLL-11	Ordinance No. 5250 (Adopting 2020 Master Plan)	18	3312-3319

Exhibit	Exhibit Description	Vol.	Bates No.
LLLL-12	Las Vegas 2020 Master Plan	18	3320-3402
LLLL-13	Ordinance No. 5787 (Adopting 2005 Land Use Element)	18	3403-3469
LLLL-14	2005 Land Use Element	18	3470-3527
LLLL-15	Ordinance No. 6056 (Adopting 2009 Land Use and Rural Neighborhoods Preservation Element)	18	3528-3532
LLLL-16	2009 Land Use and Rural Neighborhoods Preservation Element	19	3533-3632
LLLL-17	Ordinance No. 6152 (Adopting revisions to 2009 Land Use and Rural Neighborhoods Preservation Element)	19	3633-3642
LLLL-18	Ordinance No. 6622 (Adopting 2018 Land Use and Rural Neighborhoods Preservation Element)	19	3643-3653
LLLL-19	2018 Land Use & Rural Neighborhoods Preservation Element	19	3654-3753
MMMM	State of Nevada State Board of Equalization Notice of Decision, <i>In the Matter of Fore Star Ltd., et al.</i> (Nov. 30, 2017)	20	3754-3758
NNNN	Clark County Real Property Tax Values	20	3759-3774
OOOO	Clark County Tax Assessor's Property Account Inquiry - Summary Screen	20	3775-3776
PPPP	February 22, 2017 Clark County Assessor Letter to 180 Land Co. LLC, re Assessor's Golf Course Assessment	20	3777
QQQQ	Petitioner's Opening Brief, <i>In the matter of 180 Land Co. LLC</i> (Aug. 29, 2017), State Board of Equalization	20	3778-3815
RRRR	September 21, 2017 Clark County Assessor Stipulation for the State Board of Equalization	20	3816
SSSS	Excerpt of Reporter's Transcript of Hearing in <i>180 Land Co. v. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-17-758528-J (Feb. 16, 2021)	20	3817-3868
TTTT	June 28, 2016 Letter from Mark Colloton re: Reasons for Access Points Off Hualapai Way and Rampart Blvd.	20	3869-3874

Exhibit	Exhibit Description	Vol.	Bates No.
UUUU	Transcript of City Council Meeting (May 16, 2018)	20	3875-3950
VVVV	Supplemental declaration of Seth Floyd	21	3951-3953
VVVV-1	Southwest Sector Land Use Map (1992)	21	3954
VVVV-2	10/10/1991 Planning Commission Minutes	21	3955-3957
VVVV-3	10/22/1991 Planning Commission Minutes	21	3958-3962
VVVV-4	11/14/1991 Planning Commission Minutes	21	3963-3965
VVVV-5	11/26/1991 Planning Commission Minutes	21	3966-3968
VVVV-6	12/12/1991 Planning Commission Minutes	21	3969-3976
VVVV-7	12/12/1991 Planning Commission Resolution adopting 1992 General Plan	21	3977-3978
VVVV-8	2/5/1992 City Council Meeting Minutes	21	3979
VVVV-9	2/18/1992 Recommending Committee Meeting Minutes	21	3980-4000
VVVV-10	2/19/1992 City Council Meeting Minutes	21	4001-4002
VVVV-11	3/12/1992 Planning Commission Meeting Minutes	21	4003-4004
VVVV-12	3/16/1992 Recommending Committee Meeting Minute	21	4005
VVVV-13	4/1/1992 City Council Meeting Minutes	21	4006-4008
VVVV-14	Ordinance No. 3636 (adopting new general plan)	21	4009-4011

Exhibit	Exhibit Description	Vol.	Bates No.
VVVV-15	2/13/1992 Citizens Advisory Committee Meeting Minutes	21	4012-4015
VVVV-16	3/27/1991 Citizens Advisory Committee Mailout	21	4016-4025
WWWW	Excerpts of NRCP 30(b)(6) Designee of Peccole Nevada Corporation – William Bayne	21	4026-4039
XXXX	Findings of Facts, Conclusions of Law and Order Regarding Motion to Dismiss and Countermotion to Allow More Definite Statement if Necessary and Countermotion to Stay Litigation of Inverse Condemnation Claims Until Resolution of the Petition for Judicial Review and Countermotion for NRCP Rule 56(F) Continuance	21	4040-4051
YYYY	Declaration of Christopher Molina in Support of the City's Countermotion for Summary Judgment and Opposition to Motion to Determine Property Interest	21	4052-4053
ZZZZ	Declaration of Seth Floyd	21	4054-4055
ZZZZ -1	Master planned communities with R-PD zoning	21	4056-4061
ZZZZ -2	General Plan Maps for Master Planned Communities with R-PD zoning	21	4062-4067
AAAAA	Recorder's Amended Transcript of Pending Motions in <i>180 Land Company LLC, et al. vs. City of Las Vegas</i> , Eighth Judicial District Court Case No. A-18-775804 (September 17, 2021)	22	4068-4235
BBBBB	December 23, 2021 letter from Seth Floyd re Entitlements on 17-acre Property; Applications for development of other segments of former Badlands Golf Course	22	4236-4238
CCCCC	July 19, 2022 letter from Seth Floyd re Entitlements on 17-acre portion of Badlands	22	4239-4240
DDDDD	Appraisal of Real Property prepared by The DiFederico Group re the 17-Acre Property	23	4241-4394
EEEEEE	Affidavit of Donald Richards (Ex. 50 to Plaintiff Landowners' Reply in Support of Countermotion for Discovery Pursuant to NRCP 56(d) filed 7/7/2021)	23	4395-4396
FFFFF	Bill No. 2018-5 (Ordinance No. 6617)	23	4397-4405

Exhibit	Exhibit Description	Vol.	Bates No.
GGGGG	Appraisal Consulting Report prepared by Charles E. Jack of Integra Realty Resources	24	4406-4586
HHHHH	Supplemental Declaration Peter Lowenstein	24	4587-4600
HHHHH-1	Email from Steve Swanton re PMP – 58526 and PMP-58527 (Queensridge/Badlands Golf Course)	24	4601-4602
HHHHH-2	June 8, 2015 letter to Angie Scott from Steve Swanton re PMP-59572	24	4603
HHHHH-3	Email from Stephanie Allen to Peter Lowenstein re Development Agreement	24	4604-4605
HHHHH-4	Email from Lucien Paet re New Badlands Parcel Map	24	4606
HHHHH-5	Approved Site Plan for SDR-62393	24	4607
IIIII	Declaration of Kevin McOsker	25	4608-4609
JJJJJ	Videotaped Deposition of Tio Stephan DiFederico, MAI	25	4610-4711
KKKKK	Appellant's Opening Brief filed 11/6/18 in Nevada Supreme Court Case No. 75481	26	4712-4791
LLLLL	Appellant's Amended Reply Brief filed 5/1/19 in Nevada Supreme Court Case No. 75481	26	4792-4829
MMMMM	City of Las Vegas's Motion for Summary Judgment filed 11/9/20 in the 65-Acre Case (No. A-18-780184-C)	26	4830-4862
NNNNN	Plaintiff Landowners' Opposition to the City's Motion for Summary Judgment Etc. filed 11/23/20 in the 65-Acre Case (No. A-18-780184-C)	26	4863-4950
OOOOO	City of Las Vegas' Motion to Remand 133-Acre Applications to the Las Vegas City Council filed 8/9/2021 in the 133-Acre Case (No. A-18-775804-J)	27	4951-4961
PPPPP	Notice of Entry of Findings of Fact, Conclusions of Law Regarding (1) Motion to Remand 133-Acre Applications to Las Vegas City Council and (2) Motion to Dismiss Civil Complaint Improperly Joined with Petition for Judicial Review	27	4962-4973

Exhibit	Exhibit Description	Vol.	Bates No.
QQQQQ	Deposition Transcript of Charles E. Jack, June 16, 2022	28	4974-5168
RRRRR	Deposition Transcript of NRCP 30(b)(6) Designee of Peccole Nevada Corporation – William Bayne	29	5169-5411
SSSSS	Order Granting the City of Las Vegas' Motion to Compel and for an Order to Show Cause in the 35-Acre Case (No. A-17-758528-J)	30	5412-5416
TTTTT	Order Granting the City of Las Vegas' Objection to the Discovery Commissioner's Report and Recommendation in the 35-Acre Case (No. A-17-758528-J)	30	5417-5422
UUUUU	Appraisal of Real Property prepared by The DiFederico Group re the 35-Acre Property	30	5423-5558
VVVVV	Excerpts of Deposition Transcript of Yohan Lowie	31	5559-5566
WWWWW	Declaration of Philip R. Byrnes in Support of City's Reply in Support of City's Renewed Motion for Summary Judgment and City's Motion to Strike Developer's Countermotion for Approval of Entitlements and to End Take	32	5567-5568
WWWWW-1	Agenda Summary Page for Item 28 of the August 3, 2022 Las Vegas City Council meeting	32	5569-5570
WWWWW-2	Settlement Proposal	32	5571-5583
XXXXX	Order Granting Stay	33	5584-5588
YYYYY	Declaration of Oh-Sang Kwon	34	5589-5595
YYYYY-1	Technical Drainage Study for the Seventy 840-050 March 2016	34-35	5596-5982
YYYYY-2	Supplement to Technical Drainage Study for the Seventy 840-050 March 2016	35	5983-6024
YYYYY-3	March 24, 2016 City of Las Vegas Inter-Office Memorandum re Drainage Study for The Seventy	36	6025-6028
YYYYY-4	September 2017 Response to 1st CLV Comments on the Technical Drainage Study for the 435 (Formerly "The Seventy")	36	6029-6193
YYYYY-5	September 14, 2017 - Improvement Plans for the 435	37	6194-6210
YYYYY-6	March 24, 2016 City of Las Vegas Inter-Office Memorandum re Drainage Study for The Seventy	37	6211-6215
YYYYY-7	January 2018 Response to 2nd CLV Comments on the Technical Drainage Study for the 435 (Formerly "The Seventy")	37	6216-6292

Exhibit	Exhibit Description	Vol.	Bates No.
YYYYYY-8	January 10, 2018 - Improvement Plans for the 435	37	6293-6309
YYYYYY-9	February 1, 2018 City of Las Vegas Inter-Office Memorandum re Drainage Study for the 435 formerly the SEVENTY	37	6310-6314
YYYYYY-10	June 2018 Response to 3 rd CLV Comments on the Technical Drainage Study for the 435 (Formerly "The Seventy")	38	6315-6461
YYYYYY-11	Improvement Plans for the 435	39	6462-6483
YYYYYY-12	July 26, 2018 City of Las Vegas Inter-Office Memorandum re Drainage Study for the 435 formerly the Seventy	39	6484-6489
YYYYYY-13	August 13, 2016 GCW Engineers Meeting Minutes	39	6490-6495
YYYYYY-14	Email re The 435 TD5 Comments Review Meeting	39	6496-6499
ZZZZZ	Declaration of Michael Cunningham	39	6500
ZZZZZ-1	Administrative Code, 2019 Edition	39	6501-6507

Dated this 23rd day of November, 2022.

McDONALD CARANO LLP

By: /s/ George F. Ogilvie III

George F. Ogilvie III (NV Bar No. 3552)
Christopher Molina (NV Bar No. 14092)
2300 W. Sahara Avenue, Suite 1200
Las Vegas, Nevada 89102

LAS VEGAS CITY ATTORNEY'S OFFICE
Bryan K. Scott (NV Bar No. 4381)
Philip R. Byrnes (NV Bar No. 166)
Rebecca Wolfson (NV Bar No. 14132)
495 South Main Street, 6th Floor
Las Vegas, Nevada 89101

SHUTE, MIHALY & WEINBERGER, LLP
Andrew W. Schwartz (CA Bar No. 87699)
(Admitted *pro hac vice*)
Lauren M. Tarpey (CA Bar No. 321775)
(Admitted *pro hac vice*)
396 Hayes Street
San Francisco, California 94102

Attorneys for City of Las Vegas

1 **CERTIFICATE OF SERVICE**

2 I HEREBY CERTIFY that I am an employee of McDonald Carano LLP, and that on the 23rd
3 day of November, 2022, I caused a true and correct copy of the foregoing **FOURTH SUPPLEMENTAL**
4 **APPENDIX OF EXHIBITS IN SUPPORT OF CITY'S COUNTERMOTION FOR SUMMARY**
5 **JUDGMENT ON JUST COMPENSATION – VOLUME 39** to be electronically served with the
6 Clerk of the Court via the Clark County District Court Electronic Filing Program which will provide
7 copies to all counsel of record registered to receive such electronic notification.

8 /s/ Jelena Jovanovic

9 An employee of McDonald Carano LLP

EXHIBIT “YYYYYY-11”

FOR

APN: 138-32-301-005

INDEX OF DRAWINGS		SHEET TITLE
SHEET	DATE	
1	01/02	COVER SHEET
2	01/02	PROJECT DATA
3	01/03	GENERAL NOTES
4	04/07	GRADING PLAN 1
5	04/02	GRADING PLAN 2
6	04/03	SEWERING PLAN
7	04/04	GRADING PLAN 4
8	03/00	PLAN & PROFILE: GENERAL
9	03/07	PLAN & PROFILE 1
10	03/09	PLAN & PROFILE 2
11	03/10	PLAN & PROFILE 3
12	03/09	PLAN & PROFILE 4
13	03/09	PLAN & PROFILE 5
14	03/06	PLAN & PROFILE 6
15	03/07	PLAN & PROFILE 7
16	03/08	LATERAL PLAN & PROFILE 1
17	03/09	LATERAL PLAN & PROFILE 2
18	03/10	LATERAL PLAN & PROFILE 3
19	03/11	LATERAL PLAN & PROFILE 4
20	03/07	SECTION 1: DETAILS
21	03/07	SECTION 2: DETAILS
22	03/07	SECTION 3: DETAILS

[illegible]

LEGAL DESCRIPTION	<p>LOTS 1 AND 2 AS SHOWN IN FILE 120, PAGE 31 OF PARCEL MAPS AND LOTS 3 AS SHOWN IN FILE 120, PAGE 32 OF PARCEL MAPS AND LOTS 4 AS SHOWN IN FILE 120, PAGE 33 OF PARCEL MAPS.</p>
DRAINAGE CERTIFICATION	<p>I CERTIFY THAT THE GRADINGS PLANS ARE IN CONFORMANCE WITH THE CITY OF LAS VEGAS' 2000-00-000000 ON FILE AT THE CITY OF LAS VEGAS FOR THIS PROJECT.</p>
MARK 2: FINDER	DATE
OWNER/DEVELOPER	<p>REACTIV, ARELL, LLC AND FOUR STARS, LLC 1000 S. FORT MOHAVE RD. LAS VEGAS NV, 89117</p>

DRAWING	C1.01	SEVENTY ACRES, LLC	PROJECT NO.	840-050
		THE 435	DATE: 08-29-18	
COVER SHEET		ENGINEERS / SURVEYORS	DATE: 11-15-18	PROJECT NO. 840-050

PROJECT DATA

THE 435

SEVENTY ACRES, LLC

ENGINEERS, SURVEYORS

GCV

1555 S. RAINBOW BLVD
LAS VEGAS, NV 89146

840-050

PROJECT NO. 840-050

DATE 01/29/2018

TIME 10:00 AM

BY J. L. HARRIS

FOR J. L. HARRIS

PROJECT THE 435

DESCRIPTION SEVENTY ACRES, LLC

DATE 01/29/2018

TIME 10:00 AM

BY J. L. HARRIS

FOR J. L. HARRIS

PROJECT THE 435

DESCRIPTION SEVENTY ACRES, LLC



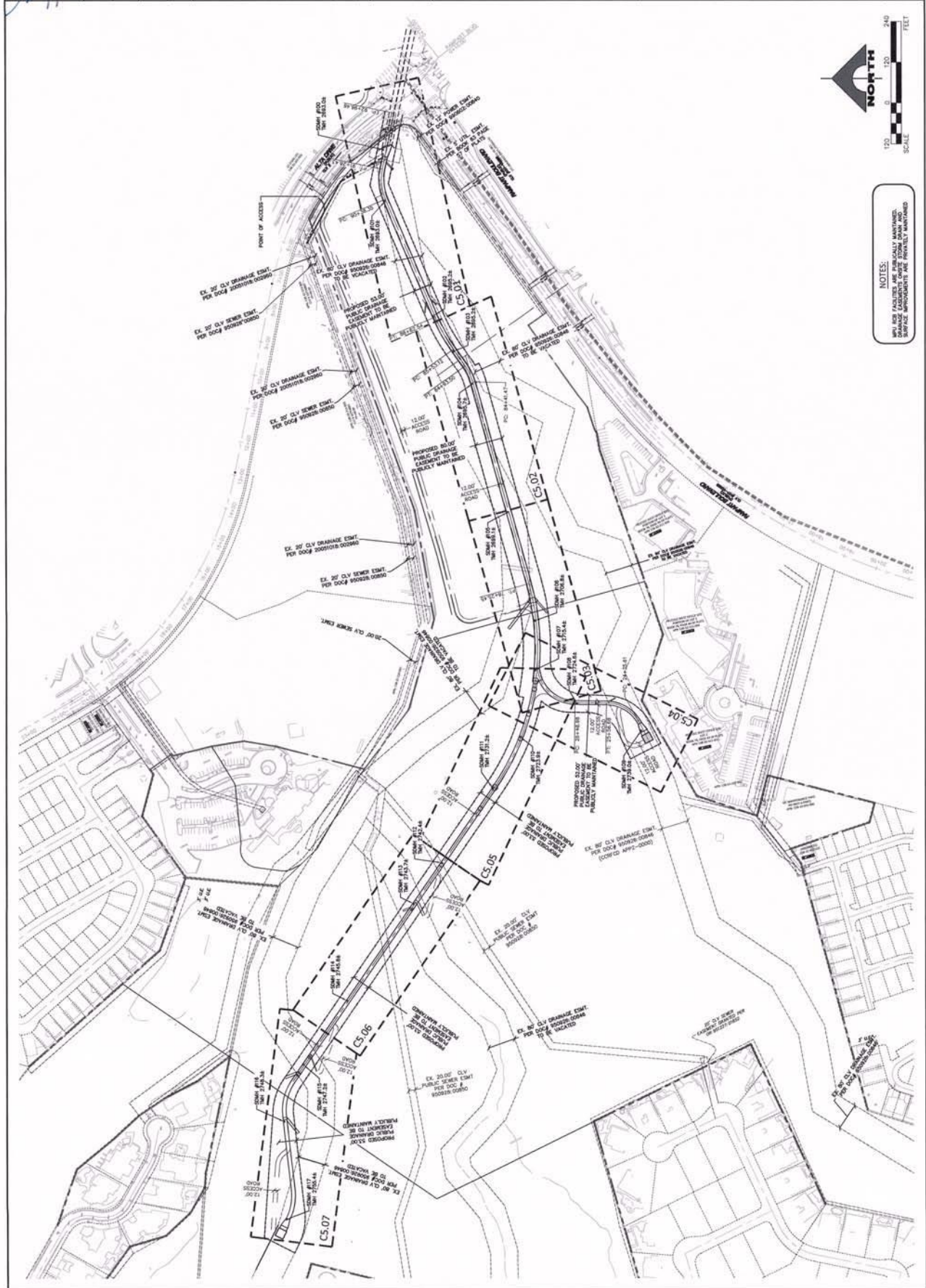
TDS SUBMITTAL



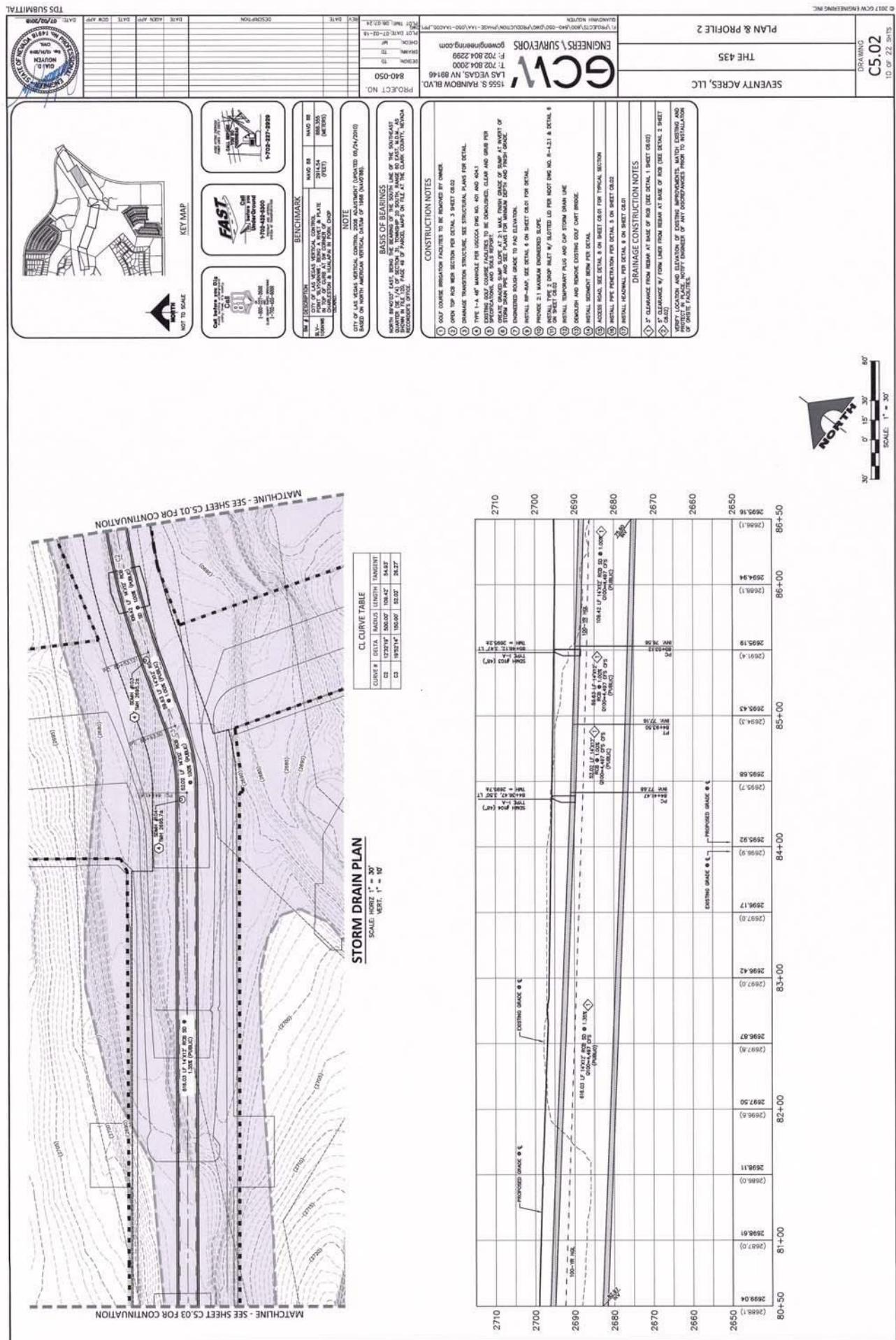
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05/02/2018	05/02/2018
05/03/2018	05/03/2018
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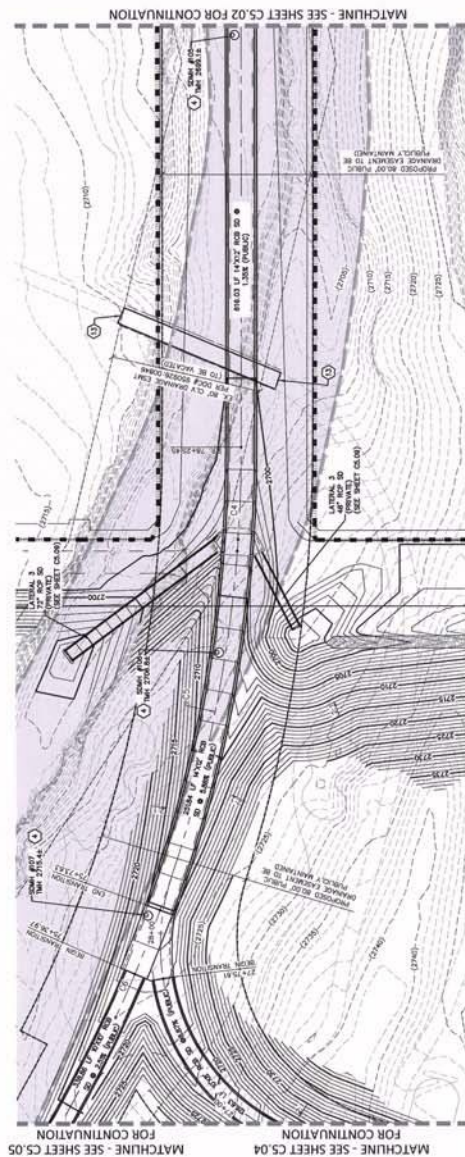
PROJECT NO. 840-950
 1555 S. RAINBOW BLVD.
 LAS VEGAS, NV 89146
 ENGINEERS & SURVEYORS
 F: 702.804.2298
 E: gowling@engineers.com

SEVENTY ACRES, LLC
 THE 435
 PLAN & PROFILE OVERALL
 DRAWING C5.00
 8 OF 22 SHEETS

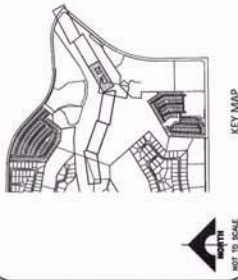
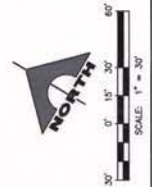
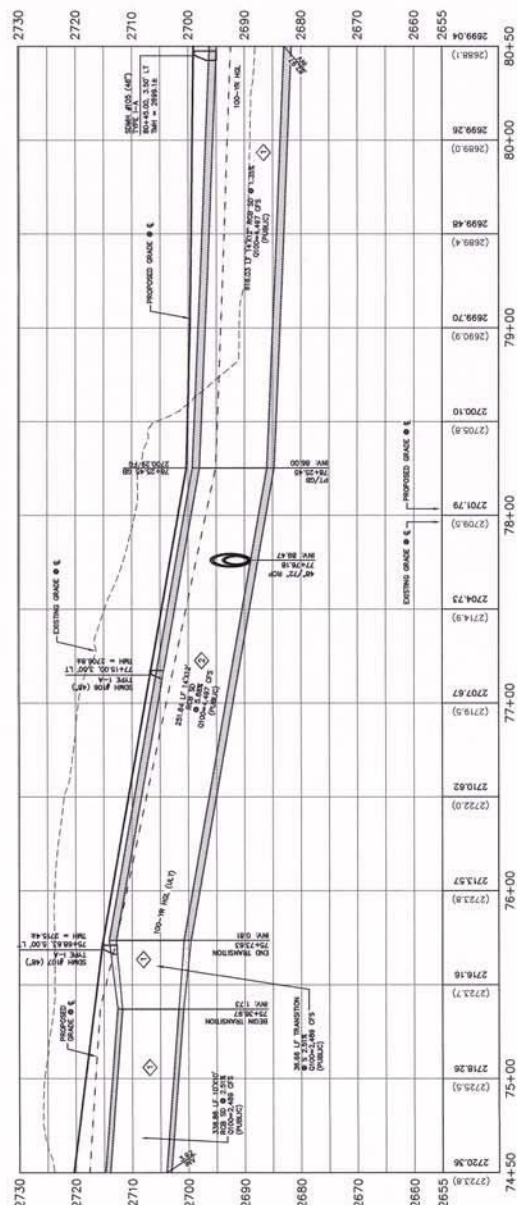


NOTES:
 1. ALL NEW FACILITIES ARE PUBLICLY MAINTAINED.
 2. ALL EXISTING FACILITIES ARE PRIVATELY MAINTAINED.
 3. SURFACE IMPROVEMENTS ARE PRIVATELY MAINTAINED.





CURVE #	DELTA	RADIUS	LENGTH	TANGENT
04	49°50'20"	720.00'	827.34'	3305.15'
05	49°50'20"	720.00'	827.34'	3305.15'
06	49°50'20"	720.00'	827.34'	3305.15'



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toll free
anywhere in the
U.S.

BENCHMARK			
BM #	DESCRIPTION	NAVD 88	NAVD 88
SLV-1	CITY OF LAS VEGAS VERTICAL CONTROL POINT "STATIONING BEING A STREET & PLATE (CORNER) OF INTERSECTION OF CHARLESTON & HULMAN IN PARK CIRCLE	2914.34	688.355 (METHOD)

15-00001

NOTE

CITY OF LAS VEGAS VERTICAL CONTROL 2008 ADJUSTMENT (UPDATED 06/29/2010)

BASIS OF BEARINGS
NORTH BRADSHAW EAST, BEING THE BEARING OF THE SOUTH LINE OF THE SOUTHEAST QUARTER (SE 1/4) OF SECTION 21, TOWNSHIP 30 SOUTH, RANGE 60 EAST, M.24M. AS SHOWN IN FILE 120, PAGE 48 OF PARCEL MAPS ON FILE AT THE CLARK COUNTY, NEVADA RECORDER'S OFFICE.

CONSTRUCTION NOTES

- ① GOLF COURSE IRRIGATION FACILITIES TO BE REMOVED BY OWNER.
- ② OPEN TOP RICH WOOD SECTION PER DETAIL 3 SHEET C6-02
- ③ DRAINAGE TRANSITION STRUCTURE. SEE STRUCTURAL PLANS FOR DETAIL.

7. EXISTING GOLF COURSE FACILITIES TO BE DEMOLISHED, CLEAR AND GRADE PER DETAIL 8.
8. CREATE GRADED SLOPE DETAIL 2.1 MAX. FILL DEPTH OF 5'0" SLUMP AT INSET OF STORM DRAIN PIPE AND SET PLANS FOR MANHOLE DITCH AND TIE-IN GRADE.
9. EXISTING ROUGH GRADE TO FILL AND ELEVATION.
10. EXISTING ROUGH GRADE TO FILL AND ELEVATION.
11. INSTALL 18" DIA. SEE DETAIL 4 ON SHEET GOLF FOR DETAIL.
12. PROVIDE 2.1' MANHOLE ENLARGED SLOPE.
13. INSTALL PIPE 2' DROP SLOPE 1/8" SLOTTED 10' PER MTD CWD NO. 8-4-2.1 & DETAIL 8 ON SHEET G-023
14. INSTALL TEMPORARY PLUG AND CAP STORM DRAIN LINE
15. DITCHING AND REMOVE EXISTING GOLF CART BRIDGE.

15 ACCESS ROAD, SEE DETAIL 8 ON SHEET C&D FOR TYPICAL SECTION

16 INSTALL PIPE PENETRATION PER DETAIL 5 ON SHEET C&D

17 INSTALL MEADOW PER DETAIL 9 ON SHEET C&D

DRAINAGE CONSTRUCTION NOTES

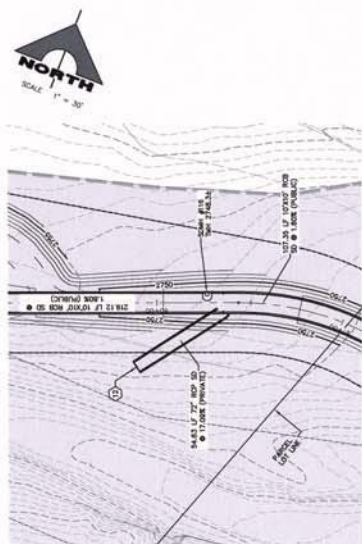
2. 5" CLEARANCE W/ FORM LINER FROM REBAR AT BASE OF PIVOT (SEE DETAIL 2 SHEET C&U)

VERIFY LOCATION AND ELEVATION OF EXISTING IMPROVEMENTS, MATCH EXISTINGS AND PROTECT IN PLACE, NOTIFY OWNER OF ANY DISCREPANCIES PRIOR TO INSTALLATION OF CURB FACILITIES.

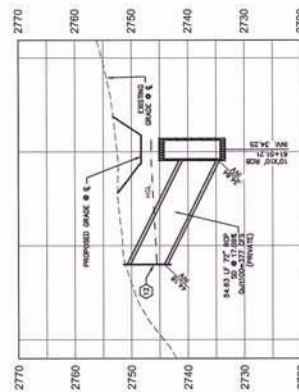
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REPLY APP 1436

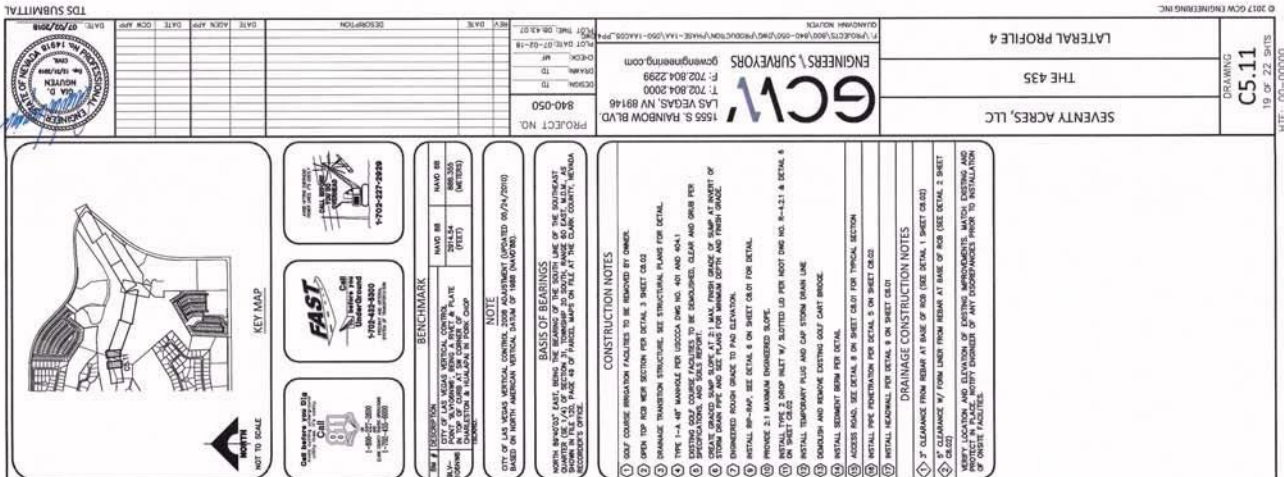
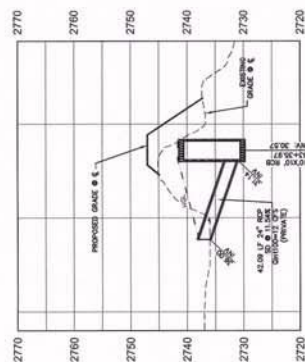




STORM DRAIN - LATERAL 8



STORM DRAIN - LATERAL 9



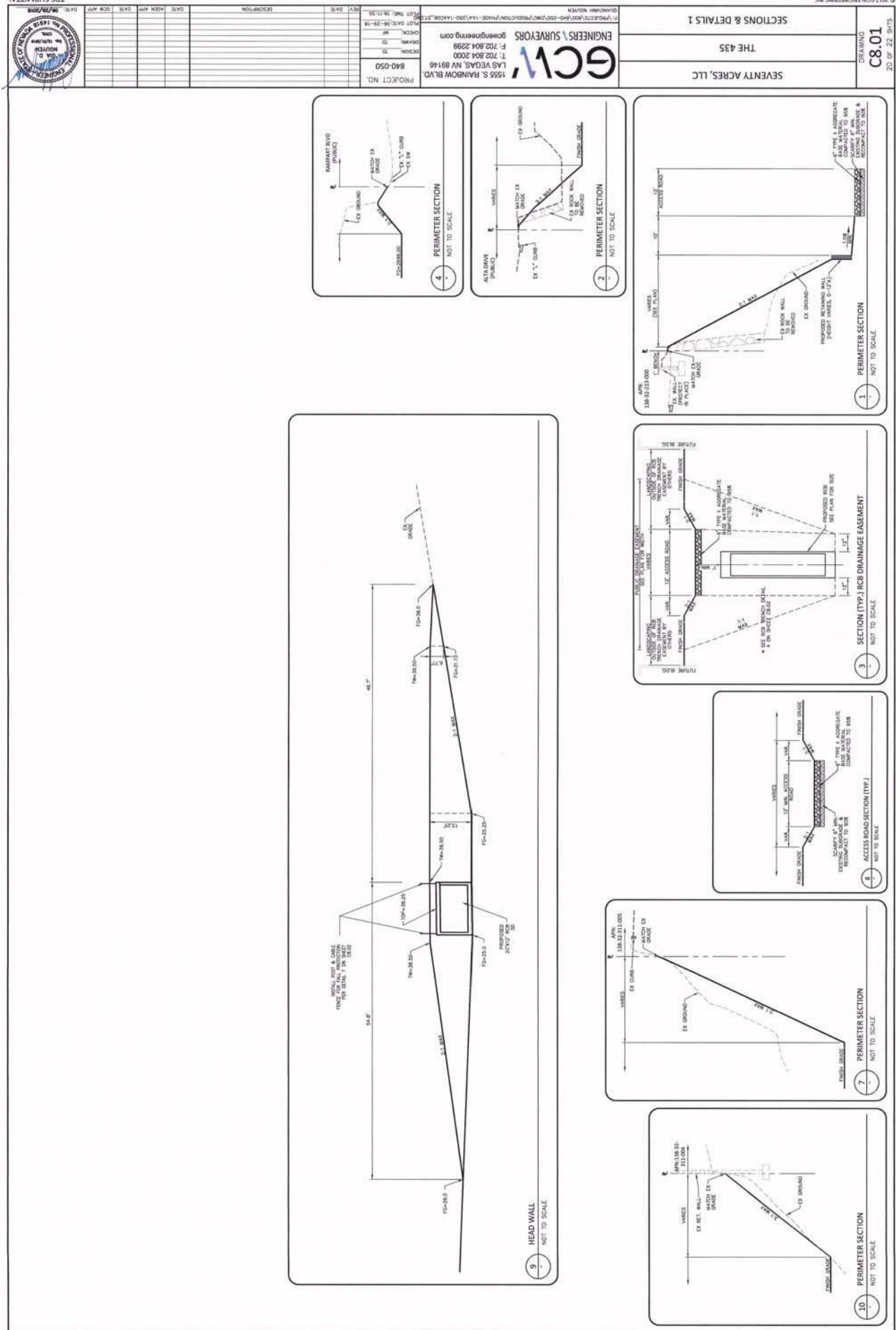


EXHIBIT “YYYYYY-12”

CITY OF LAS VEGAS		DATE:
INTER-OFFICE MEMORANDUM		July 26, 2018
TO: Land Development Services Department of Building & Safety		FROM: Jennifer Shinn, P.E. Flood Control Engr. Associate Department of Public Works
SUBJECT:	Drainage Study for:	
	The 435 formerly The SEVENTY	
Cross Streets:	SWC of Rampart & Alta	
File Number:	F:\Depot\DSMemos\DS4787D.ZNA.doc	
Parcel Number:	138-32-301-005, 006, 210-008	
Zoning Action:	SDR-62393; GPA-62387; ZON-62392	
FEMA Flood Zone	YES	X NO
Proposed Storm Drain	YES	X NO
		COPIES TO: GCW Engineers Seventy Acres LLC Bart Anderson, P.E., DevCo CCRFCD

HISTORY	DATE RECEIVED	DATE REVIEWED	COMMENTS	REVIEW FEES	FEES PAID Payment Trn #
1 st Submittal	3/3/2016 & 3/9/2016	3/23/2016	See Comments Below	\$400.00	425231: \$400
2 nd Submittal	9/18/17	11/9/2017	See Comments Below	\$400.00	490193: \$400
3 rd Submittal	1/11/18	2/1/2018	See Comments Below	\$400.00	492825: \$400
4 th Submittal	7/2/2018	7/26/2018	See Comments Below	\$400.00	497041: \$400
TOTAL FEES (LDDRS):				\$1600.00	----

REMARKS: This site development is within a **FEMA SPECIAL FLOOD HAZARD AREA, Zone A**. No permits of any kind will be issued for this project until a **Conditional Letter of Map Revision (CLOMR/CLOMR-F)** is received from FEMA.

4th Submittal: Redesign and evaluation of proposed storm drain system design.

The Drainage Study for the subject project has been reviewed and:

	is approved subject to conformance to all City standards and the following conditions:
X	must be resubmitted or supplemented including the following:
	is conditionally approved subject to Clark County Regional Flood Control District concurrence.
	is conditionally approved subject to NDOT concurrence.

- Based on the WSPG models, the velocity head and super elevation depth in Mainline 1 and Mainline 2 result in additional hydraulic pressure in the system that is not accounted for in the current design. Provide conceptual structural details of the storm drain improvements (Mainline, manholes, etc.) to address the hydraulic pressures and high velocities. CLV Flood Control review of the conceptual structural details is required prior to conditional approval of the drainage study.

2. Horizontal curvature information has been included in the WSPG model for Mainline 1, but no super elevation is shown in the results. The super elevation depth and velocity head results are needed to estimate the additional hydraulic pressure in the system and is to be incorporated in the storm drain system structural design.
3. The design of the storm drain system shall include the impacts of super elevation to the established HGL. As an example, the WSPG model for Mainline 2 shows an 8 foot super elevation depth that needs to be added to the HGL shown.
4. Transition No 19 presented in the WSPG model shows a transition structure length of 30 feet. The model of this transition does not adequately reflect the proposed design per C5.01 since this is not a symmetrical transition structure. Provide calculations to evaluate the hydraulic performance of this transition structure as well as its impact to the water surface elevation.
5. A post-project condition HEC-RAS model is required to show how the proposed, new SFHA Zone A ties into the existing SFHA Zone A areas. Provide an exhibit to reflect the post-project condition model and include a summary table. Clearly indicate the SFHA Zone A areas to remain, proposed SFHA Zone A tie-in, and SFHA Zone A to be removed.
6. Provide calculations to support the water surface elevation shown on C5.04 and C5.07 at the entrances of Mainline 1 and Mainline 2. It appears that the water surface elevations shown were obtained directly from the WSPG model outputs. Supporting calculations need to be provided to verify the water surface elevations presented adequately represent the flow entering the proposed improvement from the natural channels.
7. Due the extension of the storm drain system, provide a grated access structure along Mainline 1 upstream of the junction structure. Revise the drainage easement to include this area and provide a maintenance road to access structure.
8. Provide WSPG models for the newly proposed storm drain system using a Manning's n-value of 0.013 in order to identify critical sections of storm drain with high velocities. Once these areas have been identified, utilize the combined n-values as discussed in the response letter to reflect erosion mitigation measures. The models with the combined n-values shall also utilize an n-value of 0.015 for the rest of the storm drain that does not require erosion mitigation for sensitivity analysis.
9. The .WSX file for "Main0626" (Mainline 1) WSPG models have been provided with this submittal. Provide the typical input and output files for the "Main0626" WSPG models for the interim and ultimate conditions in order to verify input and output information.
10. Provide WSPG models of the interim condition reflecting the 20'x14' RCB entrance and transition to 10'x10' RCB for Mainline 1 and the 20'x12' RCB entrance and transition to 10'x8' RCB for Mainline 2.
11. Provide a Standard Form 4 for the basis of the HEC-1 model for the interim condition.
12. Revise FIG8R to match the WSPG model for Mainline 1 reflecting the combined n-value of 0.023 for WSPG stations -7825.45 and -7573.63.
13. It is noted that Mainline 2 was modeled as the system extended for future conditions. Discuss/provide the future design parameters the model was based upon.
14. Provide calculations to support the design of the 2:1 slope and verify that the ground cover material is sufficient for conveying the flows entering the Mainline 1 and 2 systems. Provide erosion protection based upon velocities.
15. Verify the velocities at all sumps of the lateral facilities to ensure erosion is mitigated and provide Best Management Practices accordingly.

16. Provide sediment control at inlet structures of Mainline 1 and Mainline 2.
17. It is noted that maintenance access has been provided for Lateral 5 (6'x6' RCB) and Lateral 9 (24" RCP) but not for Lateral 3 facilities. Review and revise accordingly.
18. Show the location of Section 1 on FIG15.
19. Update the inlet calculations to include the corresponding Facility numbers (e.g. 24 inch RCP – Facility 7A).
20. Laterals 5, 7, and 8 have velocities that exceed the maximum allowable velocity of 25 feet per second based on design slopes. Revise the lateral slopes accordingly to meet criteria.
21. The future minimum finished floor elevations of the southern portion of the proposed lots must be higher than the road grades of the future road. Future road grades (CL and TC elevations) are not apparent, therefore the minimum finished floor elevations cannot be verified to meet criteria.
22. Show future road grades on profiles.
23. Remove the note for temporary plug and cap for the 6' x 6' RCB as it appears it is proposed to convey interim flows.
24. Label Laterals 5 through 9 on the plan and profile to correspond to the lateral profiles on Sheets C5.010 and C5.11.
25. Provide stationing on all lateral profiles. Lateral profiles shall be based on the mainline stationing with corresponding offsets and angles.
26. SDMH #101 and #102 are called out as Type I manholes on the profile but the plan references Construction Note 4 which calls out Type I-A. Review and revise accordingly.
27. Revise the Construction Notes to remove any notes that are no longer applicable to the current proposed design (e.g. notes 2 and 14) and provide Construction Note labels on the plans (e.g. notes 3, 16, and 17)
28. Provide structural details for the RCB construction including the sections of the tined invert and corrugated wall faces.
29. Provide structural details for shallow manholes.
30. Provide structural details for all transition structures.
31. Provide structural details for connection into existing dual 12'x12' RCBs.
32. Provide structural details for the proposed headwall at the 20' x 12' RCB storm drain.
33. Provide a note on the structural details that specifies 6000-psi strength concrete for all segments of storm drain where velocities exceed 25 feet per second based on the n-value of 0.013.
34. It appears that the HGL is within 1 foot of the proposed grade at the transition structure for the confluence of Mainline 1 and Mainline 2. Review and revise accordingly.
35. Verify that the minimum allowable cover over the storm drain is 1 foot or greater at any point along the system, specifically between stations 75+50 to 79+00.
36. The engineer must review the pipe hydraulics to verify system design to keep the HGL 18 inches below finished grade. Where the HGL is less than 18 inches, the manholes shall have hinged and grated lids with extended concrete collars tied to the box.

37. Provide fall protection at the Mainline 1 inlet structure as well as the bigger interim facilities.
38. Provide access to all storm drain manholes from the main access path along the system. Include turnaround areas where the access road dead-ends.
39. It appears there is a storm drain manhole shown on the plans at approximate station 69+28 but not labeled or shown in the profile. If no manhole is proposed at this location, revise the location of storm drain access manhole SDMH #111 to be spaced a maximum of 400 feet from SDMH #113.
40. Revise CLV General Note 21 (effective June 4, 2018) to reference the applicable Final Location Map option for this project.
41. All manholes in unimproved/rough graded areas shall include a locking lid with extended concrete collar, set above grade.
42. Waterproofing of the RCB is required where future landscaping is anticipated and outside of future roadway improvements.

The following comments are repeated to reflect routine items previously acknowledged by the Engineer.

43. This site development is located within a FEMA SPECIAL FLOOD HAZARD AREA, Zone A. **No permits will be issued until a Conditional Letter of Map Revision (CLOMR/CLOMR-F) is received from FEMA. Permits may be issued upon the receipt of Conditional Letter of Map Revision (CLOMR or CLOMR-F) from FEMA.**
44. A Letter of Map Revision (LOMR/LOMR-F) must be obtained from FEMA after the completion of any project within a FEMA Special Flood Hazard Area, Flood Zone "A". The bonded improvements shall include a line item of **\$50,000.00** for the LOMR. The bonded improvements will not be released until the LOMR/LOMR-F is obtained from FEMA and filed with the City of Las Vegas.
45. The site is located within the Flood Zone A and is adjacent to an existing or proposed *Clark County Regional Flood Control District (CCRFCD)* master planned facility. Therefore, CCRFCD concurrence is required prior to final approval of the drainage study.

Structural calculations of facilities must be approved by the *City* prior to submittal to *Clark County Regional Flood Control District* for their review and concurrence.
46. Please obtain necessary 404 permits from US Army Corps of Engineers and provide a copy of the permit to City of Las Vegas Flood Control Section prior to issuance of the grading permit. Contact the St. George Field Office of the US Army Corps of Engineers for permit information.
47. Provide complete *Plans and Project Specifications* for approval by the *City of Las Vegas*. The Structural Plans and Details shall be a part of the Civil Improvement Plan set. This project is considered as a *Capital Improvement Project (CIP)* with developer funding.
48. Structural plans for the proposed storm drain improvements and pertinent flood control facilities must be submitted for review. Provide a soils report, structural calculations and specifications, two wet stamped structural sets, and a grading plan to the *Building Department* for processing. The engineer must provide a copy of *Building Department* approval of the structures to Regional Flood prior to their concurrence and to *Flood Control* prior to final acceptance of the drainage study.
49. All proposed improvements associated with the Storm Drain facilities shall be bonded and inspected. This project shall require Special Inspection. Coordinate the requirements of and the Agreements needed for Special Inspection with the Building Department.
50. The proposed improvements show drainage facilities of a size that must be reviewed for access and maintenance concerns. The engineer must submit an extra set of improvement plans to the *City*

Streets & Sanitation Department for their review and comments. *Streets & Sanitation Department's* approval must be secured prior to the conditional drainage study approval.

51. Provide new public drainage easements for the area of the site impacted by the proposed MPU facility improvements. The easement shall note that the public drainage improvements (MPU facilities) are publicly maintained and all onsite storm drain and surface improvements are privately maintained and the easement must be dedicated and recorded by separate document prior to the final acceptance of the improvement plans. Provide legal description and an exhibit of the drainage easement to Flood Control and *Rae Heller* (702-229-2139) of *City of Las Vegas Right of Way Section* for the recordation process after the subject drainage study is conceptually approved. The existing drainage easements shall be vacated by separate action and the recording of the new easements shall be done consecutively.
52. Technical drainage studies are required for each of the future development super pads. The technical drainage studies for the developments may not be submitted until the conditional approval of this pertinent infrastructure drainage study is obtained. Final approval for the infrastructure study must be obtained prior to conditional approval of the impacted development super pad drainage studies.
53. This project currently has no Proposed Buildings or Structures. Should the project propose changes to this design assumption, then the Engineer is to update the drainage study detailing the flood zone impacts and provide addresses for each building in a FEMA Flood Hazard Zone prior to obtaining a grading permit. This information is necessary to insure that the elevation certificates are provided for each address prior to completion of construction. This information is required until such time as a LOMR is approved that removes the development from the SFHA.

Flood Control understands that this overall project will be developed in Phases. The following comments are repeated to reflect items that shall be addressed in future study updates as the Phases develop.

54. Proposed storm drain laterals have been identified to collect flows from Peccole West Lot 9 and Queensridge Fairway Homes. Extend the storm drain system to collect the 100-year flows from these adjacent subdivisions.
55. Continue to coordinate the MPU facility changes that are proposed with this development.

NOTE: Please be advised that all land surface area disturbances over 1 acre or any area adjacent to a water way must submit to the *Nevada Division of Environmental Protection* a "Notice of Intent" to discharge that certifies a stormwater pollution prevention plan has been developed and is maintained on site; for inclusion in the Stormwater General Permit No. NVR100000. A phased construction unit in a contiguous subdivision is considered under construction until all stripped or disturbed surface areas have been covered by paving, building construction or planting. For more information, including forms and applications see <http://ndep.nv.gov/bwpc/storm01.htm> or call (775) 687-9429.

NOTE: The engineer must submit the drainage study to FEMA for a Conditional Letter of Map Revision (CLOMR). A favorable CLOMR must be obtained prior to the issuance of any permits. This site is located in a **FEMA Zone A**. *Clark County Regional Flood Control District* (CCRFCD) review and approval is required prior to recordation of final map or issuance of building/grading permits. The Engineer must send a copy of the report to the CCRFCD for review. **The developer/engineer must also obtain a Letter of Map Revision (LOMR) using the approved drainage study as technical support to inform FEMA of the modifications within the flood zone. The approved LOMR must be submitted to the *City of Las Vegas* prior to the release of the bond.** FEMA Elevation Certificates, showing as-built finish floor elevations, must be completed for each building in the FEMA A Zone. The certificate must be submitted to the *City of Las Vegas Flood Control Section* prior to scheduling a framing inspection.

END OF REMARKS
JKS/PBJ

T/R/S: T20S/R60E/12
AREA L-32

EXHIBIT “YYYYYY-13”

840-050



MEETING MINUTES

Prepared By: Steve Jones

702-804-2130
sjones@gcwengineering.com

Re: The 435 TDS
Design Workshop on 435 TDS 7/26/2018 Comments

Place: City of Las Vegas Public Works – Opal Conference Room (7th Floor)

Date: August 13, 2018 Time: 9:00 am to 10:30am

Attendees: Peter Jackson, CLV
Jennifer Shinn, CLV
Mark Sorensen, CLV
Steve Jones, GCW
Scott Plummer, GCW

General Discussion Items:

- Rules state when processing a Technical Drainage Study (TDS) through the CLV, that zoning/planning approval of the entitlements on a property are required to be approved prior to conditional approval can be given on a TDS. CLV staff discussed that due to the ongoing litigation standing on the entitlements for the property, that direction from the City Manager's office was that City staff is not authorized to provide conditional approval on this TDS. CLV also discussed that review of any addendums or responses to comments can proceed; however, until litigation on the entitlements is resolved, conditional approval can't be issued on this TDS.
- This project is required to submit and receive approval on a CLOMR thru FEMA. Typically on a project like this where improvements are the reason for the map revision request, the City has authorization to sign off on the community acknowledgement block on the FEMA forms with a conditional drainage study approval. If the TDS is not able to receive conditional approval per above discussion, CLV staff will have to review if it has the authority to sign the community acknowledgement block on the FEMA forms required for CLOMR submittal.
 - CLV staff did note that if the owner wanted to complete a LOMR application based on existing condition hydraulics thru the property, an approved TDS may not be necessary.
- GCW inquired why this comment letter produced so many comments on the storm drain design that they saw the design similarly presented in the previous submittals, and very few comments were regarding the storm drain extended through the site. CLV clarified that the previous 2 submittals were addressing a proposed interim collector design near the boundary of the 17.5 acres known as The 435 and the storm drain was only presented as a concept for the engineer's use to ensure proper design of the storm drain through the The 435 property. Now that the design is shown proposed, and the engineer had changed design parameters with a smaller size RCB and had addressed other commented concerns, CLV staff communicated that this was considered a fresh review of the storm drain in the July 2018 comment letter. CLV staff iterated that the design as presented is an approvable design, much preferred over the last 2 submittals

1555 South Rainbow Boulevard
Las Vegas, Nevada 89146



702.804.2000
702.804.2299



info@gcwengineering.com
gcwengineering.com

with the interim open channel collector concept and also the design presented in the 1st submittal from 2016 because the high velocities are managed more effectively. The CLV staff also discussed that the comments at this stage are more for clarification, in which GCW noted this meeting is intended as a design workshop to ensure any clarification needed is provided to the CLV staff in an effort to receive conditional approval on the TDS.

Comment No.	Comment	Discussion/Response
1	Based on the WSPG models, the velocity head and super elevation depth in Mainline 1 and Mainline 2 result in additional hydraulic pressure in the system that is not accounted for in the current design. Provide conceptual structural details of the storm drain improvements (Mainline, manholes, etc.) to address the hydraulic pressures and high velocities. CLV Flood Control review of the conceptual structural details is required prior to conditional approval of the drainage study.	CLV noted that since the RCBs are minimally covered, extra RCB design such as strengthening manhole designs on top of the RCB, or stronger concrete is required to protect against high HGLs and velocities in the RCB. Therefore, CLV is requiring some further structural information such as concept details to show adequate design parameters. It was agreed that GCW would provide 30% level structural details for this project in the next submittal.
2	Horizontal curvature information has been included in the WSPG model for Mainline 1, but no super elevation is shown in the results. The super elevation depth and velocity head results are needed to estimate the additional hydraulic pressure in the system and is to be incorporated in the storm drain system structural design	GCW concurred that although the WSPG program is supposed to compute additional bend/super-elevation losses in a closed storm drain, it was observed thru internal calculation that this additional loss is negated. Therefore, it was agreed that GCW will perform an additional CCRFCD Manual super-elevation calculation at bends and arithmetically add it to the HGL currently shown on the plans. GCW would ensure that in the next submittal the FG over the RCB would be minimum 18-inches above the new HGL accounting for super-elevation in order to protect the structural integrity of the RCB including manhole risers and pipe penetration collars. Additionally, GCW would account for the velocity head by using the energy grade line thru the confluence structure of the two main trunks as the design HGL in the structure.
3	The design of the storm drain system shall include the impacts of super elevation to the established HGL. As an example, the WSPG model for Mainline 2 shows an 8 foot super elevation depth that needs to be added to the HGL shown	GCW agreed to adjust the plans to show the HGL as the WSPG water depth plus additional CCRFCD Manual super-elevation depth. GCW also discussed that all bends in the design meet CCRFCD Manual super-elevation criteria.
4	Transition No 19 presented in the WSPG model shows a transition structure length of 30 feet. The model of this transition does not adequately reflect the proposed design per C5.01 since this is not a symmetrical transition structure. Provide calculations to evaluate the hydraulic performance of this transition structure as well as its impact to the water surface elevation	After discussion, CLV understood that the project proposes to connect directly into the existing headwall of the dual 12'x12' RCBs and not reconstruct any portion of the skewed existing dual RCBs. GCW will clarify design in the conceptual structural detail of the connection structure, and no additional hydraulic calculations are necessary.
5	A post-project condition HEC-RAS model is required to show how the proposed, new SFHA Zone A ties into the existing SFHA Zone A areas. Provide an exhibit to reflect the post-project condition model and include a	GCW agreed to provide a post-project HEC-RAS thru the existing condition sections previously provided upstream of the project to the proposed sump prior to flow entering the storm drain. The downstream boundary condition in the sump will be established as

Comment No.	Comment	Discussion/Response
	summary table. Clearly indicate the SFHA Zone A areas to remain, proposed SFHA Zone A tie-in, and SFHA Zone A to be removed	the improved inlet WSE. GCW discussed and will summarize in the next submittal that the FEMA mapping tie-in will begin where the difference in WSE between existing and proposed conditions is 1-ft or less, per FEMA criteria. The Figure 8R previously submitted showing the mapping tie-ins will be blown up to better show the proposed FEMA mapping.
6	Provide calculations to support the water surface elevation shown on C5.04 and C5.07 at the entrances of Mainline 1 and Mainline 2. It appears that the water surface elevations shown were obtained directly from the WSPG model outputs. Supporting calculations need to be provided to verify the water surface elevations presented adequately represent the flow entering the proposed improvement from the natural channels	GCW discussed its method for computing WSE and determining improved inlet design was by inlet/outlet control with minimum computed CCRFCD Manual transition length to the larger RCB opening, because extending the WSPG model to the upstream terminus of the improved inlet resulted in unreasonable results such as a larger size inlet than the inlet existing at Alta for almost twice the amount of flow. Now that the methodology is understood, CLV staff agreed to re-review these areas after GCW sends the unreasonable hydraulic model.
7	Due the extension of the storm drain system, provide a grated access structure along Mainline 1 upstream of the junction structure. Revise the drainage easement to include this area and provide a maintenance road to access structure	GCW noted that this request was identified in previous meetings, and the next submittal will provide accordingly. The grate elevation shall be minimum 18-inches above the HGL with super-elevation.
8	Provide WSPG models for the newly proposed storm drain system using a Manning's n-value of 0.013 in order to identify critical sections of storm drain with high velocities. Once these areas have been identified, utilize the combined n-values as discussed in the response letter to reflect erosion mitigation measures. The models with the combined n-values shall also utilize an n-value of 0.015 for the rest of the storm drain that does not require erosion mitigation for sensitivity analysis	CLV clarified that it agrees the design presented in the last submittal is acceptable with 0.015 roughness and rougher 0.023 where corrugated sides is proposed. CLV only requests the 0.013 manning's roughness model as a side model for adhering to CCRFCD criteria that RCBs are to be analyzed with 0.013 roughness. The results of the 0.013 roughness model is to be used only for informational purposes to protect against potential abnormalities such as unusual hydraulic jumps, etc. If GCW finds any abnormalities, re-consultation with CLV may be required.
9	The .WSX file for "Main0626" (Mainline 1) WSPG models have been provided with this submittal. Provide the typical input and output files for the "Main0626" WSPG models for the interim and ultimate conditions in order to verify input and output information	The type of modeling program was clarified with CLV staff as an acceptable resource, which was agreed to. GCW volunteered to create a summary table that will help the CLV staff more easily review its results
10	Provide WSPG models of the interim condition reflecting the 20'x14' RCB entrance and transition to 10'x10' RCB for Mainline 1 and the 20'x12' RCB entrance and transition to 10'x8' RCB for Mainline2	CLV staff will re-review GCW methodology per discussion included in response to Comment #6.
11	Provide a Standard Form 4 for the basis of the HEC-1 model for the interim condition	GCW acknowledged the City's request, and will provide accordingly.
12	Revise FIG8R to match the WSPG model for Mainline 1 reflecting the combined n-value of 0.023 for WSPG stations -7825.45 and -7573.63	GCW acknowledged the City's request, and will provide accordingly.

Comment No.	Comment	Discussion/Response
13	It is noted that Mainline 2 was modeled as the system extended for future conditions. Discuss/provide the future design parameters the model was based upon	GCW discussed that its assumptions for the Mainline 2 hydraulic model extension was discussed and included in the 1st response to comments from September 2017. CLV concurred and determined the comment to be voided.
14	Provide calculations to support the design of the 2:1 slope and verify that the ground cover material is sufficient for conveying the flows entering the Mainline 1 and 2 systems. Provide erosion protection based upon velocities	Both CLV and GCW agreed for the potential of erosion or head-cutting down the 2:1 slope to the improved inlet. GCW agreed to extend the concrete with cut-off wall at its 2 major improved inlets up the 2:1 slope to the existing wash for erosion protection.
15	Verify the velocities at all sumps of the lateral facilities to ensure erosion is mitigated and provide Best Management Practices accordingly	CLV agreed that GCW could place riprap pads in the sumps to protect against erosion upstream of the lateral drains. Additionally, GCW will re-evaluate slopes of the lateral storm drains to eliminate high velocities (over 25-fps) in the storm drain to protect the pipe itself from erosion.
16	Provide sediment control at inlet structures of Mainline 1 and Mainline 2	GCW showed a similar means for sediment control at the improved inlet structures accepted on a similar project. CLV agreed that GCW could stage the bottom of the sump below the invert of the RCB opening by 2-ft, with a low flow DI and drain pipe for positive drainage.
17	It is noted that maintenance access has been provided for Lateral 5 (6'x6' RCB) and Lateral 9 (24" RCP) but not for Lateral 3 facilities. Review and revise accordingly	After review, GCW agreed to provide according to the CLV comment.
18	Show the location of Section 1 on FIG15	GCW acknowledged the City's request, and will provide accordingly.
19	Update the inlet calculations to include the corresponding Facility numbers (e.g. 24 inch RCP – Facility 7A).	GCW acknowledged the City's request, and will provide accordingly.
20	Laterals 5, 7, and 8 have velocities that exceed the maximum allowable velocity of 25 feet per second based on design slopes. Revise the lateral slopes accordingly to meet criteria	GCW acknowledged the City's request, and will provide accordingly. Additionally, CLV agreed that if the slope in the pipe was reduced to minimum (0.5%) and high velocities still result, GCW could utilize 1-inch sacrificial concrete as a means for protection of the pipe. CLV requests that 6,000 psi concrete also be specified in these areas.
21	The future minimum finished floor elevations of the southern portion of the proposed lots must be higher than the road grades of the future road. Future road grades (CL and TC elevations) are not apparent, therefore the minimum finished floor elevations cannot be verified to meet criteria	CLV and GCW agreed that future studies will address minimum finished floor elevations on the site. Additionally, it was also discussed that future finished floor elevations do not need to be higher than the future road as the comment suggests; however, the engineer will be required to mitigate for these areas where the road is higher by other improvements such as floodwalls, waterproofing, etc. that will be reviewed in the future studies.

Comment No.	Comment	Discussion/Response
22	Show future road grades on profiles	CLV staff clarified that the intent of showing the future road grades is to make sure that the manholes are constructed in a manner that minimizes re-construction of the entire cone/collar when they are adjusted in the future. GCW agreed to show the manholes an adequate height above the proposed rough grade and show a conceptual road profile to enough accuracy to design manholes with some permanence. CLV will allow stipulations on the plans by GCW to ensure that roadway design on the site could change in the future when the buildings are detailed graded.
23	Remove the note for temporary plug and cap for the 6' x 6' RCB as it appears it is proposed to convey interim flows	GCW acknowledged the City's request, and will provide accordingly.
24	Label Laterals 5 through 9 on the plan and profile to correspond to the lateral profiles on Sheets C5.010 and C5.11	GCW acknowledged the City's request, and will provide accordingly.
25	Provide stationing on all lateral profiles. Lateral profiles shall be based on the mainline stationing with corresponding offsets and angles	GCW acknowledged the City's request, and will provide accordingly.
26	SDMH #101 and #102 are called out as Type I manholes on the profile but the plan references Construction Note 4 which calls out Type I-A. Review and revise accordingly	GCW acknowledged the City's request, and will provide accordingly.
27	Revise the Construction Notes to remove any notes that are no longer applicable to the current proposed design (e.g. notes 2 and 14) and provide Construction Note labels on the plans (e.g. notes 3, 16, and 17).	GCW acknowledged the City's request, and will provide accordingly.
28	Provide structural details for the RCB construction including the sections of the lined invert and corrugated wall faces	CLV staff agrees that the structural details required for next submittal are conceptual in nature, similar to 30% design plans on a CIP. GCW will comply.
29	Provide structural details for shallow manholes	CLV staff agrees that the structural details required for next submittal are conceptual in nature, similar to 30% design plans on a CIP. GCW will comply.
30	Provide structural details for all transition structures	CLV staff agrees that the structural details required for next submittal are conceptual in nature, similar to 30% design plans on a CIP. GCW will comply.
31	Provide structural details for connection into existing dual 12'x12' RCBs	CLV staff agrees that the structural details required for next submittal are conceptual in nature, similar to 30% design plans on a CIP. GCW will comply.
32	Provide structural details for the proposed headwall at the 20' x 12' RCB storm drain	CLV staff agrees that the structural details required for next submittal are conceptual in nature, similar to 30% design plans on a CIP. GCW will comply.
33	Provide a note on the structural details that specifies 6000-psi strength concrete for all segments of storm drain where velocities exceed 25 feet per second based on the n-value of 0.013	GCW acknowledged the City's request, and will provide accordingly. Note that the comment was corrected by CLV staff to provide 6,000-psi note on the areas with high velocities determined in the 0.015 roughness model.

Comment No.	Comment	Discussion/Response
34	It appears that the HGL is within 1 foot of the proposed grade at the transition structure for the confluence of Mainline 1 and Mainline 2. Review and revise accordingly	GCW will be adjusting all FG on the project to be minimum 18-inches above the design HGL (adjusted per discussions in Response to Comment #2). Therefore, no additional structural design is required.
35	Verify that the minimum allowable cover over the storm drain is 1 foot or greater at any point along the system, specifically between stations 75+50 to 79+00	GCW will be adjusting all FG on the project to be minimum 18-inches above the design HGL (adjusted per discussions in Response to Comment #2). Therefore, no additional structural design is required.
36	The engineer must review the pipe hydraulics to verify system design to keep the HGL 18 inches below finished grade. Where the HGL is less than 18 inches, the manholes shall have hinged and grated lids with extended concrete collars tied to the box	GCW will be adjusting all FG on the project to be minimum 18-inches above the design HGL (adjusted per discussions in Response to Comment #2). Therefore, no additional structural design is required.
37	Provide fall protection at the Mainline 1 inlet structure as well as the bigger interim facilities	CLV and GCW agreed that post and cable railing will be provided anywhere there is a vertical drop from the top of the 2 main trunk storm drains.
38	Provide access to all storm drain manholes from the main access path along the system. Include turnaround areas where the access road dead-ends	Larger areas for turnaround will be provided at the storm drain manholes on the transition structures, and access grate.
39	It appears there is a storm drain manhole shown on the plans at approximate station 69+28 but not labeled or shown in the profile. If no manhole is proposed at this location, revise the location of storm drain access manhole SDMH #111 to be spaced a maximum of 400 feet from SDMH #113	GCW acknowledged the City's request, and will provide accordingly.
40	Revise CLV General Note 21 (effective June 4, 2018) to reference the applicable Final Location Map option for this project	CLV staff provided GCW the applicable note to add onto the plans to satisfy comment.
41	All manholes in unimproved/rough graded areas shall include a locking lid with extended concrete collar, set above grade	CLV staff is requesting crossbar locking lid, similar to the sewer locking manhole detail, and GCW agreed to provide.
42	Waterproofing of the RCB is required where future landscaping is anticipated and outside of future roadway improvements	To further landscaping restrictions within public drainage easements, GCW agreed to add notes to the RCB trench detail that no deep rooted trees or 3-ft plus high trees are allowed directly over the RCB.
50	The proposed improvements show drainage facilities of a size that must be reviewed for access and maintenance concerns. The engineer must submit an extra set of improvement plans to the City Streets & Sanitation Department for their review and comments. Streets & Sanitation Department's approval must be secured prior to the conditional drainage study approval	Since there has been no response to review on the plans by Streets & Sanitation Department which is required for conditional approval of the TDS, GCW was tasked to schedule a meeting with Matthew Meyer to discuss the project prior to resubmittal.

EXHIBIT “YYYYYY-14”

From: [Todd Davis \(EHB Companies\)](#)
To: [SJones@gcwengineering.com](#); [SPlummer@gcwengineering.com](#)
Cc: [msorensen@LasVegasNevada.GOV](#); [okwon@LasVegasNevada.GOV](#); [jshinn@LasVegasNevada.GOV](#); [pjackson@LasVegasNevada.GOV](#); [Yohan Lowie \(EHB Companies\)](#); [Frank Pankratz \(EHB Companies\)](#); [bjerbic@lasvegasnevada.gov](#)
Subject: FW: The 435 TDS Comments Review Meeting
Date: Thursday, September 13, 2018 11:43:59 AM
Attachments: [image002.png](#)
[image003.png](#)
[image004.png](#)
[image006.png](#)
[image007.png](#)
[image002.png](#)
[image003.png](#)
[image004.png](#)
[image006.png](#)
[image008.png](#)
[image011.png](#)

Scott/Steve,

Seventy Acres LLC is OK with attaching both Peter's 8/21/18 email and Mark's 9/12/18 email to the August 13 dated GCW meeting minutes as CLV's comments to the minutes.

Thx, td

Todd D. Davis
General Counsel
EHB Companies LLC
1215 South Fort Apache, Suite 120
Las Vegas, NV 89117
702.940.6930 office
702.940.6931 fax
702.940.6938 direct
TDavis@EHBCompanies.com
www.EHBCompanies.com

Begin forwarded message:

From: Mark Sorensen <msorensen@LasVegasNevada.GOV>
Date: September 12, 2018 at 6:02:17 PM PDT
To: Steve Jones <SJones@gcwengineering.com>, Scott Plummer <SPlummer@gcwengineering.com>
Cc: Oh-Sang Kwon <okwon@LasVegasNevada.GOV>, Jennifer Shinn <jshinn@LasVegasNevada.GOV>, "Frank Pankratz (frank@EHBCompanies.com)" <frank@EHBCompanies.com>, "Yohan Lowie (EHB Companies)" <yohan@EHBCompanies.com>, Peter Jackson <pjackson@LasVegasNevada.GOV>
Subject: RE: The 435 TDS Comments Review Meeting

Hi Scott and Steve, we have been checking our e-mails over here in Flood Control Planning and it does not look like we have received the corrected minutes from the subject meeting yet addressing Peter's comments below (sent on August 21st).

Please send them at your earliest convenience.

LO 00009856

REPLY APP 1463

6496

Also, could you please let the minutes reflect that I had to leave the meeting in the first 5 minutes or so to attend another meeting?

And, in case there was any confusion, the first bullet would need to be *replaced in its entirety* with Peter's applicable paragraph below to accurately reflect the discussion as recollected by the CLV staff present.

Mark A. Sorensen, PE
Engineering Program Manager
Department of Public Works | City Engineering Division
Phone: 702-229-2203 | Cell 702-286-6954
333 N. Rancho, floor | Las Vegas, NV 89106



lasvegasnevada.gov



Your opinion is important! Click [here](#) to take a short survey

From: Peter Jackson

Sent: Tuesday, August 21, 2018 12:08 PM

To: Steve Jones <SJones@gcwengineering.com>; Scott Plummer <SPlummer@gcwengineering.com>

Cc: Mark Sorensen <msorensen@LasVegasNevada.GOV>; Oh-Sang Kwon <okwon@LasVegasNevada.GOV>; Jennifer Shinn <jshinn@LasVegasNevada.GOV>; Frank Pankratz <frank@EHBCompanies.com> <frank@EHBCompanies.com>; Yohan Lowie (EHB Companies) <yohan@EHBCompanies.com>

Subject: RE: The 435 TDS Comments Review Meeting

Steve and Scott;

Flood Control has reviewed the notes and has some concerns. Please revise the notes to reflect our understanding.

First bullet point

Revise the bullet point

Conditional Approval of a Technical Drainage Study (TDS) requires zoning/planning approval of the entitlements before CLV Flood Control can issue Conditional Approval of the TDS.

Flood Control advised that the 435 site entitlements are not currently approved based upon ongoing litigation, therefore Flood Control cannot grant conditional approval until the entitlements are approved.

Flood Control will continue to review TDS submittals based upon the engineer's submitted Addendum, however we will not conditionally approve the study until we have approved

LO 00009857

REPLY APP 1464

6497

entitlements.

Second Bullet Point

Revise the third sentence...

Flood Control cannot sign a CLOMR Community Acknowledgement without conditional approval of the TDS as the City is stating in the acknowledgement *"we find the completed or proposed project meets or is designed to meet all of the community floodplain management requirements.."*

Flood Control can review a CLOMR application with the supporting technical information, however the TDS that is used as the basis for the CLOMR shall be conditionally approved.

Revise the subset bullet point

CLV staff advised that the owner could apply for a LOMR of the site to accurately delineate the Special Flood Hazard Area from the current Zone A (without an established Base Flood Elevation (BFE)) to a Zone AE (with BFE's). This process, the City believes, would reduce the mapped flood zone and accurately map the risk associated based upon detailed information.

Comments

Add note before the comments.

The response to comments discussed are general in nature and any Addendum will provide detailed response with supporting information and technical data.

Comment #21 add note: That these plans are rough grade for future building areas in support of the master drainage facilities and any Finish Floor Elevations shall be established with the future TDS.

Thanks,

Peter Jackson, CFM

Senior Engineering Associate
City of Las Vegas | Dept. of Public Works
City Engineering Division, Flood Control Section
Development Service Center (DSC) 7th Floor
333 North Rancho Drive | Las Vegas, Nevada 89106



Work: 702-229-5266 Link: www.lasvegasnevada.gov

LO 00009858

6498

REPLY APP 1465

pjackson@lasvegasnevada.gov

“Building Community to Make Life Better”



Your opinion is important! Click [here](#) to take a short survey.

From: Steve Jones [<mailto:SJones@gcwengineering.com>]

Sent: Thursday, August 16, 2018 5:06 PM

To: Peter Jackson; Jennifer Shinn; Scott Plummer; Mark Sorensen

Cc: Frank Pankratz (frank@EHBCompanies.com); Yohan Lowie (EHB Companies); Oh-Sang Kwon

Subject: The 435 TDS Comments Review Meeting

GCW has constructed the attached meeting notes have been to summarize the meeting between GCW and CLV Flood Control on August 13, 2018 regarding the TDS for The 435 Storm Drain project addressing the comments received from CLV staff dated July 26, 2018.

Please review and inform me of any comments or questions.

Thanks,



[Steve Jones, P.E.](#)

Vice President

Flood Control Division Manager

O 702.804.2000

D 702.804.2130

F 702.804.2299

C 702.545.5034

1555 South Rainbow Boulevard

Las Vegas, Nevada 89146



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Note - Any files contained within are to be used for information ONLY.

Accuracy or design information to be verified from approved original plans. Use of electronic media is at the sole risk of the user.

LO 00009859

6499

REPLY APP 1466

EXHIBIT “ZZZZZ”

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1. I am the Building Official in the Community Development Department for the City of Las Vegas. I have held this position since September of 2022. I am one of the custodians of records for the Community Development Department. I have personal knowledge of the facts set forth herein, except as to those stated on information and belief and, as to those, I am informed and believe them to be true. If called as a witness, I could and would competently testify to the matters stated herein.

3. Section 301.1 of the Administrative Code states the general rule that no owner shall cause any building, structure, or improvements to be constructed unless an appropriate permit for each building, structure, or improvement has first been obtained from the Building Official.

5. Temporary construction fences erected for the duration of construction or demolition activities are exempt from building permit requirements under Administrative Code Section 301.4.1, item 32. Accordingly, a property owner in possession of a building permit does not require the Building Department's permission to erect a construction fence around the construction site. The majority of construction projects in Las Vegas erect such construction fences to control access to the construction site.

I declare under the penalty of perjury of the laws of the State of Nevada that the foregoing is true and correct.


Michael Cunningham

EXHIBIT “ZZZZZ-1”

CITY OF LAS VEGAS
ADMINISTRATIVE CODE, 2019 EDITION



unlawful occupancy of the building or structure in violation of the provisions of this Code or the adopted technical or of the order or direction made pursuant thereto.

205.4 VIOLATION PENALTIES. Any person who violates a provision or fails to comply with any of the requirements of this Code or the adopted technical codes or who erects, constructs, alters, demolishes, alters or repairs a building or structure in violation of the approved construction or demolition documents or directive of the Building Official or of a permit or certificate issued under the provisions of this Code shall be subject to the penalties as prescribed by law.

Chapter 3

PERMITS AND INSPECTIONS

SECTION 301 – PERMITS

301.1 Permits Required. Except as otherwise specified in this section, no owner or authorized agent shall cause any new building, structure, building service equipment or onsite improvement regulated by this Code or any of the technical codes to be erected, constructed, enlarged, altered, repaired, moved, improved, removed, converted, demolished, change the occupancy of any existing building or structure or erect, install, enlarge, alter, repair remove, convert or replace any existing electrical, gas, mechanical, or plumbing system, which the installation of is regulated by this Code or cause any such work described above to be done unless a separate, appropriate permit for each building, structure, building service equipment or onsite improvement has first been obtained from the Building Official.

Exception: Emergency repairs of building service equipment may be repaired or replaced without a permit which is serving an occupied portion of the building and may be operated temporarily if a request for a permit and an inspection of that replacement equipment has been filed with the Building Official not more than 1 business day after such replacement work was completed and before any portion of the building service equipment is concealed.

Required permits and permit exemptions applicable to special events shall be as specified in the policy document titled “Special Events Permits” developed and administered by the Building Official and the Fire Marshall.

If work is commenced before a necessary and appropriate permit for the work has been obtained, the Building Official is authorized to charge an additional fee in the amount of the building permit fee on a graduated scale with double fees as a minimum depending on the number of offenses. If technical officer(s) is(are) required to inspect a site, an

investigation fee shall be charged in addition to the additional graduated permit fees. Additional fees for compliance or investigations by other departments or agencies may apply. The graduated scale shall be as follows:

1st offense – Double Permit Fees plus an Investigation Fee

2nd offense – Up to Triple Permit Fees plus an Investigation Fee, the department may send a notice of complaint to Nevada State Contractor's board

3rd and subsequent offenses – Up to Quadruple Permit Fees plus an Investigation fee, the department may send notice of complaint to Nevada State Contractor's Board and refer the work without permit violation to Code Enforcement for citation for further remedy.

301.2 Licensing and Contractor Requirements. Building permits shall not be issued for building work required to be performed by a licensed contractor under NRS Chapter 624 unless the general contractor or applicant is appropriately licensed by the State of Nevada and has the appropriate business license issued or recognized by the City. A general contractor or design professional licensed by the State of Nevada to whom a permit is issued shall be responsible for all work authorized for the project and shall post at the job site a list of all subcontractors doing work on the job with their names, their State subcontractor's license numbers and classifications and their business license numbers. Mechanical, electrical and plumbing subcontractors shall register with the Department when all permits have been obtained by the general contractor prior to scheduling of inspections. Contractor and subcontractors shall meet all applicable qualifications and requirements described in the technical codes. Applications for all building permits shall include the design professional's and/or contractor's license number, monetary limits, and licensed subcontractors and monetary limits.

NOTE: Additional licensing requirements concerning plumbing work are contained in this chapter. Additional licensing requirements concerning mechanical work are contained in this chapter.

301.4 Work Exempt from Permit. Permits shall not be required for the following:

301.4.1 Building Permits Exemptions:

1. Construction work on property owned by the United States or on property owned by any other governmental entity, to the extent exempted by State law.
2. Amusement devices and structures, including merry-go-rounds, Ferris wheels, rotating conveyances, slides and similar devices, and any other accessory structure consisting of a cover or roof whose use is necessary for the operation of any such device or structure when such device or

structure is used for less than 30 days. A storage building or detached structure that is not an integral part of an amusement device or structure does not qualify as an exempt accessory structure for purposes of this paragraph. The exemption contained in this paragraph does not apply to any electrical, mechanical or plumbing work that is to be done in connection with amusement devices or structures that are to be used on a site.

3. Oil derricks.
4. Cases, counters, and partitions that do not exceed 5 feet 9 inches in height and not containing electrical branch circuits.
5. Privately owned water tanks supported directly upon grade if the capacity does not exceed 5,000 gallons and the ratio of height to diameter or width does not exceed two to one.
6. Platforms, walks, driveways, and similar exterior flatwork not more than 30 inches above grade and not over any basement or story below, and are not part of an accessible route.
7. Painting, papering, cabinets, countertops, and similar finish work, floor covering, except for trim and decorative work.
8. Temporary motion picture, television and theater stage sets and scenery.
9. Window awnings supported by an exterior wall of a one-family or two-family dwelling, or an accessory structure, when projecting not more than 54 inches.
10. Residential television or radio antennas whose height design does not exceed 10 feet above the height of the tallest structure on the property, and so located that the distance to the nearest property line is equal to or greater than the total height of the antenna mast.
11. Construction directly relating to the delivery of a utility service, built by a public utility company operating under the control of the Public Utilities Commission. This exemption applies only to buildings, structures, or service equipment that is directly used in utility generation or distribution and is installed on properly registered easements belonging to water, gas, power, telephone, or other utility companies governed under the State of Nevada Public Utilities Commission, another State agency, or a public franchise. This exemption does not apply to office buildings, grading, occupied support buildings and general site development.
12. Any portable unit refrigerating system (cooling only) as defined in the Mechanical Code.

13. Any wall, including a retaining wall, that is not over 30 inches in height, measured from the low finished grade to the grade on the opposite side. This exemption does not apply to:
 - a. Any wall that supports a surcharge;
 - b. Any wall that retains flammable liquids; or
 - c. Any wall of combined materials that exceeds 30 inches in height.
14. One-story detached single family residential accessory buildings used as tool and storage sheds, playhouses, and similar uses, provided the floor area does not exceed 200 square feet. This exemption does not eliminate applicable zoning codes requirements.
15. Temporary grandstands, bleachers, viewing platforms, and similar uses mounted on, or attached to, motor vehicles or trailers (including stairs, ramps and similar access features serving such motor vehicles or trailers) used in conjunction with special events. Where deemed appropriate by the Building Official, reference shall be made to the policy document titled "Special Events Permits" developed by the Building Official.
16. Tents and canopies erected for a period of 180 days or less.

NOTE: This exemption does not eliminate applicable fire codes requirements.
17. Temporary fences erected for a period of time as approved by the Building Official or 180 days as directed.
18. On-ground storable pool as defined in the International Swimming Pool and Spa Code which is accessory to a single family dwelling and in which the pool walls are entirely above the adjacent grade.
19. Portable spas, accessory to a single family residence with all heating and circulating equipment integral to the manufacturing product and entirely above the adjacent grade.
20. Project offices including construction trailers and related storage sheds used for the purpose of the construction on an active construction project.
21. Travel trailers and recreational vehicles, or other axled vehicles as permitted or licensed by the State of Nevada.
22. Livestock shade structures open on a minimum of three sides and not more

than 1,500 square feet in area.

23. Non-motorized outdoor playground equipment.
24. Storage racks and/or shelving less than or equal to 8 feet in height.
25. Minor repair of interior or exterior stucco/lath/drywall, provided:
 - a. No framing needs replacement or repair; and
 - b. For stucco, the repaired area not exceed 32 square feet in area; and
 - c. The area of repair is not a fire-resistance rated assembly comprised of more than one layer of drywall on each side or any special material(s) necessary to maintain the required fire-resistance rating of the assembly (i.e. fire-stopping of penetrations.)
26. Replacement of roof covering materials, other than tile roofing, provided no structural components are repaired or replaced and provided no more than 64 square feet of roof sheathing is replaced.
27. Repair or replacement of components of listed appliances.
28. Replacement of exterior or interior doors, hinges, hardware and decorative trim related to such doors, provided the following conditions are met:
 - a. The replacement door is of the same size and type.
 - b. The replacement door does not require any modification to existing wall framing.
 - c. The existing door is not a component of a fire-resistive rated construction element.
29. Replacement of exterior or interior window glazing, provided the following conditions are met:
 - a. The replacement window glazing is of the same size and type and thickness.
 - b. The replacement window does not require any modification to existing wall framing.
 - c. The existing glazing is not a component of a fire-resistive rated construction element.

30. Installation of insulation on existing single-family residences where other permits are not required;
31. Fencing not over 7 feet high except for those fences within the front setback of a single family dwelling and those that are not a part of a pool or spa barrier;
32. Temporary construction fences erected for the duration of the construction or demolition activity. Such fences shall be removed upon completion of the activity.
33. Minor demolition of unpermitted work when the work is restored to the previously permitted condition.
34. Repair of less than 32 square feet of stone or brick veneer when the damage is less than 6 feet above adjacent grade.
35. Repair of block walls 6 feet in height or less and the repair is no greater in length than 20 linear feet, provided there is no damage to existing footing.
36. Work required to render a building or structure stable following damage from fire, wind, water, vehicle impact, or other causes and to clear the site of damaged materials to allow inspection to ascertain the scope of required repairs, when authorized by the *Building Official*.

301.4.2 Grading Permit Exemptions:

1. Grading associated with agriculture within districts approved for agriculture.
2. Excavation for construction of a structure permitted under this code.
3. Excavation for Cemetery graves.
4. Earthwork or grading for refuse disposal sites controlled by other regulations.
5. Excavations for wells, septic systems, or trenches for utilities.
6. Mining, quarrying, excavation, processing or stockpiling rock, sand, gravel, aggregate or clay controlled by other regulatory agencies provided such operations do not affect the lateral support of, or significantly increase stresses in soil on adjoining properties.
7. Exploratory excavations performed under the direction of a registered design professional.